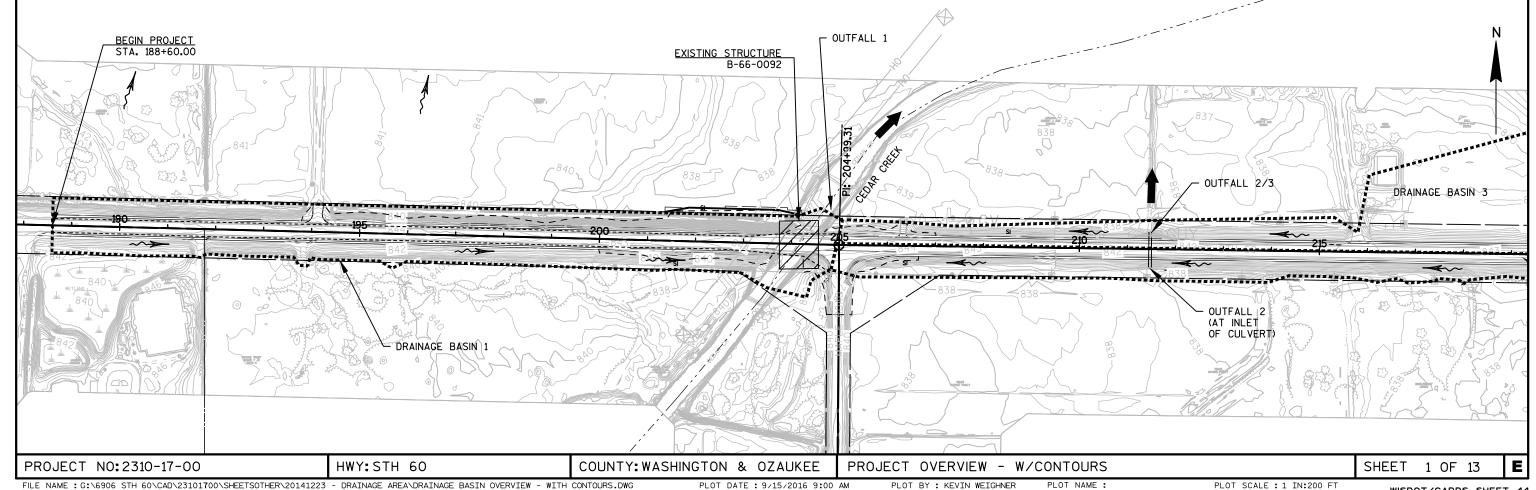
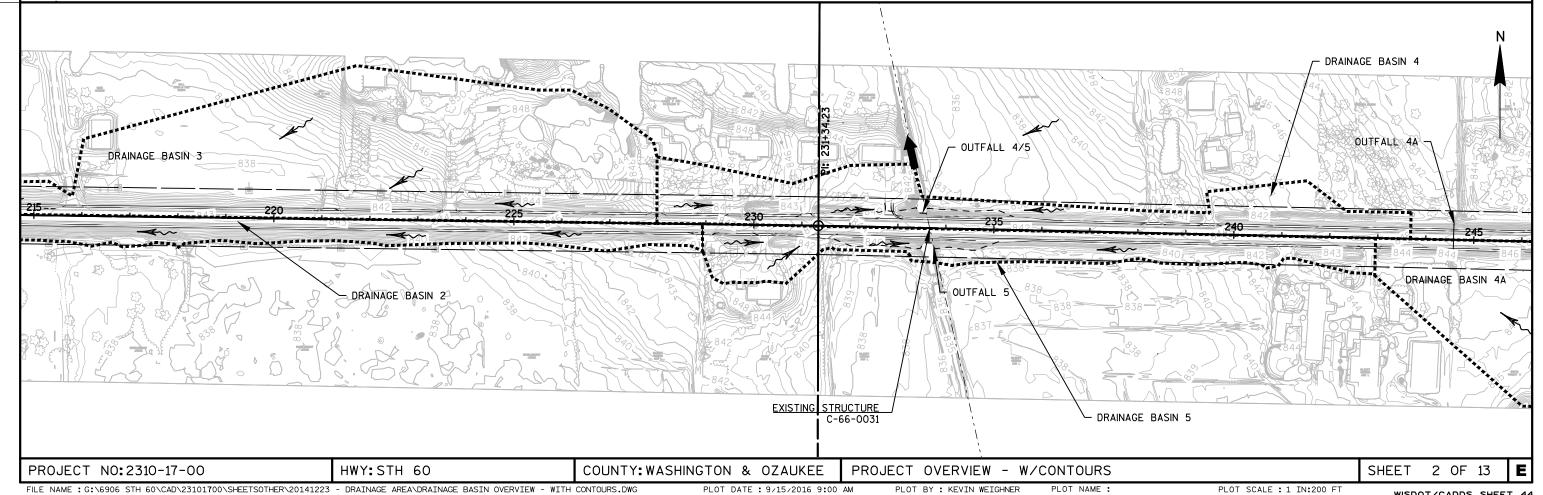
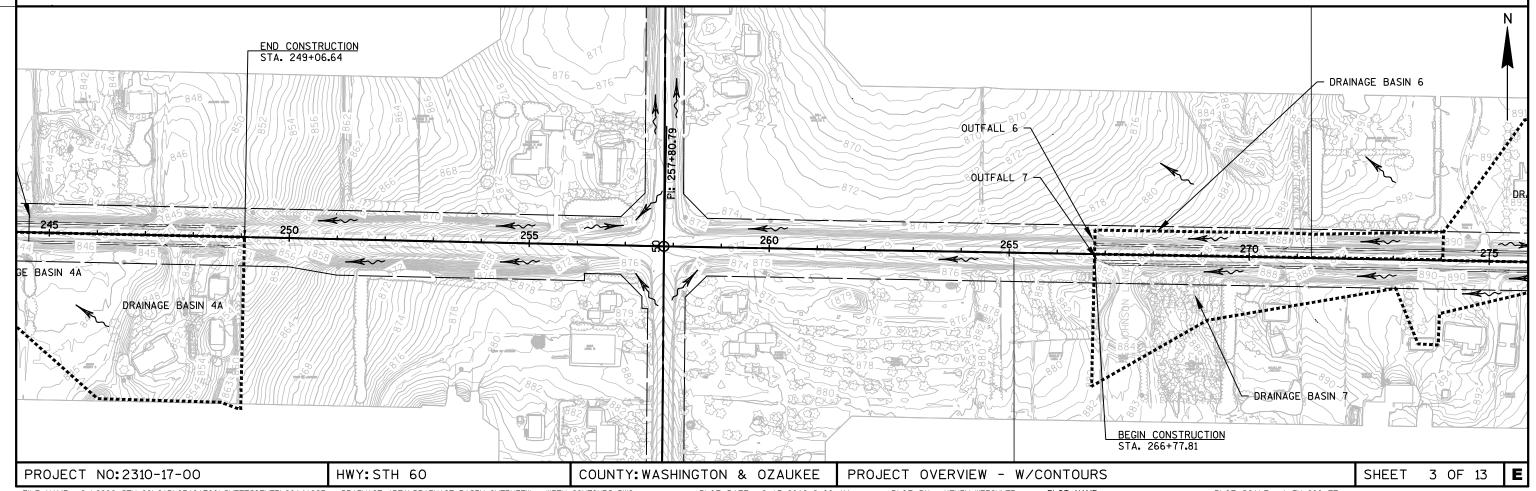
OUTFALL	1	2	2/3
PROPOSED OUTFALL STATION (APPROX.)	204+00	211+50	211+50
PROPOSED STATIONS (APPROX.)	188+60 TO 205+00	205+00 TO 228+93	205+00 TO 228+93
EXISTING DRAINAGE AREA (AC) (APPROX.)	4.49	3.15	11.6
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/CULVERT	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/CULVERT	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING OUTFALL STATION (APPROX.)	204+00	211+50	211+50
EXISTING STATIONS (APPROX.)	188+60 TO 205+00	205+00 TO 228+93	205+00 TO 228+93
PROPOSED LENGTH (FT) (APPROX.)	1640	2393	2393
EXISTING LENGTH (FT) (APPROX.)	1640	2393	2393
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		



OUTFALL	4/5	4A	5
PROPOSED OUTFALL STATION (APPROX.)	233+53	244+50	233+53
PROPOSED STATIONS (APPROX.)	228+00 TO 243+70	243+00 TO 249+00	228+93 TO 243+00
EXISTING DRAINAGE AREA (AC) (APPROX.)	5.27	3.87	2.27
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH	OVERLAND/PAVEMENT RUNOFF/CULVERT	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH	OVERLAND/PAVEMENT RUNOFF/CULVERT	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
EXISTING OUTFALL STATION (APPROX.)	233+53	244+50	233+53
EXISTING STATIONS (APPROX.)	227+98 TO 243+70	243+00 TO 249+00	228+93 TO 243+00
PROPOSED LENGTH (FT) (APPROX.)	1570	600	1407
EXISTING LENGTH (FT) (APPROX.)	1570	600	1407
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		



	OUTFALL	6	7	
	PROPOSED OUTFALL STATION (APPROX.)	266+78	266+78	
2	PROPOSED STATIONS (APPROX.)	266+78 TO 274+00	266+78 TO 277+00	
	EXISTING DRAINAGE AREA (AC) (APPROX.)	0.85	2.8	
	PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH	
	EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH	
	EXISTING OUTFALL STATION (APPROX.)	266+78	266+78	
	EXISTING STATIONS (APPROX.)	266+78 TO 274+00	266+78 TO 277+00	
	PROPOSED LENGTH (FT) (APPROX.)	722	1022	
	EXISTING LENGTH (FT) (APPROX.)	722	1022	
	PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
	EXISTING ROADWAY			



10
283+53
277+00 TO 284+20
0.92
OVERLAND/PAVEMENT RUNOFF/DITCH
OVERLAND/PAVEMENT RUNOFF/DITCH
283+97

277+00 TO 284+00

720

720

RURAL 2-LANE HIGHWAY WITH BYPASS LANES RURAL 2-LANE HIGHWAY WITH BYPASS LANES

9

288+98

284+20 TO 300+93

2.54

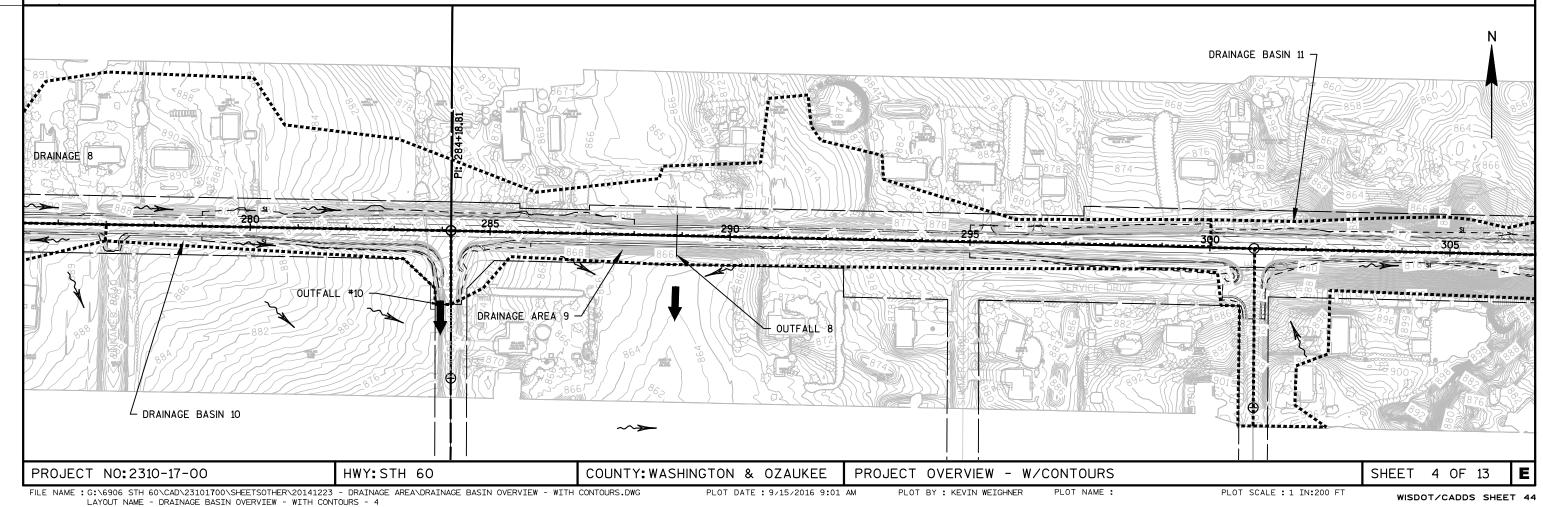
OVERLAND/PAVEMENT RUNOFF/DITCH

OVERLAND/PAVEMENT RUNOFF/DITCH

288+98 284+20 TO 300+93

1673

1673



8

288+98

274+00 TO 300+01

9.98

OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT

OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT

288+98

274+00 TO 300+01

2601

2601

OUTFALL

PROPOSED OUTFALL STATION (APPROX.)

EXISTING DRAINAGE AREA (AC) (APPROX.)

EXISTING OUTFALL STATION (APPROX.)

PROPOSED STATIONS (APPROX.)

EXISTING STATIONS (APPROX.) PROPOSED LENGTH (FT) (APPROX.)

EXISTING LENGTH (FT) (APPROX.)

PROPOSED CONDITIONS

EXISTING CONDITIONS

PROPOSED ROADWAY

OUTFALL	11/12	12	13/14
PROPOSED OUTFALL STATION (APPROX.)	320+61	320+61	327+65
PROPOSED STATIONS (APPROX.)	300+01 TO 323+19	300+93 TO 323+19	322+83 TO 350+38
EXISTING DRAINAGE AREA (AC) (APPROX.)	11.78	5.06	9.16
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING OUTFALL STATION (APPROX.)	320+61	320+61	327+65
EXISTING STATIONS (APPROX.)	300+01 TO 323+19	300+93 TO 323+19	322+83 TO 350+38
PROPOSED LENGTH (FT) (APPROX.)	2318	2226	2755
EXISTING LENGTH (FT) (APPROX.)	2318	2226	2755
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
OUTFALL	14		

327+65 323+19 TO 350+38

7.06

OVERLAND/PAVEMENT RUNOFF/CULVERT

OVERLAND/PAVEMENT RUNOFF/CULVERT

327+65

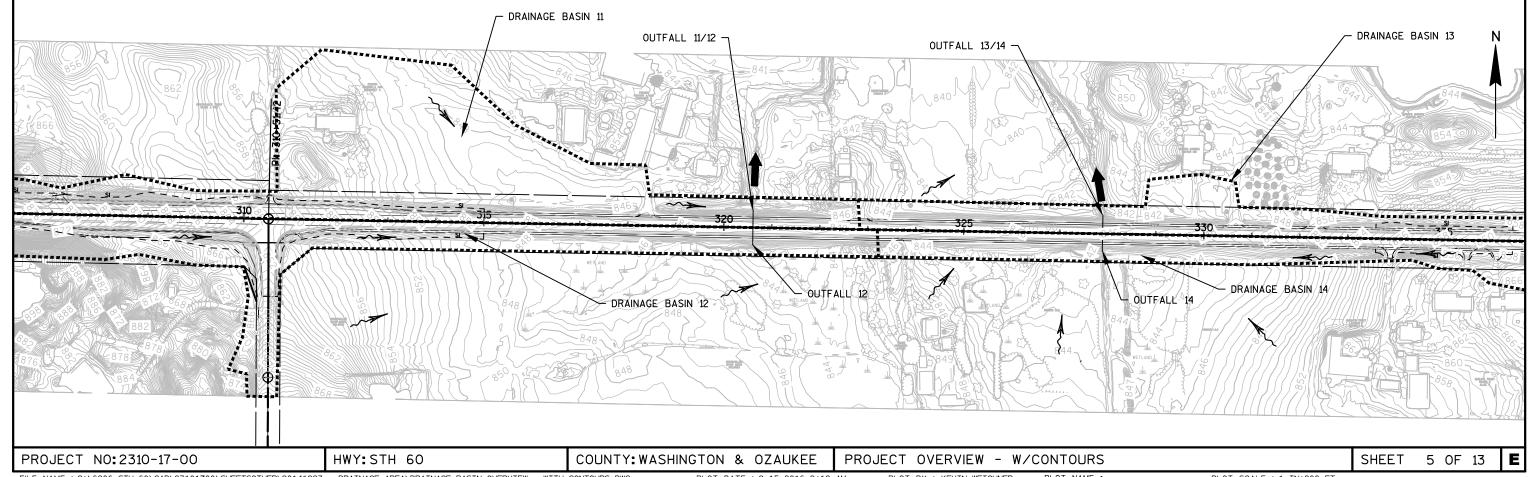
323+19 TO 350+38

2719

2719

RURAL 2-LANE HIGHWAY WITH BYPASS LANES

RURAL 2-LANE HIGHWAY WITH BYPASS LANES



PROPOSED OUTFALL STATION (APPROX.)

EXISTING DRAINAGE AREA (AC) (APPROX.)

EXISTING OUTFALL STATION (APPROX.)

PROPOSED STATIONS (APPROX.)

EXISTING STATIONS (APPROX.)

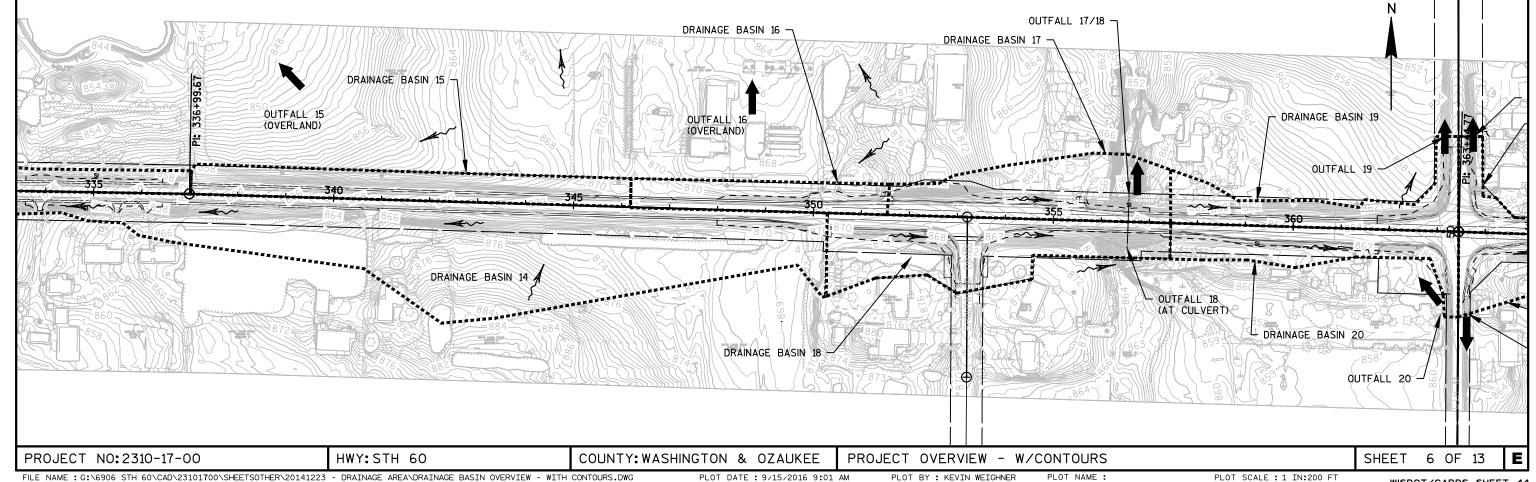
PROPOSED LENGTH (FT) (APPROX.)

EXISTING LENGTH (FT) (APPROX.)

PROPOSED CONDITIONS
EXISTING CONDITIONS

PROPOSED ROADWAY

OUTFALL	15	16	17/18
PROPOSED OUTFALL STATION (APPROX.)	OVERLAND	OVERLAND	356+55
PROPOSED STATIONS (APPROX.)	337+02 TO 347+19	347+19 TO 351+53	350+28 TO 357+44
EXISTING DRAINAGE AREA (AC) (APPROX.)	1.27	0.76	3.36
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF	OVERLAND/PAVEMENT RUNOFF	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF	OVERLAND/PAVEMENT RUNOFF	OVERLAND/PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING OUTFALL STATION (APPROX.)	OVERLAND	OVERLAND	356+55
EXISTING STATIONS (APPROX.)	337+02 TO 347+19	347+19 TO 351+53	350+28 TO 357+44
PROPOSED LENGTH (FT) (APPROX.)	1017	434	716
EXISTING LENGTH (FT) (APPROX.)	1017	434	716
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
OUTFALL	18	19	20
PROPOSED OUTFALL STATION (APPROX.)	356+55	363+02	363+02
PROPOSED STATIONS (APPROX.)	350+28 TO 357+40 357+44 TO 363+02		358+29 TO 363+02
EXISTING DRAINAGE AREA (AC) (APPROX.)	1.89	1.02	1.06
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH
EXISTING OUTFALL STATION (APPROX.)	356+55	363+02	363+02
EXISTING STATIONS (APPROX.)	350+28 TO 357+40	357+44 TO 363+02	358+29 TO 363+02
PROPOSED LENGTH (FT) (APPROX.)	712	558	473
EXISTING LENGTH (FT) (APPROX.)	712	558	473
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		



OUTFALL	21	22	23
PROPOSED OUTFALL STATION (APPROX.)	363+68	363+68	378+47
PROPOSED STATIONS (APPROX.)	363+68 TO 365+99	363+45 TO 365+99	365+99 TO 389+75
EXISTING DRAINAGE AREA (AC) (APPROX.)	0.42	0.74	6.58
PROPOSED CONDITIONS	PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH	PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING CONDITIONS	PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH	PAVEMENT RUNOFF/CULVERT/DITCH
EXISTING OUTFALL STATION (APPROX.)	363+68	363+68	378+47
EXISTING STATIONS (APPROX.)	363+68 TO 365+99	363+45 TO 365+99	365+99 TO 389+75
PROPOSED LENGTH (FT) (APPROX.)	231	254	2376
EXISTING LENGTH (FT) (APPROX.)	231	254	2376
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
OUTFALL	24		

378+47

365+99 TO 389+75

3.3

OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT

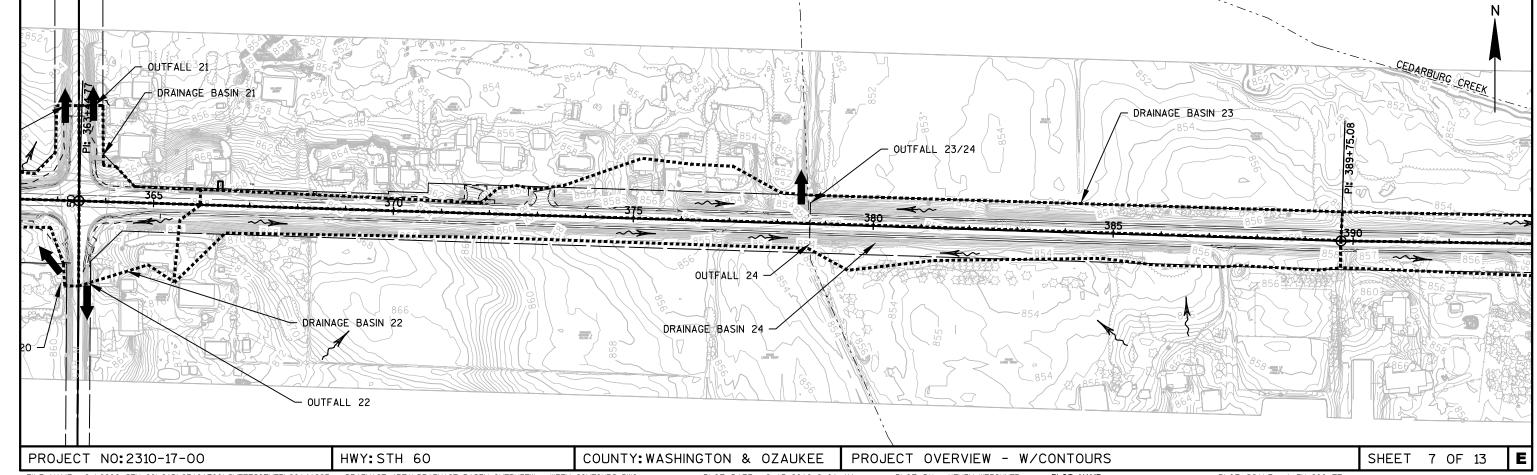
378+47

365+99 TO 389+75

2376 2376

RURAL 2-LANE HIGHWAY WITH BYPASS LANES

RURAL 2-LANE HIGHWAY WITH BYPASS LANES



PROPOSED OUTFALL STATION (APPROX.)

EXISTING DRAINAGE AREA (AC) (APPROX.)

EXISTING OUTFALL STATION (APPROX.)

PROPOSED STATIONS (APPROX.)

EXISTING STATIONS (APPROX.)

PROPOSED LENGTH (FT) (APPROX.)

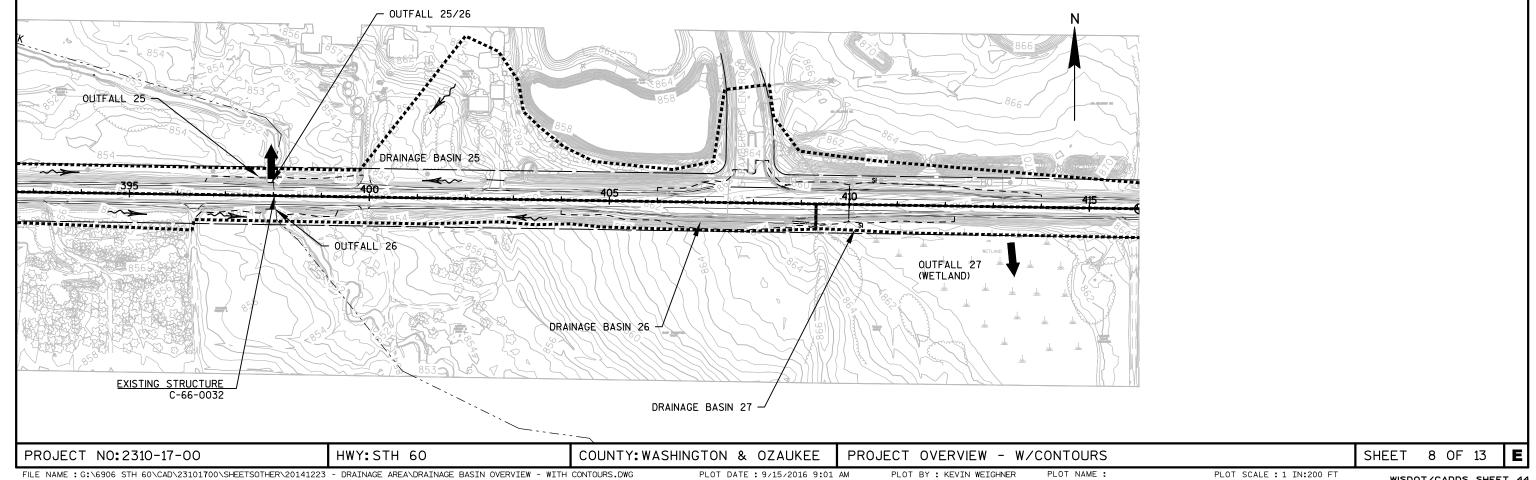
EXISTING LENGTH (FT) (APPROX.)

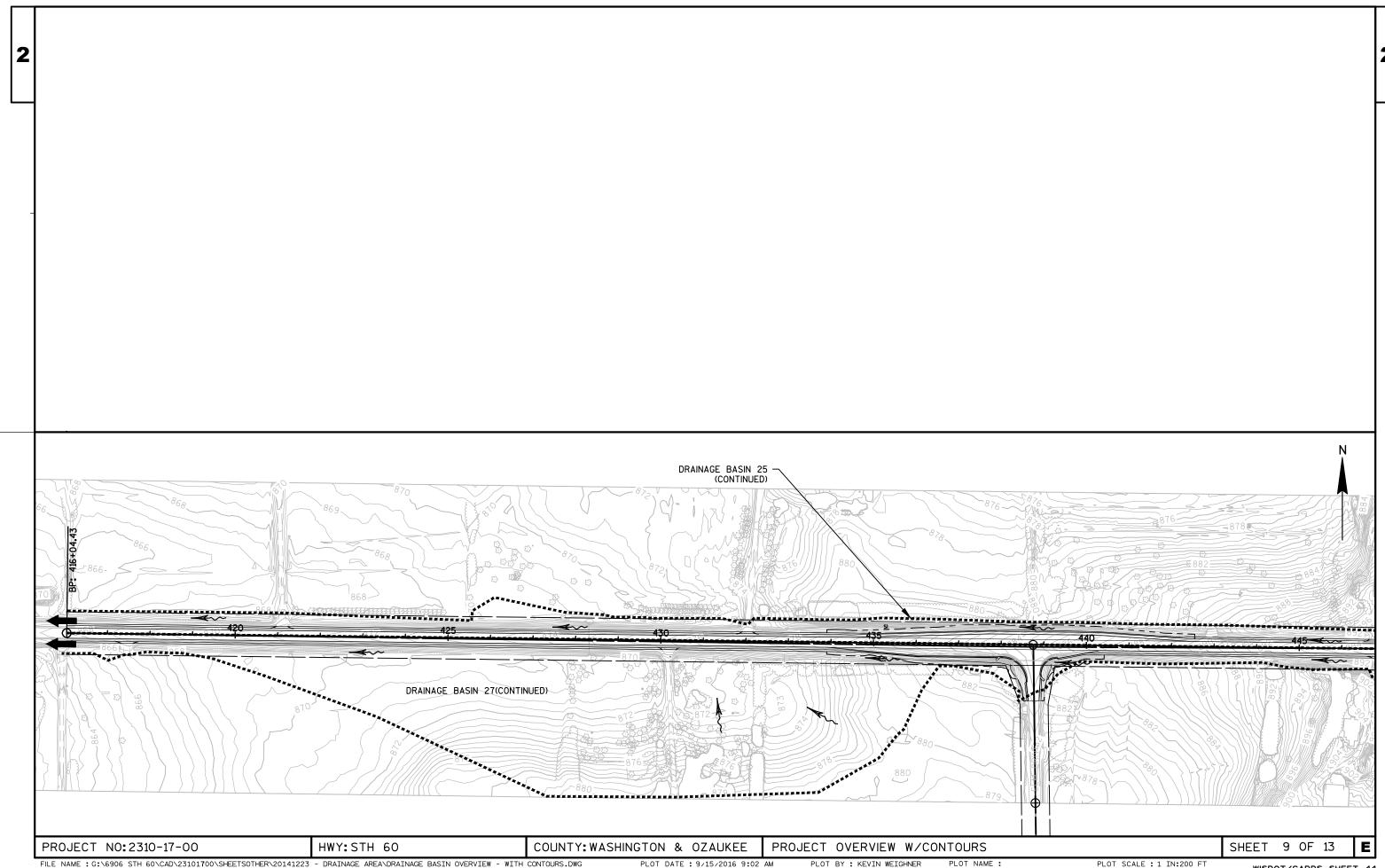
PROPOSED CONDITIONS

EXISTING CONDITIONS

PROPOSED ROADWAY

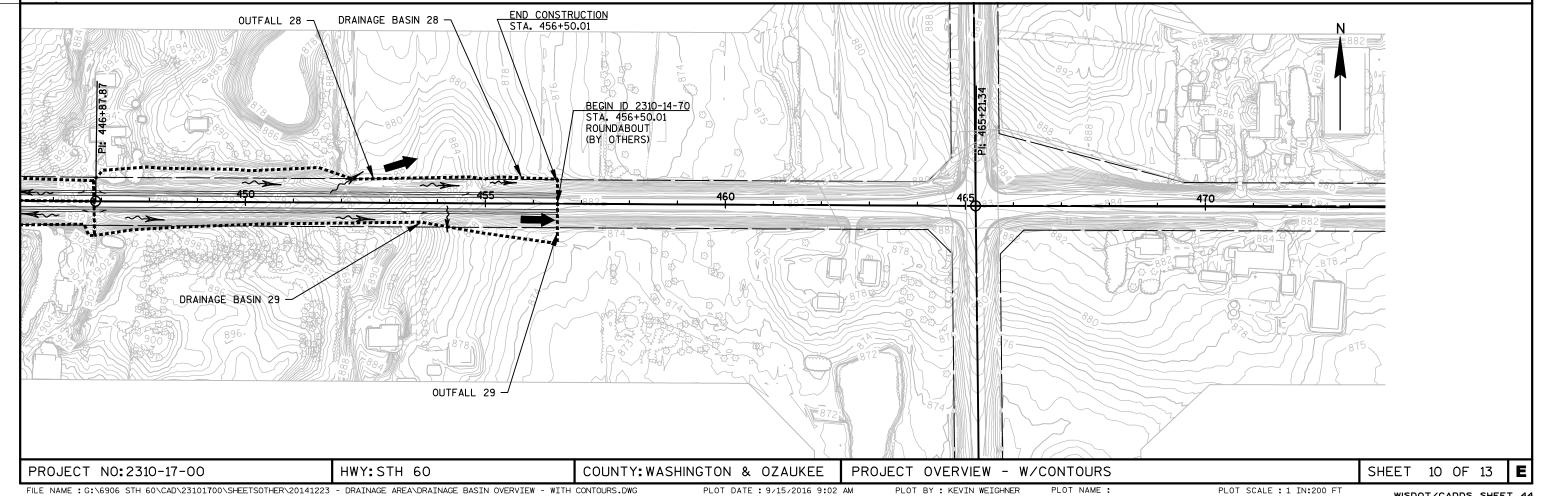
OUTFALL	25/26	26	27
PROPOSED OUTFALL STATION (APPROX.)	397+95	397+95	OVERLAND
PROPOSED STATIONS (APPROX.)	389+75 TO 446+84	389+75 TO 409+31	409+31 TO 446+84
EXISTING DRAINAGE AREA (AC) (APPROX.)	12.7	2.6	13.07
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	OVERLAND/PAVEMENT RUNOFF/DITCH/WETLAND
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	OVERLAND/PAVEMENT RUNOFF/DITCH/WETLAND
EXISTING OUTFALL STATION (APPROX.)	397+95	397+95	OVERLAND
EXISTING STATIONS (APPROX.)	389+75 TO 446+84	389+75 TO 409+31	409+31 TO 446+84
PROPOSED LENGTH (FT) (APPROX.)	5709	1956	3753
EXISTING LENGTH (FT) (APPROX.)	5709	1956	3753
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		



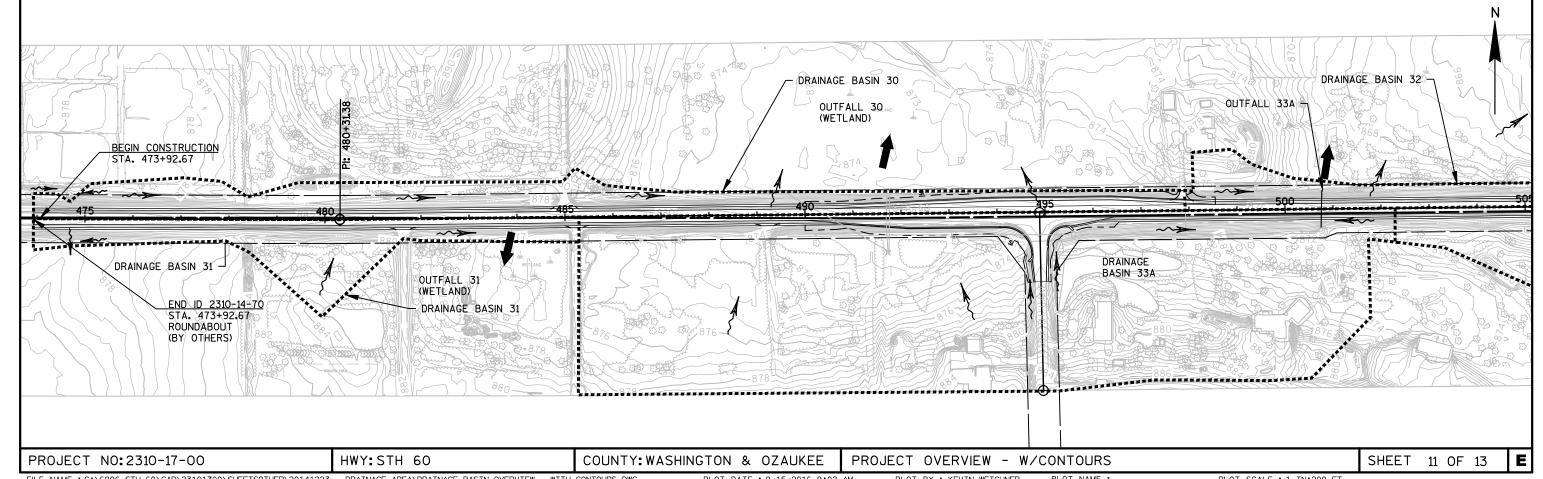


|--|

	OUTFALL 28		29	
	PROPOSED OUTFALL STATION (APPROX.) 452+40		456+50	
2	PROPOSED STATIONS (APPROX.)	446+84 TO 456+50	446+84 TO 456+50	
	EXISTING DRAINAGE AREA (AC) (APPROX.)	1.33	1.33	
	PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH	
	ISTING CONDITIONS OVERLAND/PAVEMENT RUNOFF/DITCH		OVERLAND/PAVEMENT RUNOFF/DITCH	
	EXISTING OUTFALL STATION (APPROX.)	452+40	456+50	
	EXISTING STATIONS (APPROX.)	446+84 TO 456+50	446+84 TO 456+50	
	PROPOSED LENGTH (FT) (APPROX.)	966	966	
	EXISTING LENGTH (FT) (APPROX.)	966	966	
	PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
_	EXISTING ROADWAY			



OUTFALL	30	31	33A
PROPOSED OUTFALL STATION (APPROX.)	OVERLAND	483+87	500+76
PROPOSED STATIONS (APPROX.)	474+06 TO 497+91	474+06 TO 485+30	485+30 TO 502+29
EXISTING DRAINAGE AREA (AC) (APPROX.)	3.3	1.88	13.74
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH/OVERLAND	OVERLAND/PAVEMENT RUNOFF/DITCH/WETLAND	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH/OVERLAND	OVERLAND/PAVEMENT RUNOFF/DITCH/WETLAND	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
EXISTING OUTFALL STATION (APPROX.)	OVERLAND	483+87	500+76
EXISTING STATIONS (APPROX.)	474+06 TO 497+91	474+06 TO 485+30	485+30 TO 502+29
PROPOSED LENGTH (FT) (APPROX.)	2385	1124	1699
EXISTING LENGTH (FT) (APPROX.)	2385	1124	1699
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES		



OUTFALL	32	33B	34	
PROPOSED OUTFALL STATION (APPROX.)	510+83	510+83	OVERLAND	
PROPOSED STATIONS (APPROX.)	497+91 TO 524+28	502+29 TO 522+39	524+28 TO 536+00	
EXISTING DRAINAGE AREA (AC) (APPROX.)	3.68	10.18	1.61	
PROPOSED CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	PAVEMENT/WETLAND/OVERLAND	
EXISTING CONDITIONS	OVERLAND/PAVEMENT RUNOFF/DITCH	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT	PAVEMENT/WETLAND/OVERLAND	
EXISTING OUTFALL STATION (APPROX.)	510+83	510+83	536+00	
EXISTING STATIONS (APPROX.)	497+91 TO 524+28	502+29 TO 522+39	524+28 TO 536+00	
PROPOSED LENGTH (FT) (APPROX.)	2637	2010	1171	
EXISTING LENGTH (FT) (APPROX.)	2637	2010	1171	
PROPOSED ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES			
- EXISTING ROADWAY	RURAL 2-LANE HIGHWAY WITH BYPASS LANES			
OUTFALL	35			

530+97

522+39 TO 536+00

2.31
OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT

OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT

530+97

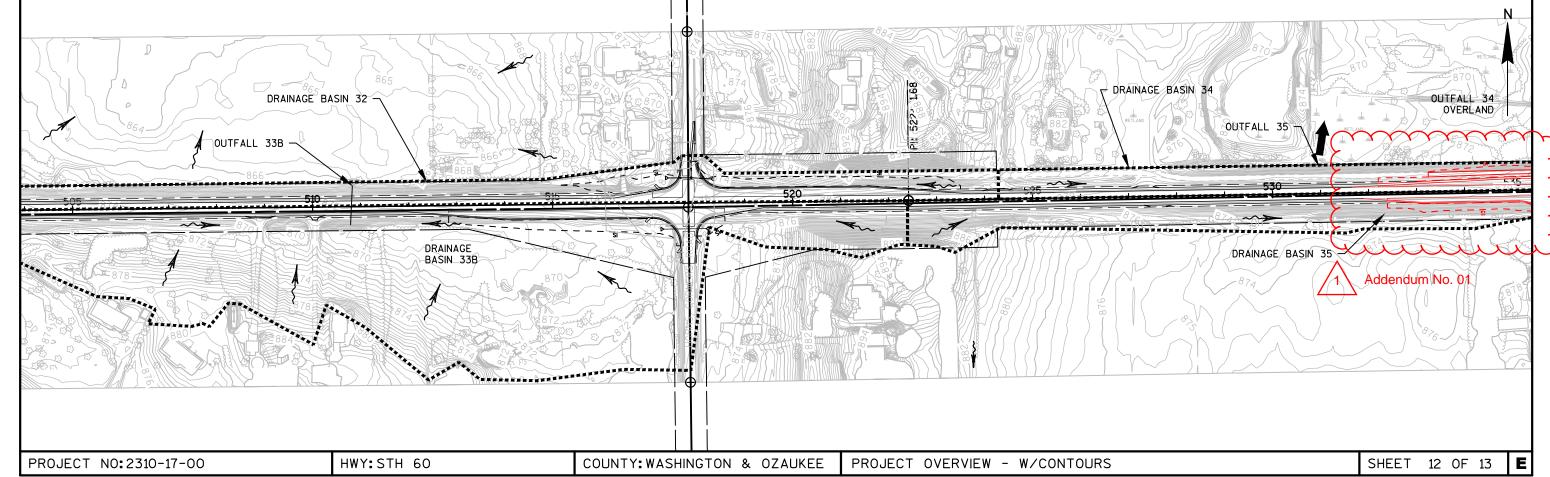
522+39 TO 536+00

1361

1361

RURAL 2-LANE HIGHWAY WITH BYPASS LANES

RURAL 2-LANE HIGHWAY WITH BYPASS LANES



PROPOSED OUTFALL STATION (APPROX.)

EXISTING DRAINAGE AREA (AC) (APPROX.)

EXISTING OUTFALL STATION (APPROX.)

PROPOSED STATIONS (APPROX.)

EXISTING STATIONS (APPROX.)

PROPOSED LENGTH (FT) (APPROX.)

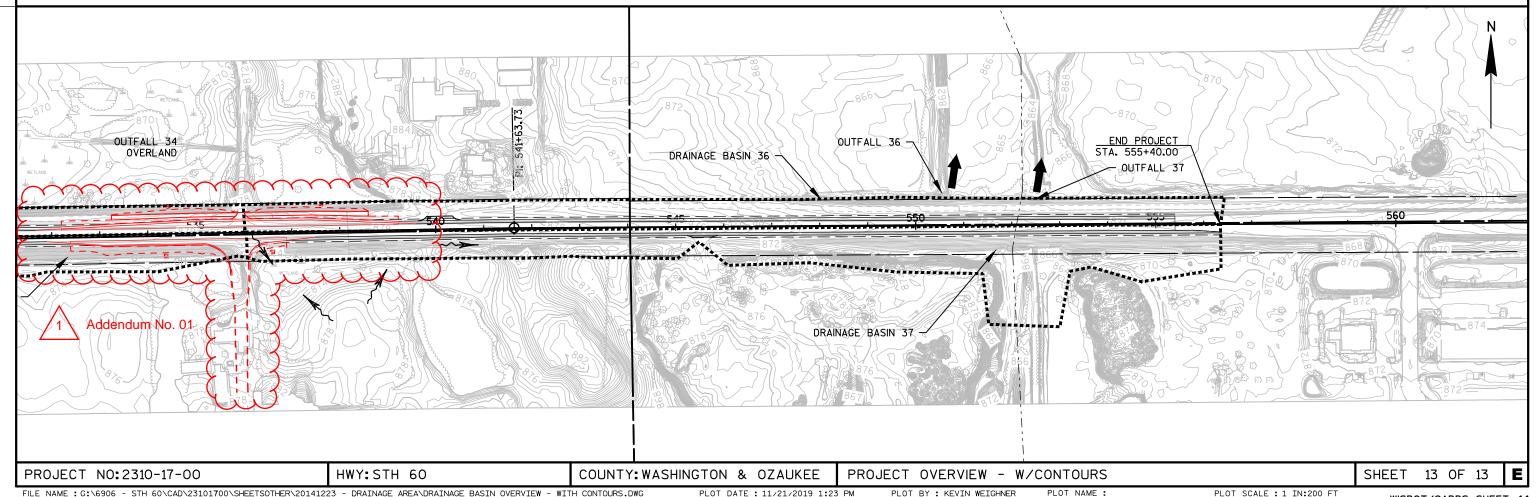
EXISTING LENGTH (FT) (APPROX.)

PROPOSED CONDITIONS

EXISTING CONDITIONS

PROPOSED ROADWAY

OUTFALL	36	37
PROPOSED OUTFALL STATION (APPROX.)	550+50	552+45
PROPOSED STATIONS (APPROX.)	536+00 TO 555+40	536+00 TO 555+40
EXISTING DRAINAGE AREA (AC) (APPROX.)	2.58	3.92
PROPOSED CONDITIONS	PAVEMENT RUNOFF/DITCH/OVERLAND	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
EXISTING CONDITIONS	PAVEMENT RUNOFF/DITCH/OVERLAND	OVERLAND/PAVEMENT RUNOFF/DITCH/CULVERT
EXISTING OUTFALL STATION (APPROX.)	550+50	552+45
EXISTING STATIONS (APPROX.)	536+00 TO 555+40	536+00 TO 555+40
PROPOSED LENGTH (FT) (APPROX.)	1940	1940
EXISTING LENGTH (FT) (APPROX.)	1940	1940
PROPOSED ROADWAY	RURAL 2-LANE HIGHWA	AY WITH BYPASS LANES
EXISTING ROADWAY	RURAL 2-LANE HIGHWA	AY WITH BYPASS LANES



1	Basic Project Information	
2	Project ID: 2310-17-00 Title: STH 60 - Eagle Drive to STH 181	
4 5	Designer/Checker: JP/RT	INC
6	DOT Region/Firm Name: SE/COLLINS ENGINEERS Date: 3/5/2015 Updated 11/26/2019	INC.
7	HIGHWAY:	STH 60
8	LIMITS:	EAGLE DRIVE TO STH 181
9	COUNTY:	WASHINGTON & OZAUKEE
10 11	DESCRIPTION OF WORK: PROJECT MANAGER:	RESURFACING AND INTERSECTION IMPROVEMENTS NGUYEN LY
12	PS&E DATE:	1-Aug-19
13	DESIGN STAGE	☐ Planning ☐ 30% ☐ 60% ☐ 90% ☑ Final
14	Drainage Summary	
	-	TO MUTUUM AND CUR DACIN OF THE DROUGETS IF VEC DESCRIBE THE CAUSE OF THE CHANCE
15	AND WHY IT IS NECESSARY.	E WITHIN ANY SUB BASIN OF THE PROJECT? IF YES, DESCRIBE THE CAUSE OF THE CHANGE
		21, 22, 23, 24, 25, 27, 28, 29, 30, 31, 32, 33A, 33B, 2/3, 4/5, 13/14, and 23/24 have an increase
		e increase in these basins is minimal and will no adverse impact to the surrounding areas since is not changing as a result of the project improvements. In addition, existing culverts and
	ditches have been anlyzed to shown no significant incre	ease in headwater in the proposed condition. Drainage Basin 8 has an increase in runoff (7%)
	-	 This increase will have no impact as the existing ditch and culvert have been determined to north of Drainage Basin 8 will pond and be contained on private property in minor rain events,
		ring larger rain events and reach the R/W ditch. Drainage Basin "8 (Off-Site)" was created to
		e R/W ditch. The existing ditch north of STH 60 will be widened to accomodate the potential for
16		les intersection improvements with a new ditchline proposed at the intersection and where the new ditch section will deter the peak runoff within the drainage basin. A new ditch and culvert is
		utall 10. The increase runoff in drainage basin 11 will be maintained within the existing roadside
		have been analyzed to show no significant increase in headwater in the improved condition. eet flow into large flat wetland areas. No significant change to water surface elevations is
		% increase) and 37 (6% increase) both flow into 30" diameter culverts. No significant change to
		ses. Combined outfalls have been analyzed for 11/12 (7% increase), 17/18 (14% increase), and
		into well defined ditches and will still be maintained within the existing ditch. Furthermore, outfalls is approximately 1 cfs at each location, resulting in no major impacts.
۸		/ 1 Addendum No. 01
	IS THERE A SIGNIFICANT IMPERVIOUS AREA CHANGE	TO ANY SUB BASIN OF THE PROJECT? IF YES, DESCRIBE THE CAUSE OF THE CHANGE AND WHY
17	IT IS NECESSARY.	TO ANY 300 DASIN OF THE PROJECT: IT 123, DESCRIBE THE CROSE OF THE CHANGE AND WIT
		halt shoulder from 3' to 6' for bicycle accomodations. The right turn and bypass lanes are being
10	widened at the intersections to the latest standards to	
19	HAVE THE DRAINAGE SUB BASIN AREAS OR FLOW PAT NECESSARY.	IHS CHANGED SIGNIFICANTLY? IF YES, DESCRIBE THE CAUSE OF THE CHANGE AND WHY IT IS
	No. Drainage flow paths remain consistent with existin	g conditions.
20		
21	DESCRIBE THE PROPOSED DRAINAGE CONVEYANCE A	ND CONTROL SYSTEMS FOR THE PROJECT.
		conveyance of roadside ditches and culvert crossings with new intersection culverts where
22	necessary to meet slope intercept and ditch flow lines.	
23	DESCRIBE THE AQUATIC ORGANISM PASSAGE ISSUES	FOR THE PROJECT, IF ANY.
	N/A.	
24		
25		ER 13 DRAINAGE REQUIREMENTS, EXPLAIN HOW AND WHY.
•	N/A.	
26		
27	DESCRIBE WDNR COORDINATION. PROVIDE NAME OF	F WDNR CONTACT AND DATE, AND ATTACH ANY CORRESPONDENCE.
	Kristina Betzold, WDNR initial letter of concurrence Ap	ril 16, 2012. A copy of the letter is attached.
28		
29	IF THE DRAINAGE DESIGN MEETS LOCAL, MUNICIPAL (OR REGIONAL GUIDELINES THAT EXCEED FDM CHAPTER 13 DRAINAGE REQUIREMENTS,
_3	EXPLAIN HOW AND WHY.	
30	N/A.	
29	IF A SIGNIFICANT IMPACT TO THE PROJECT OCCURS D	UE TO DRAINAGE, PROJECT MANAGER CONCURRENCE IS REQUIRED. (PM SIGN AND DATE)

Project ID: 2310-17-00
Title: STH 60 - Eagle Drive to STH 181
Designer/Checker: JP/RT
DOT Region/Firm Name:
Date: 3/5/2015 Updated 11/26/2019

7	OUTFALL INFORMATION														
8	Outfall number	1	2	3	4	4A	5	6	7	8	8 (Off-Site)	9	10	11	12
9	Outfall discharges to:	Creek	Creek	Creek	Creek	Ditch	Creek	Ditch	Ditch	Overland	Overland	Ditch	Ditch	Ditch	Overland
	Waterway crossing type		Culvert			Culvert	Culvert			Culvert	Culvert				Culvert
11	If discharging to environmentally sensitive area, what kinds of buffers were used at outfall?														
12	Previous flooding issues or flow restrictions?	No	No See Note 3	No	No	No	No	No	No	No	No	No	No	No	No
13	Is the drainageway in the DOT ROW a navigable waterway?	No	No	No	No	No	No	No	No	No	No	No	No	No	No
14	Classify the drainageway in the DOT ROW	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

Outfall number	1	2	3	4	4A	5	6	7	8	8 (Off-Site)	9	10	11	12
Stormwater conveyance type	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale
Outfall station	204+00	211+50	211+50	233+53	244+50	233+53	266+78	266+78	288+98	288+98	288+98	283+53	320+61	320+61
Subbasin starting station	188+60	205+00	205+00	228+00	243+00	228+93	266+78	266+78	274+00	274+00	284+20	277+00	300+01	300+93
Subbasin ending station	205+00	228+93	228+00	243+70	249+00	243+00	274+00	277+00	300+01	300+01	300+93	284+20	322+83	323+19
Proposed roadway length (ft)	1640	2393	2300	1570	600	1407	722	1022	2601	2601	1673	720	2282	2226
Flow conveyance change	None	None	None	None	None	None	None	None	None	None	None	None	None	None
Flood design frequency (yrs)	25	50	25	25	50	50	25	25	50	50	25	25	25	50
Check design frequency (yrs)	50	100	50	50	100	100	50	50	100	100	50	50	50	100
Is the check design storm safely passed?	Yes See Note 2	Yes	Yes See Note 2	Yes See Note 2	Yes	Yes	Yes See Note 2	Yes See Note 2	Yes	Yes	Yes See Note 2	Yes See Note 2	Yes See Note 2	Yes
DOT right-of-way area (acres)	4.49	3.15	3.16	2.16	0.83	1.93	0.85	1.4	3.39	3.39	2.49	0.92	3.18	4.37
Subbasin drainage area (acres)	4.49	3.15	8.45	3	3.87	2.27	0.85	2.8	9.98	25.84	2.54	0.92	6.72	5.06
DOT right-of-way compared to subbasin drainage area (%)	100%	100%	3%	72%	21%	85%	100%	50%	34%	13%	98%	100%	47%	86%
DOT impervious area - existing (acres)	1.38	0.82	0.79	0.72	0.72	0.69	0.25	0.57	1.05	1.05	0.75	0.35	0.90	
DOT impervious area - proposed (acres)	1.74	0.98	0.95	0.87	0.87	0.83	0.30	0.64	1.40	1.40	1.00	0.45	1.20	1.38
Change in impervious area (acres)	0.36	0.16	0.16	0.15	0.15	0.14	0.05	0.07	0.35	0.35	0.25	0.10	0.30	0.28
Percent change in DOT impervious area	26%	20%	20%	21%	21%	20%	20%	12%	33%	33%	33%	29%	33%	25%
Design software used														
Method used to estimate peak flows	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational
Complete lines 36-46 for culverts only														
Existing peak flow (cfs)	8.17	5.61	6.25	5.54	5.88	4.23	2.24	5.64	9.78	19.90	5.72	2.85	7.98	9.19
Proposed peak flow (cfs) (before detention)	8.51	5.74	6.25	5.72	6.07	4.38	2.33	5.80	10.48	20.80	6.48	3.17	8.75	9.67
Proposed peak flow (cfs) (after detention/in-line storage/other)	8.51	5.74	6.25	5.72	6.07	4.38	2.33	5.80	10.48	20.80	6.48	3.17	8.75	9.67
Change in peak flow (cfs)	0.35	0.14	0	0.18	0.18963	0.15	0.10	0.16	0.70	0.90	0.76	0.32	0.77	0.48
Percent change in peak flow	4%	2%	0%	3%	3%	3%	4%	3%	7%	5%	13%	11%	10%	5%
Existing 2-yr peak flow (cfs)	4.22	2.58	3.20	2.87	2.76	2.04	1.18	2.98	4.89	9.95	3.14	1.48	4.12	4.31
Proposed 2-yr peak flow (cfs) (before detention)	4.40	2.65	3.20	2.97	2.85	2.11	1.23	3.07	5.24	10.40	3.56	1.65	4.52	4.53
Proposed 2-yr peak flow (cfs) (after detention/in-line storage/other)	4.40	2.65	3.20	2.97	2.85	2.11	1.23	3.07	5.24	10.40	3.56	1.65	4.52	4.53
Change in 2-yr peak flow (cfs)	0.18	0.06	0.00	0.09	0.09	0.07	0.05	0.08	0.35	0.45	0.42	0.17	0.40	0.23
Percent change in 2-yr peak flow	4%	2%	0%	3%	3%	3%	4%	3%	7%	5%	13%	11%	10%	5%
Existing Tc (min)	25	25	40	10	20	10	12	12	20	20	15	11	26	21
Proposed Tc (min)	25	25	40	10	20	10	12	12	20	20	15	11	26	21
C or CN (existing)	0.47	0.41	0.24	0.31	0.31	0.29	0.47	0.36	0.28	0.22	0.45	0.53	0.31	0.38

¹ Drainage Data

2	Project ID: 2310-17-00
	Title: STH 60 - Eagle Drive to STH 181
4	Designer/Checker: JP/RT
5	DOT Region/Firm Name:
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	·														
	C or CN (proposed)	0.49	0.42	0.24	0.32	0.32	0.3	0.49	0.37	0.3	0.23	0.51	0.59	0.34	0.4
50	Rainfall intensity (in/hr) (rational method only)	3.87	4.34	3.08	5.96	4.9	6.43	5.6	5.6	3.5	3.5	5	5.84	3.83	4.78
51	Rainfall depth used for design storm, if applicable (in)	N/A	N/A	N/A	N/A	N/A	N/A	N/A							

(in)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
2 CHI VERT RESIGN														
CULVERT DESIGN Existing Culvert														
4 Outfall number	1	2	3	4	4A	5	6	7	8	8 (Off-Site)	9	10	11	12
5 Culvert present? (Yes or No)	No	Yes	No	No	Yes	Yes	No	No	Yes	Yes	No	No	No	Yes
Existing culvert shape		Circular			Circular	Box			Circular	Circular				Circular
7 Existing culvert material		RCP			RCP	RC			RCP	RCP				RCP
8 Existing culvert size (ft)		3			2.5	8X6			2	2				3
9 Existing number of culverts		2			1	2			1	1				1
Existing Manning's n		0.013			0.013	0.013			0.013	0.013				0.013
Inlet entrance type		AEW			AEW	Miter to Slope			AEW	AEW				AEW
Inlet loss coefficient (Ke)		0.5			0.5	0.2			0.5	0.5				0.5
Upstream invert (ft)		835.87			841.47	834.45			864.16	864.16				841.21
Downstream invert (ft)		835.74			841.45	833.81			863.8	863.8				840.42
5 Length (ft)		72.4			63.6	64			85.9	85.9				72.9
Slope (%)	#DIV/0!	0.18%	#DIV/0!	#DIV/0!	0.03%	1.00%	#DIV/0!	#DIV/0!	0.42%	0.42%	#DIV/0!	#DIV/0	! #DIV/0!	1.08%
Floodplain Management														
Is culvert in a mapped floodplain?		Yes			No	No			No	No				No
Will proposed culvert increase water surface														
profile?		No			Yes See Note 1	No			Yes See Note 1	Yes See Note 1				Yes See Note 1
Drainage District Issues														
Is culvert in a drainage district?		Yes			No	No			No	No				No
		Jackson-												
2 Drainage District Name		Germantown												
Will proposed culvert raise the culvert invert or														
increase water surface profile?		No			Yes See Note 1	No			Yes See Note 1	Yes See Note 1				Yes See Note 1
Has drainage board approved increases?														
Aquatic Organism Passage														
Is aquatic organism passage a concern?		No			No	No			No	No				No
Does WDNR agree with AOP design?		Exist to Remain			Exist to Remain	Exist to Remain			Exist to Remain	Exist to Remain				Exist to Remain
Proposed Culvert Design														
9 Design ADT		>7500			>7500	>7500			>7500	>7500				>7500
Design flow		5.74			6.07	4.38			10.48	20.80				9.67
Design year frequency		50			50	50			50	50				50
2 Hydrological method used		Rational			Rational	Rational			Rational	Rational				Rational
Assumed tailwater condition		None			None	None			None	None				None
Maximum allowable headwater														
5														
Maximum allowable headwater design criteria	DDMenu	Top of Subgrade		DDMenu		Top of Subgrade		DDMenu	Top of Subgrade	Top of Subgrade		DDMenu	DDMenu	Top of Subgrade
Proposed culvert shape		Circular	DD Menu	DD Menu		Box	DD Menu	DD Menu	Circular	Circular		DD Menu	DD Menu	Circular
Proposed culvert material		RCP	DD Menu			RC	DD Menu	DD Menu	RCP	RCP	RCP	DD Menu	DD Menu	RCP
Proposed culvert size		3			2.5	8X6			2	2			<u> </u>	3
Proposed number of culverts		2			1	2			1	1			<u> </u>	1
Manning's n		0.013				0.013			0.013	0.013				0.013
Type of endwalls		AEW	DD Menu	DD Menu	AEW	Miter to Slope	DD Menu	DD Menu	AEW	AEW		DD Menu	DD Menu	AEW

2	Project ID: 2310-17-00														
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	DOT Region/Firm Name:														
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92	Inlet loss coefficient (Ke)	0.5				0.5	0.2			0.5	0.5				0.5
93	Proposed upstream invert (ft)	835	.87			841.47	834.45			864.16	864.16				841.21
94	Proposed downstream invert (ft)	835	.74			841.45	833.81			863.8	863.8				840.42
95	Proposed length (ft)	72.4				63.6	64			85.9	85.9				72.9
96	Proposed slope (%)	#DIV/0!	0.18%	#DIV/0!	#DIV/0!	0.03%	6 1.00%	#DIV/0!	#DIV/0!	0.42%	0	#DIV/0!	#DIV/0!	#DIV/0!	1.08%
97	Embedment depth (ft)	N/A				N/A	N/A			N/A	N/A				N/A
98	Embedment material	N/A				N/A	N/A			N/A	N/A				N/A
99	Discharge velocity (ft/s)	0.6	5			1.14	0.11			4.13	6.94				1.91
100	Riprap outfall (Size riprap or None)	Nor	ne			None	None			None	None				None
101	Station of lowest subgrade shoulder point in														
101	subbasin (0+00)	211	+50			249+00	233+53			288+98	288+98				320+61
102	Elevation of lowest subgrade shoulder point in														
102	subbasin (ft)	841	.94			846.34	842.63			870.38	870.38				847.29
103	Headwater distance below subgrade shoulder														
103	point (ft)	5.3	7			3.75	5.75			4.54	3.45				4.75
104	Headwater to pipe diameter ratio	0.4	1			0.45	0.4			0.84	1.38				0.44
105	Design software used	**H	ydraflow			Hydraflow	Hydraflow			Hydraflow	Hydraflow				Hydraflow
106	Proposed tailwater condition	N/A				N/A	N/A			N/A	N/A				N/A
107	Discharge pipe end submerged?	No				No	No			No	No				No
108	Assumed tailwater elevation (ft)	835	.74			841.45	833.81			863.8	863.8				840.42

Enter Line Number and Note. Add more boxes if necessary

Note 1: Per Hyraflow calculation summary. Water surface increase as follows: 2 - 0.00', 4A - 0.02', 5 - 0.0', 8 - 0.07', 8 (Off-Site) - 0.12', 12 - 0.03', 14 - 0.03', 18 - 0.13', 24 - 0.03', 26 - 0.0', 33A - 0.05', 33B - 0.04', 35 - 0.03', 37 - 0.0'

Note 2: Standard ditch section was evaluated at minimum 1% slope. Two drainage sheds exceeded maximum flow in the minimum slope analysis. Basin 25 contains equivalent drainage shed from east and west and therefore combined flow can be maintained in the existing ditch section either side of the outfall. Basin 33 includes a ditch section near the outfall which exceed 2' in depth and therefore has the additional capacity to handle the increase in peak flow.

Note 3: It was noted in the PIM by adjacent property owner that there is a backup of water in their property (upstream) from this culvert. Department maintenance and inspection reports do not indicate need for repair or replacement. Topo survey identifies the low area is outside the DOT Right of Way and sufficient roadside ditch section is provided directing roadway runoff to the culvert.

**Hydraflow - Civil 3D Add On

Culvert 33 Hw/D ratio exceeds 1.5.

In OPM, Town of Cedarburg indicated a concern with a culvert between Horns Corners and STH 181. They felt it was undersized and therefore the reason for the backup. Per the analysis completed for for two cross culverts at outfall 35 and 37, there does not appear to be a capacity issue in these locations.

Project ID: 2310-17-00
Title: STH 60 - Eagle Drive to STH 181
Designer/Checker: JP/RT
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7	OUTFALL INFORMATION														
8	Outfall number	13	14	15	16	17	18	19	20	21	22	23	24	25	26
9	Outfall discharges to:	Creek	Creek	Overland	Overland	Creek	Creek	Ditch	Ditch	Ditch	Ditch	Creek	Creek	Creek	Creek
	Waterway crossing type		Culvert				Culvert						Culvert		Culvert
11	If discharging to environmentally sensitive area, what kinds of buffers were used at outfall?														
12	Previous flooding issues or flow restrictions?	No	No	No	No	No	No	No	No	No	No	No	No	No	No
13	Is the drainageway in the DOT ROW a navigable waterway?	No	No	No	No	No	No	No	No	No	No	No	No	No	No
14	Classify the drainageway in the DOT ROW	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

Outfall number	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Stormwater conveyance type	Ditch/Swale	Ditch/Swale			Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale
Outfall station	327+65	327+65			356+55	356+55	363+02	363+02	363+68	363+68	378+47	378+47	397+95	397+95
Subbasin starting station	322+83	323+19	337+02	347+19	351+53	350+28	357+44	358+29	363+68	363+45	365+99	365+99	389+75	389+75
Subbasin ending station	337+02	350+38	347+19	351+53	357+44	357+40	363+02	363+02	365+99	365+99	389+75	389+75	446+84	409+31
Proposed roadway length (ft)	1419	2719	1017	434	591	712	558	473	231	254	2376	2376	5709	1950
Flow conveyance change	None	None	None	None	None	None	None	None	None	None	None	None	None	None
Flood design frequency (yrs)	25	50	50	50	25	50	25	25	25	25	25	50	25	50
Check design frequency (yrs)	50	100	100	100	50	100	50	50	50	50	50	100	50	100
Is the check design storm safely passed?	Yes See Note 2	Yes See Note 2	N/A	N/A	Yes See Note 2	Yes	Yes See Note 2	Yes	Yes See Note 2	Yes				
DOT right-of-way area (acres)	1.85	3.61	1.27	0.74	0.85	1.23	0.96	0.92	0.42	0.42	2.81	3	7.47	2.5
Subbasin drainage area (acres)	2.1	7.06	1.27	0.76	1.47	1.89	1.02	1.06	0.42	0.74	3.28	3.3	10.1	2.6
DOT right-of-way compared to subbasin drainage area (%)	88%	51%	100%	97%	58%	65%	94%	87%	100%	57%	86%	91%	74%	96%
DOT impervious area - existing (acres)	0.49	0.94	0.35	0.28	0.24	0.38	0.34	0.37	0.34	0.17	0.81	0.81	2.30	0.75
DOT impervious area - proposed (acres)	0.59	1.12	0.42	0.31	0.30	0.59			0.35	0.52	0.98	0.98	2.80	0.95
Change in impervious area (acres)	0.10	0.18	0.07	0.03	0.06	0.21	0.03	0.11	0.01	0.35	0.17	0.17	0.50	0.20
Percent change in DOT impervious area	20%	19%	20%	11%	25%	55%	9%	30%	3%	206%	21%	21%	22%	27%
Design software used														
Method used to estimate peak flows	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational
Complete lines 36-46 for culverts only														
Existing peak flow (cfs)	4.50	7.45	3.25	2.82	3.41	5.06	2.41	2.84	2.64	2.23	5.90	6.23	13.08	5.40
Proposed peak flow (cfs) (before detention)	4.73	7.71	3.41	2.94	3.51	6.18	2.46	3.12	2.70	2.34	6.19	6.55	13.79	5.78
Proposed peak flow (cfs) (after detention/in-line storage/other)	4.73	7.71	3.41	2.94	3.51	6.18				2.34	6.19	6.55	13.79	5.78
Change in peak flow (cfs)	0.23	0.26	0.15	0.11	0.10	1.12			0.06	0.11	0.29	0.32	0.71	0.38
Percent change in peak flow	5%	3%	5%	4%	3%	22%	2%	10%	2%	5%	5%	5%	5%	7%
Existing 2-yr peak flow (cfs)	2.42	3.79	1.59	1.39	1.83	2.33	1.30	1.53	1.45	1.22	3.17	2.92	6.54	2.54
Proposed 2-yr peak flow (cfs) (before detention)	2.54	3.92	1.67	1.45	1.88	2.84	1.33	1.68	1.48	1.28	3.33	3.07	6.89	2.7
Proposed 2-yr peak flow (cfs) (after detention/in-line storage/other)	2.54	3.92	1.67	1.45	1.88	2.84	1.33	1.68	1.48	1.28	3.33	3.07	6.89	2.71
Change in 2-yr peak flow (cfs)	0.12	0.13	0.07	0.06	0.05	0.52	0.03	0.15	0.03	0.06	0.15	0.15	0.35	0.18
Percent change in 2-yr peak flow	5%	3%	5%	4%	3%	22%	2%	10%	2%	5%	5%	5%	5%	7%
Existing Tc (min)	13	28	13	7	7	8	14	13	5	6	19	20	30	20
Proposed Tc (min)	13	28	13	7	7	8	14	13	5	6	19	20	30	20
C or CN (existing)	0.4	0.29	0.43	0.5	0.34	0.36	0.45	0.5	0.84	0.41	0.41	0.39	0.37	0.43

¹ Drainage Data

2	Project ID: 2310-17-00
3	Title: STH 60 - Eagle Drive to STH 181
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49	C or CN (proposed)	0.42	0.3	0.45	0.52	0.35	0.44	0.46	0.55	0.86	0.43	0.43	0.41	0.39	0.46
50	Rainfall intensity (in/hr) (rational method only)	5.36	3.64	5.96	7.43	6.82	7.43	5.24	5.36	7.47	7.35	4.39	4.84	3.5	4.83
51	Rainfall depth used for design storm, if applicable	N/A	N/A	N/A	N/A	N/A	N/A	N/Δ	N/A	N/A	N/Δ	N/A	N/A	N/A	N/A

(in)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
CULVERT DESIGN														
Existing Culvert														
Outfall number	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Culvert present? (Yes or No)	No	Yes	No	No	No	Yes	No	No	No	No	No	Yes	No	Yes
Existing culvert shape		Circular		DD Menu		Circular						Circular		Box
Existing culvert material		RCP		DD Menu		RCP						RCP		RC
Existing culvert size (ft)		2				2						3		8X5
Existing number of culverts		1				1						1		2
Existing Manning's n		0.013				0.013						0.013		0.013
Inlet entrance type		AEW		DD Menu		AEW						AEW		Miter to Slope
Inlet loss coefficient (Ke)		0.5				0.5						0.5		0.2
Upstream invert (ft)		840.6				855.91						850.98		850.14
Downstream invert (ft)		839.64				854.8						850.29		849.32
Length (ft)		73.7				109.3						86.9		56
Slope (%)	#DIV/0!	1.30%	#DIV/0!	#DIV/0!	#DIV/0!	1.02%	#DIV/0!	#DIV/0	! #DIV/0!	! #DIV/0!	#DIV/0!	. 0.79%	6 #DIV/0!	1.46
Floodplain Management														
Is culvert in a mapped floodplain?		No				No						No		Yes
Will proposed culvert increase water surface														1
profile?		Yes See Note 1		Yes See Note 1		Yes See Note 1						Yes See Note 1		No
Drainage District Issues														
Is culvert in a drainage district?		No		No		No						No		No
Drainage District Name														
Will proposed culvert raise the culvert invert or														
increase water surface profile?		Yes See Note 1		Yes See Note 1		Yes See Note 1						Yes See Note 1		No
Has drainage board approved increases?														
Aquatic Organism Passage														
Is aquatic organism passage a concern?		No		No		No						No		No
Does WDNR agree with AOP design?		Exist to Remain		Exist to Remain		Exist to Remain						Exist to Remain		Exist to Remai
Proposed Culvert Design														
Design ADT		>7500		>7500		>7500						>7500		>7500
Design flow		7.71		2.94		6.18						6.55		5.78
Design year frequency		50		50		50						50		50
Hydrological method used		Rational		Rational		Rational						Rational		Rational
Assumed tailwater condition		None		None		None						None		None
Maximum allowable headwater														
Maximum allowable be advictor design with the	2014	T . (0)	DDM	DDM	2014	T . (0)	DDM	DDM	DDM	DDM	DDM	T . (C)	DDM	T . (0)
Maximum allowable headwater design criteria		Top of Subgrade		DDMenu	DDMenu		DDMenu	DDMenu	DDMenu	DDMenu	DDMenu	, , , , , , , , , , , , , , , , , , ,		Top of Subgra
Proposed culvert shape	DD Menu	Circular	DD Menu	DD Menu	DD Menu	Circular	DD Menu	DD Menu	DD Menu	DD Menu	DD Menu	Circular	DD Menu	Box
Proposed culvert material	DD Menu	RCP	DD Menu	DD Menu	DD Menu	RCP	DD Menu	DD Menu	DD Menu	DD Menu	DD Menu	RCP	DD Menu	RC OVE
Proposed culvert size		2	1			4	+		1	1	1	3		8X5
Proposed number of culverts		0.040	1			0.040	+		1	1	1	0.040		2
Manning's n		0.013				0.013			 	 		0.013	1	0.013
Type of endwalls	DD Menu	AEW	DD Menu	DD Menu	DD Menu	AEW	DD Menu	DD Menu	DD Menu	DD Menu	DD Menu	AEW	DD Menu	Miter to Slope

2	Project ID: 2310-17-00														
3	Title: STH 60 - Eagle Drive to STH 181														
4	Designer/Checker: JP/RT														
	DOT Region/Firm Name:														
6	Date: 3/5/2015 Updated 11/26/2019														
92	Inlet loss coefficient (Ke)		0.5			0	.5						0.5		0.2
93	Proposed upstream invert (ft)		840.6			8	55.91						850.98		850.14
94	Proposed downstream invert (ft)		839.64				54.8						850.29		849.32
95	Proposed length (ft)		73.7				09.3						86.9		56
96	Proposed slope (%)	#DIV/0!	1.30%	#DIV/0!	#DIV/0!	#DIV/0!	1.02%	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	0.79%	#DIV/0!	1.46%
97	Embedment depth (ft)		N/A				/A						N/A		N/A
98	Embedment material		N/A				/A						N/A		N/A
99	Discharge velocity (ft/s)		3.26			2	.27						1.36		0.14
100	Riprap outfall (Size riprap or None)		None			N	lone						None		None
101	Station of lowest subgrade shoulder point in														
101	subbasin (0+00)		327+65			3	56+55						378+47		397+95
102	Elevation of lowest subgrade shoulder point in														
102	subbasin (ft)		846.05			8	65.46						858.3		856.6
103	Headwater distance below subgrade shoulder														
100	point (ft)		4.06			8	.46						6.24		4.7
104	Headwater to pipe diameter ratio		0.69			0	.55						0.36		0.35
105	Design software used		Hydraflow			F	lydraflow						Hydraflow		Hydraflow
106	Proposed tailwater condition		N/A			N	/A						N/A		N/A
107	Discharge pipe end submerged?		No			N	0						No		No
108	Assumed tailwater elevation (ft)		839.64			8	54.8						850.29		849.32

Enter Line Number and Note. Add more boxes if necessary

Note 1: Per Hyraflow calculation summary. Water surface increase as foll 35 - 0.03', 37 - 0.0'

Note 2: Standard ditch section was evaluated at minimum 1% slope. Two and therefore combined flow can be maintained in the existing ditch section capacity to handle the increase in peak flow.

Note 3: It was noted in the PIM by adjacent property owner that there is a repair or replacement. Topo survey identifes the low area is outside the E

**Hydraflow - Civil 3D Add On

Culvert 33 Hw/D ratio exceeds 1.5.

In OPM, Town of Cedarburg indicated a concern with a culvert between H cross culverts at outfall 35 and 37, there does not appear to be a capacity

Project ID: 2310-17-00
Title: STH 60 - Eagle Drive to STH 181
Designer/Checker: JP/RT
DOT Region/Firm Name:
Date: 3/5/2015 Updated 11/26/2019

7	OUTFALL INFORMATION														
8	Outfall number	27	28	29	30	31	32	33A	33B	34	35	36	37	2/3	4/5
9	Outfall discharges to:	Wetland	Ditch	Ditch	Wetland	Wetland	Overland	Overland	Overland	Wetland	Wetland	Creek	Creek	Creek	Creek
	Waterway crossing type							Culvert	Culvert		Culvert		Culvert		
11	If discharging to environmentally sensitive area, what kinds of buffers were used at outfall?														
12	Previous flooding issues or flow restrictions?	No	No	No	No	No	No	No	No	No	No	No	No	No	No
1.0	Is the drainageway in the DOT ROW a navigable waterway?	No	No	No	No	No	No	No	No	No	No	No	No	No	No
14	Classify the drainageway in the DOT ROW	N/A	N/A	N/A	Wetland	Wetland	N/A	N/A	N/A	Wetland	Wetland	N/A	N/A	N/A	N/A

Outfall number	27	28	29	30	31	32	33A	33B	34	35	36	37	2/3	4/5
Stormwater conveyance type	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Overland	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale [Ditch/Swale
Outfall station		452+40	456+37		483+87	N/A	500+76	510+83	530+97	530+97	550+50	552+45	211+50	233+53
Subbasin starting station	409+31	446+84	446+84	474+06	474+06	497+91	485+30	502+29	524+28	522+39	536+00	536+00	205+00	228+00
Subbasin ending station	446+84	456+50	456+50	497+91	485+30	524+28	502+29	522+39	536+00	536+00	555+40	555+40	228+93	243+70
Proposed roadway length (ft)	3753	966	966	2385	1124	2637	1699	2010	1172	1361	1940	1940	2393	1570
Flow conveyance change	None	None	None	None	None	None	None	None	None	None	None	None	None	None
Flood design frequency (yrs)	25	25	25	25	25	25	50	50	25	50	25	50	25	25
Check design frequency (yrs)	50	50	50	50	50	50	100	100	50	100	50	100	50	50
Is the check design storm safely passed?	Yes See Note 2	N/A	Yes	Yes	Yes See Note 2	Yes	Yes See Note 2	Yes	Yes	Yes				
DOT right-of-way area (acres)	4.38	1.09	1.02	2.69	1.22	3.32	3.66	2.72	1.58	2	2.58	2.71	6.31	4.09
Subbasin drainage area (acres)	13.07	1.33	1.33	3.3	1.88	3.68	13.74	10.18	1.61	2.31	2.58	3.92	11.6	5.27
DOT right-of-way compared to subbasin drainage area (%)	34%	82%	77%	82%	65%	90%	27%	27%	98%	87%	100%	69%	54%	78%
DOT impervious area - existing (acres)	1.29	0.33	0.33	0.92	0.39				0.40	0.47	0.96		1.61	1.41
DOT impervious area - proposed (acres)	1.55	0.39	0.55	1.12	0.46				0.54	0.64	1.21	0.82	1.93	1.70
Change in impervious area (acres)	0.26	0.06	0.22	0.20	0.07	0.20	0.21	0.15	0.14	0.17	0.25	0.15	0.32	0.29
Percent change in DOT impervious area	20%	18%	67%	22%	18%	13%	17%	16%	35%	36%	26%	22%	20%	21%
Design software used														
Method used to estimate peak flows	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational	Rational
Complete lines 36-46 for culverts only														
Existing peak flow (cfs)	10.06	3.02	3.02	8.32	3.15	7.83	15.32	15.39	2.91	4.99	4.88	7.44	10.22	9.47
Proposed peak flow (cfs) (before detention)	10.06	3.18	3.18	8.70	3.23				3.19	5.51	5.35			9.78
Proposed peak flow (cfs) (after detention/in-line storage/other)	10.06	3.18	3.18	8.70	3.23					5.51	5.35	7.86	10.32	9.78
Change in peak flow (cfs)	0.00	0.16	0.16	0.38	0.08	0.28	0.57	0.57	0.27	0.52	0.47	0.42	0.10	0.31
Percent change in peak flow	0%	5%	5%	5%	3%	4%	4%	4%	9%	11%	10%	6%	1%	3%
Existing 2-yr peak flow (cfs)	5.31	1.60	1.60	4.36	1.69	4.05	7.35	7.78	1.55	2.53	2.48	4.01	5.24	4.91
Proposed 2-yr peak flow (cfs) (before detention)	5.31	1.68	1.68	4.55	1.73		7.62		1.70	2.79	2.72	4.24	5.29	5.07
Proposed 2-yr peak flow (cfs) (after detention/in-line storage/other)	5.31	1.68	1.68	4.55	1.73	4.20	7.62	8.07	1.70	2.79	2.72	4.24	5.29	5.07
Change in 2-yr peak flow (cfs)	0.00	0.08	0.08	0.20	0.04	0.15	0.27	0.07	0.14	0.27	0.24	0.23	0.05	0.16
Percent change in 2-yr peak flow	0.00	5%	5%	5%	3%	0.15 4%	4%	4%	9%	11%	10%	6%	1%	3%
Existing Tc (min)	50	10	10	11	20	25	26	14	21	13	28	13	40	10
Proposed Tc (min)	50	10	10	11	20	25	26	14	21	13	28	13	40	10
C or CN (existing)	0.28	0.39	0.39	1.1	20	0.55	20	14	۷ ا	13	20	13	40	0.30

Project ID: 2310-17-00
Title: STH 60 - Eagle Drive to STH 181
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49 C	or CN (proposed)	0.00		_											
	or CN (proposed)	0.28	0.41	0.41	0.46	0.4	0.57	0.28	0.28	§ 0.47	0.42	0.57	0.37 🕻	0.29	0.31
50 R	tainfall intensity (in/hr) (rational method only)	2.75	5.83	5.83	5.73	4.3	3.87	4.13	5.6	4.21	5.68	3.64	5.42	3.08	5.96
	tainfall depth used for design storm, if applicable														
(ir	n)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
	CULVERT DESIGN														
53 E	xisting Culvert														
54 O	Outfall number	27	28	29	30	31	32	33A	33B	34	35	36	37	2/3	4/5
55 C	culvert present? (Yes or No)	No	No	No	No	No	No	Yes	Yes	No	Yes	No	Yes		
56 E	xisting culvert shape							Circular	Circular		Circular		Elliptical		
57 E	xisting culvert material							CMP	CMP		CMP		CMP		
58 E	xisting culvert size (ft)							2.5	2.5		2.5		3.5X5.5		
59 E	xisting number of culverts							1	1		1		1		
60 E	xisting Manning's n							0.024	0.024		0.024		0.024		
61 I n	nlet entrance type							AEW	AEW		AEW		AEW		
	nlet loss coefficient (Ke)							0.5	0.5		0.5		0.5		
	lpstream invert (ft)								866.65		870.6		863.23		
64 D	Pownstream invert (ft)								865.5		870.01		863.13		
	ength (ft)							73.6	80		107.3		106.7		
	lope (%)	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	0.29%		#DIV/0!		#DIV/0!	0.09%	#DIV/0!	#DIV/0!
	Toodplain Management	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	772.070	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.2070		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.0070	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.0076	,,,,,,,,	,,,,,,,,
	s culvert in a mapped floodplain?							No	No		No		No		
W	Vill proposed culvert increase water surface														
69 pi	rofile?							Yes See Note 1	Yes See Note 1		Yes See Note 1		No		
70 D	Prainage District Issues														
71 I s	s culvert in a drainage district?							No	No		No		No		
70															
72 D	rainage District Name														
73 W	Vill proposed culvert raise the culvert invert or														
in	ncrease water surface profile?							Yes See Note 1	Yes See Note 1		Yes See Note 1		No		
74 H	las drainage board approved increases?														
75 A	Aquatic Organism Passage														
76 Is	aquatic organism passage a concern?							No	No		No		No		
77 D	oes WDNR agree with AOP design?							Exist to Remain	Exist to Remain		Exist to Remain		Exist to Remain		
78 P	roposed Culvert Design														
_	Design ADT							>7500	>7500		>7500		>7500		
	Design flow								15.96		5.513		7.86		
	Design year frequency								50		50		50		
	lydrological method used								Rational		Rational		Rational		
	Assumed tailwater condition		1						None		None		None		
			1		1					1	877.26				
ÿ. <u>IN</u>	Maximum allowable headwater		-					873.36	870.06		011.20		869.46	+	
85 N	Maximum allowable headwater design criteria	DDMenu	DDMenu	DDMenu	DDMenu	DDMenu	DDMenu	Top of Subgrade	Top of Subgrade	DDMenu	Top of Subgrade	DDMenu	DDMenu		
	<u> </u>		DD Menu	DD Menu		DD Menu	DD Menu		Circular	DD Menu			Elliptical		
	•		DD Menu			DD Menu	DD Menu		CMP				CMP		
	Proposed culvert material	U IVIOITU	DD MIGHU	JD Mellu	DD WIGHT	DD WIGHT	DD WIGHT		2.5		2.5		3.5X5.5		
	Proposed number of culverts							1	1		1		1		
_	Manning's n							0.024	0.024		0.024		0.024		
		DD Menu	DD Menu	DD Menu	DD Menu	DD Menu	DD Menu								
91 T	ype of endwalls	DD Menu	DD Menu	DD Menu	DD Menu	DD Menu	DD Menu	AEW	AEW	DD Menu	AEW	DD Menu	AEW		

	Project ID: 2310-17-00														
	Title: STH 60 - Eagle Drive to STH 181														
	Designer/Checker: JP/RT														
	DOT Region/Firm Name:														
6	Date: 3/5/2015 Updated 11/26/2019														
92	Inlet loss coefficient (Ke)							0.5	0.5		0.5		0.5		
93	Proposed upstream invert (ft)							869.25	866.65		870.6		863.23		
	Proposed downstream invert (ft)							869.04	865.5		870.01		863.13		
95	Proposed length (ft)							73.6	80		107.3		106.7		
96	Proposed slope (%)	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	0.29%	1.44%	#DIV/0!	0.55%	#DIV/0!	0.09%	#DIV/0!	#DIV/0!
97	Embedment depth (ft)								N/A		N/A		N/A		
98	Embedment material							N/A	N/A	~	N/A	~	N/A		
99	Discharge velocity (ft/s)							3.92	3.94		1.62 }	ξ.	0.81 }		
100	Riprap outfall (Size riprap or None)							None	None	5	None	3	None		
101	Station of lowest subgrade shoulder point in														
101	subbasin (0+00)							500+76	511+10		530+97		552+39		
102	Elevation of lowest subgrade shoulder point in														
102	subbasin (ft)							873.36	870.06		878.21		870.35		
103	Headwater distance below subgrade shoulder										und	>	uud		
100	point (ft)							2.08	1.36	بد	5.96 \$	ξ.	4.66 \$		
104	Headwater to pipe diameter ratio								0.82	نید	0.44	ξ.	0.56		
105	Design software used							Hydraflow	Hydraflow)	Hydraflow	~	Hydraflow		
106	Proposed tailwater condition							N/A	N/A		N/A		N/A		
107	Discharge pipe end submerged?							No	No		No		No		
108	Assumed tailwater elevation (ft)							869.04	865.5		870.01		863.13		

Enter Line Number and Note. Add more boxes if necessary

Note 1: Per Hyraflow calculation summary. Water surface increase as foll 35 - 0.03', 37 - 0.0'

Note 2: Standard ditch section was evaluated at minimum 1% slope. Two and therefore combined flow can be maintained in the existing ditch section capacity to handle the increase in peak flow.

Note 3: It was noted in the PIM by adjacent property owner that there is a repair or replacement. Topo survey identifes the low area is outside the E

**Hydraflow - Civil 3D Add On

Culvert 33 Hw/D ratio exceeds 1.5.

In OPM, Town of Cedarburg indicated a concern with a culvert between H cross culverts at outfall 35 and 37, there does not appear to be a capacity



	Project ID: 2310-17-00
	Title: STH 60 - Eagle Drive to STH 181
4	Designer/Checker: JP/RT
5	DOT Region/Firm Name:
6	Date: 3/5/2015 Updated 11/26/2019

7	OUTFALL INFORMATION					
8	Outfall number	11/12	13/14	17/18	23/24	25/26
9	Outfall discharges to:	Ditch	Creek	Creek	Creek	Creek
	Waterway crossing type					
11	If discharging to environmentally sensitive area, what kinds of buffers were used at outfall?					
12	Previous flooding issues or flow restrictions?	No	No	No	No	No
	Is the drainageway in the DOT ROW a navigable waterway?	No	No	No	No	No
14	Classify the drainageway in the DOT ROW	N/A	N/A	N/A	N/A	N/A

15	BASIC SUB BASIN DRAINAGE INFORMATIO					
16	Outfall number	11/12	13/14	17/18	23/24	25/26
17	Stormwater conveyance type	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale	Ditch/Swale
18	Outfall station	320+61	327+65	356+55	378+47	397+95
19	Subbasin starting station	300+01	322+83	350+28	365+99	389+75
20	Subbasin ending station	323+19	350+38	357+44	389+75	446+84
21	Proposed roadway length (ft)	2318	2755	716	2376	5709
22	Flow conveyance change	None	None	None	None	None
23	Flood design frequency (yrs)	25	25	25	25	25
24	Check design frequency (yrs)	50	50	50	50	50
25	Is the check design storm safely passed?	Yes	Yes	Yes	Yes	Yes
26	DOT right-of-way area (acres)	7.55	5.46	2.08	5.81	9.97
27	Subbasin drainage area (acres)	11.78	9.16	3.36	6.58	12.7
28	DOT right-of-way compared to subbasin drainage					
20	area (%)	64%	60%	62%	88%	79%
29	DOT impervious area - existing (acres)	2.00	1.43	0.72	1.62	3.05
30	DOT impervious area - proposed (acres)	2.58	1.71	0.96	1.96	3.75
31	Change in impervious area (acres)	0.58	0.28	0.24	0.34	0.70
32	Percent change in DOT impervious area	29%	20%	33%	21%	23%
33	Design software used					
34	Method used to estimate peak flows	Rational	Rational	Rational	Rational	Rational
35	Complete lines 36-46 for culverts only					
36	Existing peak flow (cfs)	15.34	10.51	7.55	11.05	16.99
37	Proposed peak flow (cfs) (before detention)	16.50	10.92	8.62	11.61	17.97
38	Proposed peak flow (cfs) (after detention/in-line storage/other)	16.50	10.92	8.62	11.61	17.97
39	Change in peak flow (cfs)	1.16	0.41	1.06		0.98
40	Percent change in peak flow	8%	4%	14%	5%	6%
41	Existing 2-yr peak flow (cfs)	7.93	5.34	4.04	5.97	8.50
42	Proposed 2-yr peak flow (cfs) (before detention)	8.53	5.55	4.60	6.27	8.99
40	Proposed 2-yr peak flow (cfs) (after detention/in-line					
43	storage/other)	8.53	5.55	4.60	6.27	8.99
44	Change in 2-yr peak flow (cfs)	0.60	0.21	0.57	0.30	0.49
45	Percent change in 2-yr peak flow	8%	4%	14%	5%	6%
46	Existing Tc (min)	26	28	8	20	30
47	Proposed Tc (min)	26	28	8	20	30
48	C or CN (existing)	0.34	0.32	0.35	0.40	0.38

¹ Drainage Data

	Project ID: 2310-17-00
	Title: STH 60 - Eagle Drive to STH 181
4	Designer/Checker: JP/RT
5	DOT Region/Firm Name:
6	Date: 3/5/2015 Updated 11/26/2019

49	C or CN (proposed)	0.37	0.33	0.40	0.42	0.40
50	Rainfall intensity (in/hr) (rational method only)	3.83	3.64	6.4	4.2	3.5
51	Rainfall depth used for design storm, if applicable (in)	N/A	N/A	N/A	N/A	N/A

52	CULVERT DESIGN					
	Existing Culvert					
	Outfall number	11/12	13/14	17/18	23/24	25/26
	Culvert present? (Yes or No)		,		20/21	20,20
	Existing culvert shape					
	Existing culvert material					
58	Existing culvert size (ft)					
59	Existing number of culverts					
	Existing Manning's n					
	Inlet entrance type					
	Inlet loss coefficient (Ke)					
63	Upstream invert (ft)					
64	Downstream invert (ft)					
65	Length (ft)					
	Slope (%)	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
67	Floodplain Management					
68	Is culvert in a mapped floodplain?					
	Will proposed culvert increase water surface					
	profile?					
	Drainage District Issues					
71	Is culvert in a drainage district?					
	Drainage District Name					
	Will proposed culvert raise the culvert invert or					
	increase water surface profile?					
	Has drainage board approved increases?					
	Aquatic Organism Passage					
	Is aquatic organism passage a concern?					
	Does WDNR agree with AOP design?					
	Proposed Culvert Design					
	Design ADT					
	Design flow					
	Design year frequency					
	Hydrological method used					
83	Assumed tailwater condition					
84	Maximum allowable headwater					
	Maximum allowable headwater design criteria					
	Proposed culvert shape					
	Proposed culvert material					
	Proposed culvert size					
	Proposed number of culverts					
	Manning's n					
91	Type of endwalls					

Drainage Data Project ID: 2310-17-00

2	Project ID: 2310-17-00					
3	Title: STH 60 - Eagle Drive to STH 181					
4	Designer/Checker: JP/RT					
5	DOT Region/Firm Name:					
6	Date: 3/5/2015 Updated 11/26/2019					
92	Inlet loss coefficient (Ke)					
93	Proposed upstream invert (ft)					
94	Proposed downstream invert (ft)					
95	Proposed length (ft)					
96	Proposed slope (%)	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
97	Embedment depth (ft)					
98	Embedment material					
99	Discharge velocity (ft/s)					
100	Riprap outfall (Size riprap or None)					
101	Station of lowest subgrade shoulder point in					
101	subbasin (0+00)					
102	Elevation of lowest subgrade shoulder point in					
102	subbasin (ft)					
103	Headwater distance below subgrade shoulder					
100	point (ft)					
104	Headwater to pipe diameter ratio					
105	Design software used					
106	Proposed tailwater condition					
107	Discharge pipe end submerged?					
108	Assumed tailwater elevation (ft)					

Enter Line Number and Note. Add more boxes if necessary

Note 1: Per Hyraflow calculation summary. Water surface increase as foll 35 - 0.03', 37 - 0.0'

Note 2: Standard ditch section was evaluated at minimum 1% slope. Two and therefore combined flow can be maintained in the existing ditch section capacity to handle the increase in peak flow.

Note 3: It was noted in the PIM by adjacent property owner that there is a repair or replacement. Topo survey identifes the low area is outside the E

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Culvert 33 Hw/D ratio exceeds 1.5.

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- **Project Summary**
- Project ID: 2310-17-00
- Title: STH 60 Eagle Drive to STH 181
- Designer/Checker: JP/RT
- DOT Region/Firm Name: SE/COLLINS ENGINEERS, INC. Date: 3/5/2015 Updated 11/26/2019

14	Water Quality Results	Total Project	Grass	Filter	Wet	Catch-	Street	Diefikens	Other	Untreated		
	Water Quality Results Dis	cussion										
13	DESIGN STAGE	Final Design	Stage									
12	PS&E DATE:	May 1, 2019										
11	PROJECT MANAGER:	NGUYEN LY	NGUYEN LY									
10	DESCRIPTION OF WORK:	RESURFACIN	G AND INTE	RSECTION I	MPROVEME	NTS						
9	COUNTY:	WASHINGTO	N & OZAUK	EE.								
8	LIMITS:	EAGLE DRIVE	EAGLE DRIVE TO STH 181									
7	HIGHWAY:	STH 60	STH 60									

Detention Drainage Swales Strips basins Cleaning Devices Areas Summary Ponds Basin Area 15 Orainage Area (ac) 16 ROW Drainage Area (ac) 17 Percent TSS Reduction by Treatement Type Project Water Quality Objectives ▼ HE PROJECT IS EXEMPT FROM TRANS 401 STORMWATER QUALITY REQUIREMENTS AND REQUIRES NO FURTHER WATER QUALITY INFORMATION. 18 DESCRIBE BELOW WHY IT IS EXEMPT. The project is considered Minor Reconstruction per TRANS 401.03(3)(f) - No TSS Reduction Required. 19 DESCRIBE THE STORMWATER QUALITY MANAGEMENT REQUIREMENTS PER TRANS 401 OR THE TMDL WASTELOAD ALLOCATION. 20 ☐ 40 % Reduction ☐ 80 % Reduction ☐ Other Reduction 21 IF THE PROJECT REQUIRES STORMWATER MANAGEMENT EXPLAIN HOW THE TRANS 401 2-YR PEAK DISCHARGE REQUIREMENT WAS MET. 22 23 24 HAS THE DEPARTMENT AGREED TO MEET ANY LOCAL STORMWATER QUALITY ORDINANCES OR REQUIREMENTS FOR THIS PROJECT? IF SO, DESCRIBE. 25 IF THE PROJECT REQUIRES STORM WATER MANAGEMENT EXPLAIN HOW THE TOTAL SUSPENDED SOLIDS REDUCTION WAS MET. Refer to Water Quality Results Summary above. Existing curb and gutter at the intersections is being replaced and extended to the meet the current intersection SDD's. Thus, the drainage pattern is not changing from the existing condition but will continue to drain through the ditch section. LIST THE POST CONSTRUCTION STORMWATER QUALITY CONTROL TREATMENT MEASURES FOR THE PROJECT. 28 29

	REGIONAL STORMWATER ENGINEER CONCURRENCE (SIGN AND DATE)
30	

	DRAINAGE AREA CALCULATIONS FOR STH 60 EAGLE TO STH 181 STATE ID 2310-17-00														
Basin	1	2	3	4	4A	5	6	7	8	8 (Off-Site)	9	10	11	12	13
RW Area	4.49	3.15	3.16	2.16	0.83	1.93	0.85	1.4	3.39	3.39	2.49	0.92	3.18	4.37	1.85
Total Area	4.49	3.15	8.45	3	3.87	2.27	0.85	2.8	9.98	25.84	2.54	0.92	6.72	5.06	2.1
Length	1640	2393	2300	1572	600	1407	722	1022	2601	2601	1673	720	2282	2226	1419
EX Paved	1.38	0.82	0.79	0.54	0.21	0.48	0.25	0.57	1.05	1.05	0.75	0.35	0.90	1.10	0.49
EX Gravel	0.53	0.38	0.37	0.25	0.10	0.23	0.12	0.16	0.42	0.42	0.26	0.12	0.37	0.36	0.23
PR Paved	1.74	0.98	0.95	0.65	0.25	0.58	0.30	0.64	1.40	1.40	1.00	0.45	1.20	1.38	0.59
PR Gravel	0.3	0.22	0.21	0.14	0.06	0.13	0.07	0.09	0.24	0.24	0.15	0.08	0.20	0.15	0.13
C Land	0.18	0.14	0.14	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18
C Pavement	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
C Gravel	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
	,	1	1					-		7	· · · · · · · · · · · · · · · · · · ·		1	7	
Pre Road	1.38	0.82	0.79	0.54	0.21	0.48	0.25	0.57	1.05	1.05		0.35			
Pre Open Land	2.58	1.95	7.29	2.21	3.57	1.56	0.48	2.07	8.51	24.37	1.53	0.45	5.45	3.60	1.38
Pre Gravel	0.53	0.38	0.37	0.25	0.10	0.23	0.12	0.16	0.42	0.42	0.26	0.12	0.37	0.36	0.23
Post Road	1.63	0.98	0.95	0.65	0.25	0.58	0.30	0.64	1.40	1.40	1.00	0.45	1.30	1.38	0.59
Post Open Land	2.52	1.95	7.29	2.21	3.57	1.56	0.48	2.07	8.34	24.20	1.39	0.39		3.53	1.38
Post Gravel	0.34	0.22	0.21	0.14	0.06	0.13	0.07	0.09	0.24	0.24	0.15	0.08			0.13
CN Existing	0.47	0.41	0.24	0.35	0.23	0.39	0.47	0.36	0.28	0.22	0.45	0.53	0.31	0.38	0.40
CN Proposed	0.49	0.42	0.24	0.37	0.24	0.40	0.49	0.37	0.30	0.23	0.51	0.59	0.34	0.40	0.42
*Time of Concentration	25.0	25.0	40.0	10.0	20.0	10.0	12.0	12.0	20.0	20.0	15.0	11.0	26.0	21.0	13.0

^{*} Time of Concentration determined from FDM 13-10 Attachment 5.3 Time of Concentration of Small Drainage Basins (Nomograph)

	DRAINAGE AREA CALCULATIONS FOR STH 60 EAGLE TO STH 181 STATE ID 2310-17-00														
Basin	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28
RW Area	3.61	1.27	0.74	0.85	1.23	0.96	0.92	0.42	0.42	2.81	3	7.47	2.5	4.38	1.09
Total Area	7.06	1.27	0.76	1.47	1.89	1.02	1.06	0.42	0.74	3.28	3.3	10.1	2.6	13.07	1.33
Length	2719	1017	434	591	712	558	473	231	254	2376	2376	5709	1956	3753	966
EX Paved	0.94	0.35	0.28	0.24	0.38	0.34	0.37	0.34	0.17	0.81	0.81	2.30	0.75	1.29	0.33
EX Gravel	0.44	0.16	0.07	0.11	0.13	0.08	0.08	0.04	0.05	0.38	0.38	0.92	0.31	0.60	0.15
PR Paved	1.12	0.42	0.31	0.30	0.59	0.37	0.48	0.35	0.20	0.98	0.98	2.80	0.95	1.55	0.39
PR Gravel	0.25	0.09	0.04	0.06	0.07	0.05	0.05	0.03	0.03	0.22	0.22	0.52	0.15	0.34	0.09
C Land	0.16	0.15	0.18	0.18	0.18	0.15	0.22	0.22	0.22	0.16	0.14	0.14	0.14	0.18	0.14
C Pavement	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
C Gravel	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Pre Road	0.94	0.35	0.28	0.24	0.38	0.34	0.37	0.340	0.170	0.810	0.81	2.30	0.75	1.29	0.33
Pre Open Land	5.69	0.76	0.41	1.12	1.38	0.60	0.61	0.043	0.520	2.088	2.11	6.88	1.54	11.17	0.85
Pre Gravel	0.44	0.16	0.07	0.11	0.13	0.08	0.08	0.037	0.050	0.382	0.38	0.92	0.31	0.60	0.15
Post Road	1.12	0.42	0.31	0.30	0.59	0.37	0.45	0.350	0.200	0.980	0.98	2.80	0.95	1.55	0.39
Post Open Land	5.69	0.76	0.41	1.11	1.23	0.60	0.56	0.040	0.510	2.080	2.10	6.78	1.50		0.85
Post Gravel	0.25	0.09	0.04	0.06	0.07	0.05	0.05	0.030	0.030	0.220	0.22	0.52	0.15		0.09
CN Existing	0.29	0.43	0.50	0.34	0.36	0.45	0.50	0.84	0.41	0.41	0.39	0.37	0.43	0.28	0.39
CN Proposed	0.30	0.45	0.52	0.35	0.44	0.46	0.55	0.86	0.43	0.43	0.41	0.39			0.41
*Time of Concentration	28.0	13.0	7.0	7.0	8.0	14.0	13.0	5.0	6.0	19.0	20.0	30.0	20.0	50.0	10.0

^{*} Time of Concentration deteri

		DRA	INAGE AREA	CALCULATIO	NS FOR STH	60 EAGLE TO	STH 181 STA	TE ID 2310-1	7-00	
Basin	29	30	31	32	33A	33B	34	35	36	37
RW Area	1.02	2.73	1.22	3.32	3.66	2.72	1.58	2	2.58	2.71
Total Area	1.33	3.3	1.88	3.68	13.74	10.18	1.61	2.31	2.58	3.92
Length	966	2385	1124	2637	1699	2010	1172	1361	1940	1940
EX Paved	0.33	0.92	0.39	1.51	1.26	0.94	0.40	0.47	0.96	0.67
EX Gravel	0.15	0.38	0.18	0.42	0.34	0.26	0.19	0.22	0.31	0.31
PR Paved	0.39	1.12	0.46	1.71	1.47	1.09	0.54	0.64	1.21	0.82
PR Gravel	0.09	0.22	0.10	0.24	0.20	0.14	9.08	0.10	0.16	0.18
C Land	0.14	0.17	0.19	0.19	0.19	0.19	0.2	0.19	0.19	0.19
C Pavement	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95	0.95
C Gravel	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Pre Road	0.330	0.920	0.39	1.510	1.260	0.940	0.40	0.47	0.96	0.67
Pre Open Land	0.85	2.00	1.31	1.75	12.14	8.98	1.02	1.62	1.31	2.94
Pre Gravel	0.150	0.380	0.181	0.420	0.340	0.260	0.19	0.22	0.31	0.31
Post Road	0.39	1.12	0.46	1.71	1.47	1.09	(0.54	0.64	1.21	0.82
Post Open Land	0.85	1.96	1.31	1.73	12.07	8.95	1 (1.21	2.93
Post Gravel	0.09	0.22	0.10	0.24	0.20	0.14	0.08ع			0.18
CN Existing	0.39	0.44	0.39	0.55	0.27	0.27	0.43	0.38	0.52	0.35
CN Proposed	0.41	0.46	0.40	0.57	0.28	0.28	(0.47	0.42	0.57	0.37
*Time of Concentration	10.0	11.0	20.0	25.0	26.0	14.0	21.0	13.0	28.0	13.0

^{*} Time of Concentration deteri



State of Wisconsin
DEPARTMENT OF NATURAL RESOURCES
101 S. Webster Street
Box 7921
Madison WI 53707-7921

Scott Walker, Governor Cathy Stepp, Secretary Telephone 608-266-2621 Toll Free 1-888-936-7463 TTY Access via relay - 711



April 16, 2012

Mohammad Hossain Wisconsin Department of Transportation 141 NW Barstow Street Waukesha, WI 53187-0798

Subject: Initial Scoping Comments for WisDOT ID: 2310-17-00, State Highway 60 Rehabilitation; Eagle Drive to STH 181, Washington and Ozaukee Counties

Dear Mr. Hossain:

Thank you for the opportunity to provide scoping comments for the State Highway 60 Rehabilitation. It is understood that the Project will include improvements to State Highway 60 from just east of Eagle Drive in the Village of Jackson, Washington County, to State Highway 181 in the Town of Cedarburg, Ozaukee County. Improvements consist of the resurfacing the mainline of STH 60, minor reconstruction of various intersections, beam guard replacement, culvert replacement/extension and shoulder reconstruction with ditch grading. The purpose of the project is to improve the condition of the pavement and safety in the corridor. I have listed Department initial review comments below.

Air

- DNR recommends that the environmental analysis assess existing and projected air pollutant emissions, health risks; identify sensitive receptors, and alternatives to minimize temporary construction and long term air quality impacts. The State of Wisconsin Implementation Plan for Air Quality http://dnr.wi.gov/org/aw/air/hot/1hrsip_p2.htm establishes emission budgets for mobile sources in Wisconsin.
- 2) If the project includes structural demolition work a **Notification of Demolition and/or Renovation** and Application for Permit Exemption (NR 406, 410, and 447 Wis. Adm. Code) may be required. Please contact Mark Davis, Asbestos Specialist (414) 263-8674 to request additional information and permit application materials.

Remediation and Redevelopment/Waste and Materials Management

- 1) Properties having documented soil and groundwater contamination in the right-of-way of WIS 60 exist in the project area. A Hazardous Materials Assessment is recommended as part of the environmental project. Please coordinate with the Department in determining the extent of this contamination and minimizing the risk of encountering hazardous waste during construction. The Department can also assist in removal and disposal of hazardous wastes that cannot be avoided during construction. Please contact me for a list of properties of concern in the project area.
- 2) Should contaminated soil or groundwater be encountered within the right-of-way either before or during construction, you must notify the appropriate person in the DNR Solid Waste Section at 1-800-943-0003 prior to continuing operations.



Land

- Primary and Secondary Environmental Corridors and Areas of Isolated Resources exists in the project area. The majority of the primary corridor is along Cedar Creek and Cedarburg Creek, and in the vicinity of the Jackson Swamp. Endangered resources and species habitat may exist in these corridors. See the SEWRPC website for more information on Environmental Corridors at: http://www.sewrpc.org/regionallandinfo/regionalmapping/default.shtm.
- DNR managed lands exist in the project area. DNR initial review indicates that the acquisition of selected properties was funded by State Stewardship Grants and US Geological Survey Great Lakes Aquatic Gap Analysis Program (USGS GAP). According to Section 6(f) of the federal Land and Water Conservation (L&WC) Act, lands acquired with L&WC funds that are taken by a highway project must be replaced with other property of equal market value and equivalent usefulness and location. Please discuss land conversion requirements with the Department if these properties will be impacted by the WIS 60 project.
- 3) DNR managed trails intersect STH 60 near Cedar Creek in Washington County, near Horns Corners Road in Ozaukee County, at the Five Corners intersection, and near County Highway O in Grafton. Any construction impacts on the trails shall be replaced at or above current condition.

Water

- The WIS 60 project area is located in the Cedar Creek Watershed and the Milwaukee River South Watershed. These watersheds are in the Milwaukee River Basin. Detailed basin reports can be found at: http://dnr.wi.gov/water/basin/milw/index.htm
- 2) The project area crosses Cedar Creek and Cedarburg Creek. In addition, several unnamed tributaries to these creeks also intersect the STH 60 corridor. Existing culverts and/or bridges need to be assessed as well as temporary or permanent alterations to the water crossings that may be necessary due to proposed construction.
- 3) Channel stability and fish and wildlife passage should be standard design and construction objectives for any bridge or culvert replacements or extensions.
- 4) Wetlands are present in the project area. DNR initial review finds wetland classifications in the project area to include:

Southern Messic Forest Harwood Swamp Southern Hardwood Swamp

- 5) Wetland impacts should be avoided or minimized. Wetland impacts that can not be avoided should be addressed through the DNR-DOT Cooperative Agreement process and compensatory mitigation plans need to be arranged. A Section 404 permit may be necessary from the U.S. Army Corps of Engineers.
- 6) Storm water facilities and erosion control best management practices should be designed to meet Trans 401 standards. Coordinate with local municipalities on designing stormwater facilities.

Endangered Resources

1) State endangered species have been observed recently in the project area. Please coordinate with the Department on laws pertaining to these species and to identify the presence of and minimize impacts to these species. An Endangered Resources Incidental Take Authorization permit (Wis. Stats 29.604) may be needed for work in species' habitat. These species include:

Regina septemvittata (Queesnake) Villosa iris (Rainbow Shell Mussel) Luxilus chrysocephalus (Striped Shiner Fish)

2) State threatened species are present in the project area. Please coordinate with the Department to identify the presence of and minimize impacts to these species. These species include:

Lythrurus umbratilis (Redfin Shiner Fish) Moxostoma valenciennesi (Greater Redhorse Fish) Venustaconcha ellipsiformis (Ellipse Mussel)

1) DNR and DOT should discuss endangered resources occurrences in the large project area and determine if specific field surveys or investigations are needed.

Thanks again for the opportunity to provide scoping comments for the project of the State Highway 60 Rehabilitation Eagle Drive to STH 181, Washington and Ozaukee Counties. I would be glad to speak or meet with you to discuss the Department's comments and provide additional information.

Sincerely,

Kristina Betzold

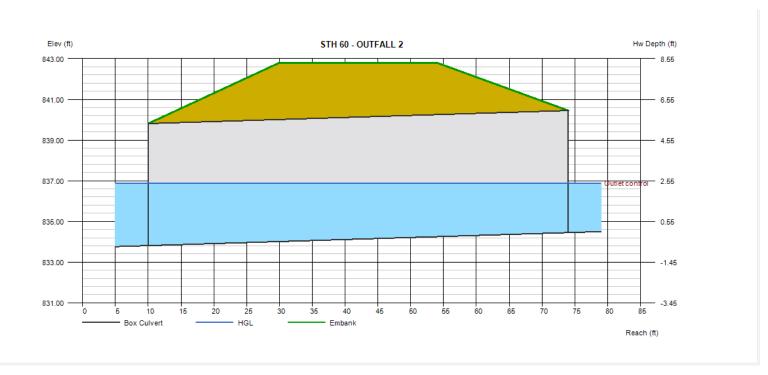
Kristina Betzold Environmental Analysis and Review Specialist (414) 263-8517 kristina.betzold@wiscosin.gov

Cc: Rachel Tranel, Collins Engineering Karla Leithoff, WDOT Scott Lee, WDOT

Friday, Apr 1 2016

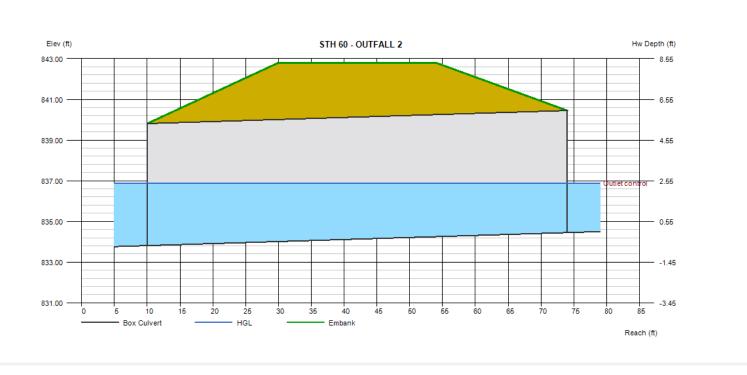
STH 60 - OUTFALL 2 50 YR Existing

Invert Elev Dn (ft)	= 833.81	Calculations	
Pipe Length (ft)	= 64.00	Qmin (cfs)	= 5.61
Slope (%)	= 1.00	Qmax (cfs)	= 5.61
Invert Elev Up (ft)	= 834.45	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 72.0		
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 5.74
No. Barrels	= 2	Qpipe (cfs)	= 5.74
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.12
Culvert Entrance	= 30D to 75D wingwall flares	Veloc Up (ft/s)	= 0.15
Coeff. K,M,c,Y,k	= 0.026, 1, 0.0347, 0.81, 0.4	HGL Dn (ft)	= 836.89
		HGL Up (ft)	= 836.89
Embankment		Hw Elev (ft)	= 836.89
Top Elevation (ft)	= 842.80	Hw/D (ft)	= 0.41
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 2 50 YR Proposed

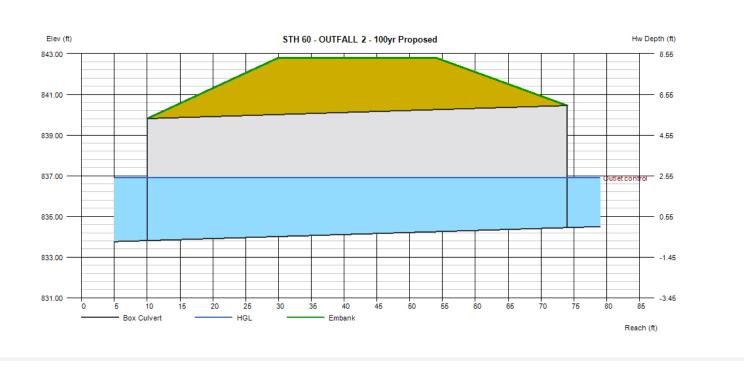
Invert Elev Dn (ft)	= 833.81	Calculations	
Pipe Length (ft)	= 64.00	Qmin (cfs)	= 5.74
Slope (%)	= 1.00	Qmax (cfs)	= 5.74
Invert Elev Up (ft)	= 834.45	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 72.0		
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 5.74
No. Barrels	= 2	Qpipe (cfs)	= 5.74
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.12
Culvert Entrance	= 30D to 75D wingwall flares	Veloc Up (ft/s)	= 0.15
Coeff. K,M,c,Y,k	= 0.026, 1, 0.0347, 0.81, 0.4	HGL Dn (ft)	= 836.89
		HGL Up (ft)	= 836.89
Embankment		Hw Elev (ft)	= 836.89
Top Elevation (ft)	= 842.80	Hw/D (ft)	= 0.41
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



Wednesday, Mar 18 2015

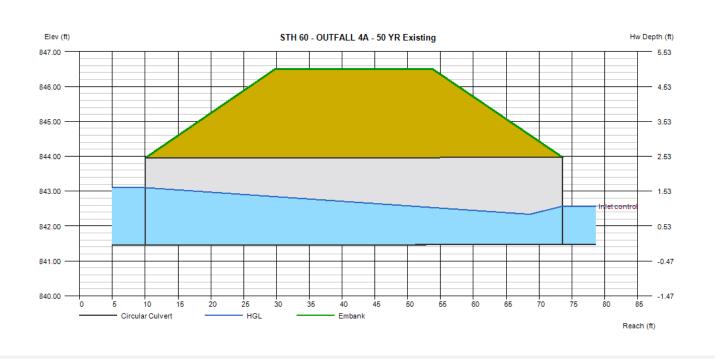
STH 60 - OUTFALL 2 - 100yr Proposed

Invert Elev Dn (ft)	= 833.81	Calculations	
Pipe Length (ft)	= 64.00	Qmin (cfs)	= 6.13
Slope (%)	= 1.00	Qmax (cfs)	= 6.13
Invert Elev Up (ft)	= 834.45	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 72.0	, ,	, ,
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 6.13
No. Barrels	= 2	Qpipe (cfs)	= 6.13
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.12
Culvert Entrance	= 30D to 75D wingwall flares	Veloc Up (ft/s)	= 0.16
Coeff. K,M,c,Y,k	= 0.026, 1, 0.0347, 0.81, 0.4	HGL Dn (ft)	= 836.89
		HGL Up (ft)	= 836.89
Embankment		Hw Elev (ft)	= 836.89
Top Elevation (ft)	= 842.80	Hw/D (ft)	= 0.41
Top Width (ft)	= 24.00	Flow Regime	Outlet Control
Crest Width (ft)	= 20.00	-	
Crest width (it)	= 20.00		



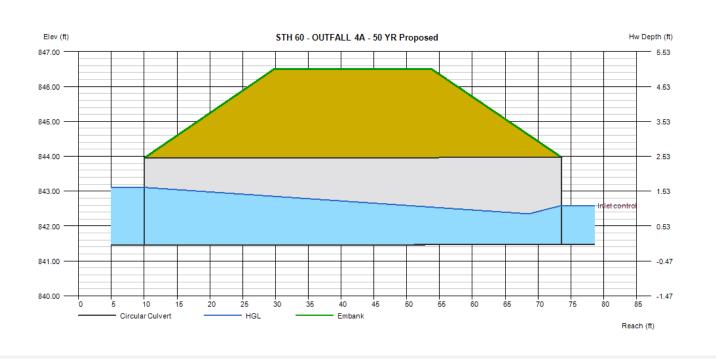
STH 60 - OUTFALL 4A - 50 YR Existing

Invert Elev Dn (ft)	= 841.45	Calculations	
Pipe Length (ft)	= 63.60	Qmin (cfs)	= 5.88
Slope (%)	= 0.03	Qmax (cfs)	= 5.88
Invert Elev Up (ft)	= 841.47	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 5.88
No. Barrels	= 1	Qpipe (cfs)	= 5.88
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 1.71
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.33
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 843.10
		HGL Up (ft)	= 842.27
Embankment		Hw Elev (ft)	= 842.57
Top Elevation (ft)	= 846.50	Hw/D (ft)	= 0.44
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



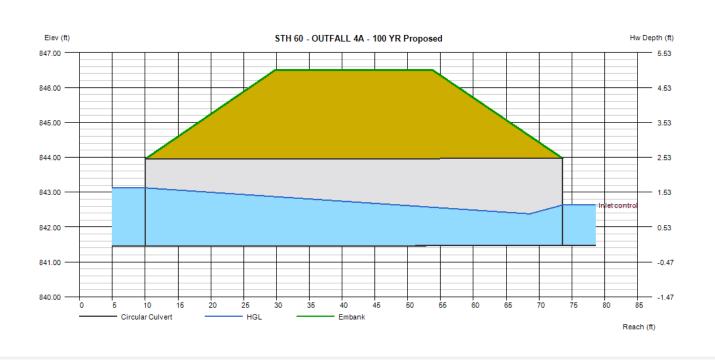
STH 60 - OUTFALL 4A - 50 YR Proposed

Invert Elev Dn (ft)	= 841.45	Calculations	
Pipe Length (ft)	= 63.60	Qmin (cfs)	= 6.07
Slope (%)	= 0.03	Qmax (cfs)	= 6.07
Invert Elev Up (ft)	= 841.47	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 6.07
No. Barrels	= 1	Qpipe (cfs)	= 6.07
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 1.76
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.37
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 843.11
		HGL Up (ft)	= 842.28
Embankment		Hw Elev (ft)	= 842.59
Top Elevation (ft)	= 846.50	Hw/D (ft)	= 0.45
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 4A - 100 YR Proposed

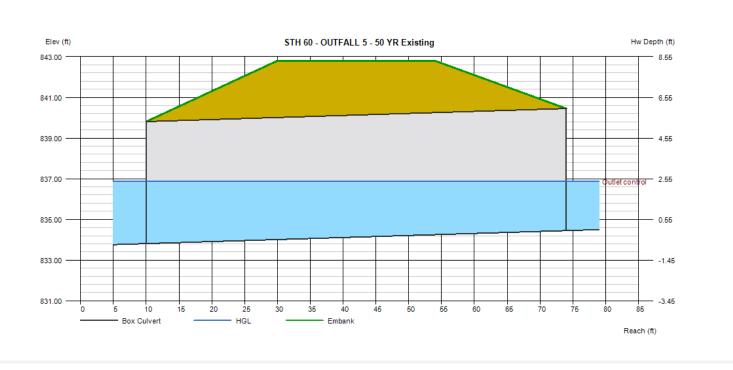
Invert Elev Dn (ft)	= 841.45	Calculations	
Pipe Length (ft)	= 63.60	Qmin (cfs)	= 6.50
Slope (%)	= 0.03	Qmax (cfs)	= 6.50
Invert Elev Up (ft)	= 841.47	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0	. ,	, ,
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 6.50
No. Barrels	= 1	Qpipe (cfs)	= 6.50
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 1.86
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.46
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 843.12
		HGL Up (ft)	= 842.31
Embankment		Hw Elev (ft)	= 842.63
Top Elevation (ft)	= 846.50	Hw/D (ft)	= 0.46
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



Friday, Apr 1 2016

STH 60 - OUTFALL 5 - 50 YR Existing

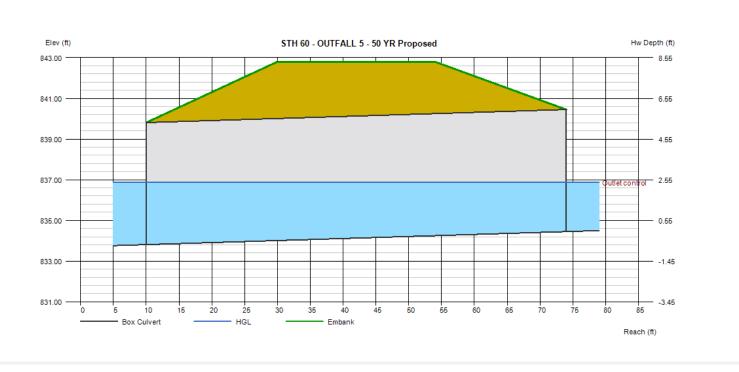
Invert Elev Dn (ft)	= 833.81	Calculations	
Pipe Length (ft)	= 64.00	Qmin (cfs)	= 4.23
Slope (%)	= 1.00	Qmax (cfs)	= 4.23
Invert Elev Up (ft)	= 834.45	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 72.0	. ,	, ,
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 4.23
No. Barrels	= 2	Qpipe (cfs)	= 4.23
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.09
Culvert Entrance	= 30D to 75D wingwall flares	Veloc Up (ft/s)	= 0.11
Coeff. K,M,c,Y,k	= 0.026, 1, 0.0347, 0.81, 0.4	HGL Dn (ft)	= 836.87
		HGL Up (ft)	= 836.88
Embankment		Hw Elev (ft)	= 836.88
Top Elevation (ft)	= 842.80	Hw/D (ft)	= 0.40
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00	-	



Friday, Apr 1 2016

STH 60 - OUTFALL 5 - 50 YR Proposed

Invert Elev Dn (ft)	= 833.81	Calculations	
Pipe Length (ft)	= 64.00	Qmin (cfs)	= 4.38
Slope (%)	= 1.00	Qmax (cfs)	= 4.38
Invert Elev Up (ft)	= 834.45	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 72.0		
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 4.38
No. Barrels	= 2	Qpipe (cfs)	= 4.38
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.09
Culvert Entrance	= 30D to 75D wingwall flares	Veloc Up (ft/s)	= 0.11
Coeff. K,M,c,Y,k	= 0.026, 1, 0.0347, 0.81, 0.4	HGL Dn (ft)	= 836.88
		HGL Up (ft)	= 836.88
Embankment		Hw Elev (ft)	= 836.88
Top Elevation (ft)	= 842.80	Hw/D (ft)	= 0.40
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



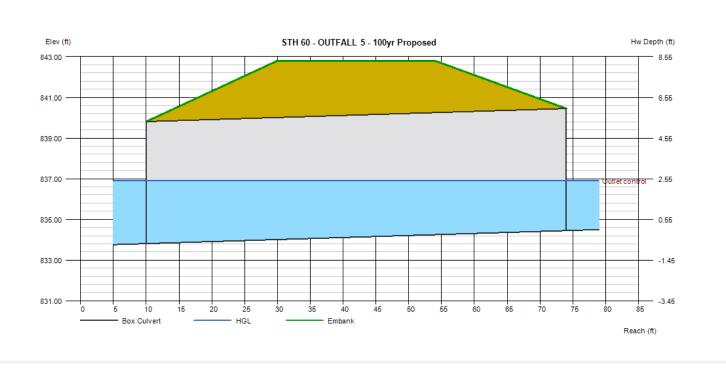
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Mar 18 2015

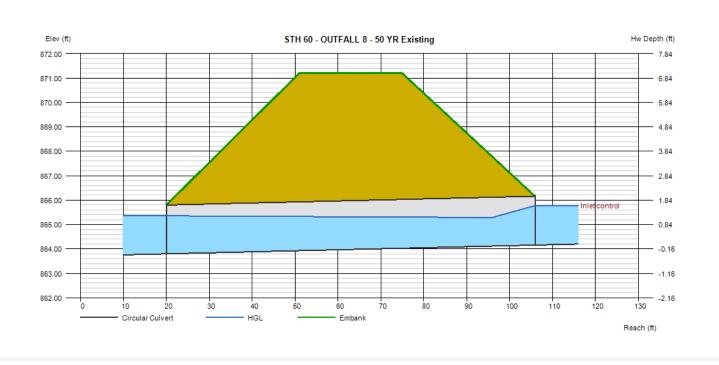
STH 60 - OUTFALL 5 - 100yr Proposed

Invert Elev Dn (ft)	= 833.81	Calculations	
Pipe Length (ft)	= 64.00	Qmin (cfs)	= 6.15
Slope (%)	= 1.00	Qmax (cfs)	= 6.15
Invert Elev Up (ft)	= 834.45	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 72.0		
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 6.15
No. Barrels	= 2	Qpipe (cfs)	= 6.15
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.12
Culvert Entrance	= 30D to 75D wingwall flares	Veloc Up (ft/s)	= 0.16
Coeff. K,M,c,Y,k	= 0.026, 1, 0.0347, 0.81, 0.4	HGL Dn (ft)	= 836.89
		HGL Up (ft)	= 836.89
Embankment		Hw Elev (ft)	= 836.89
Top Elevation (ft)	= 842.80	Hw/D (ft)	= 0.41
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 8 - 50 YR Existing

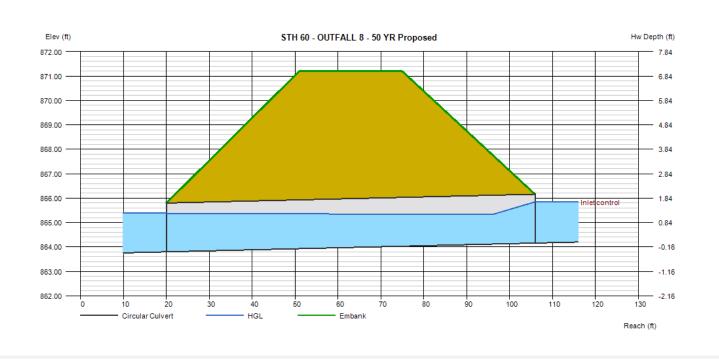
Invert Elev Dn (ft)	= 863.80	Calculations	
Pipe Length (ft)	= 85.90	Qmin (cfs)	= 9.78
Slope (%)	= 0.42	Qmax (cfs)	= 9.78
Invert Elev Up (ft)	= 864.16	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0	. ,	, ,
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 9.78
No. Barrels	= 1	Qpipe (cfs)	= 9.78
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 3.72
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 5.42
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 865.36
		HGL Up (ft)	= 865.28
Embankment		Hw Elev (ft)	= 865.77
Top Elevation (ft)	= 871.20	Hw/D (ft)	= 0.81
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



 $\label{thm:local_equation} \mbox{Hydraflow Express Extension for Autodesk@ AutoCAD@ Civil 3D@ by Autodesk, Inc.}$

STH 60 - OUTFALL 8 - 50 YR Proposed

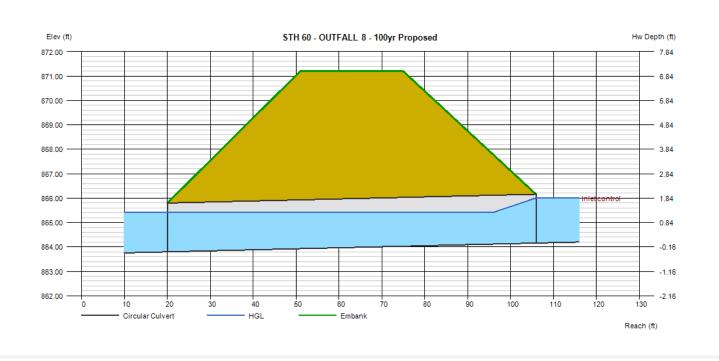
Invert Elev Dn (ft)	= 863.80	Calculations	
Pipe Length (ft)	= 85.90	Qmin (cfs)	= 10.48
Slope (%)	= 0.42	Qmax (cfs)	= 10.48
Invert Elev Up (ft)	= 864.16	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 10.48
No. Barrels	= 1	Qpipe (cfs)	= 10.48
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 3.94
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 5.56
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 865.38
		HGL Up (ft)	= 865.32
Embankment		Hw Elev (ft)	= 865.84
Top Elevation (ft)	= 871.20	Hw/D (ft)	= 0.84
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



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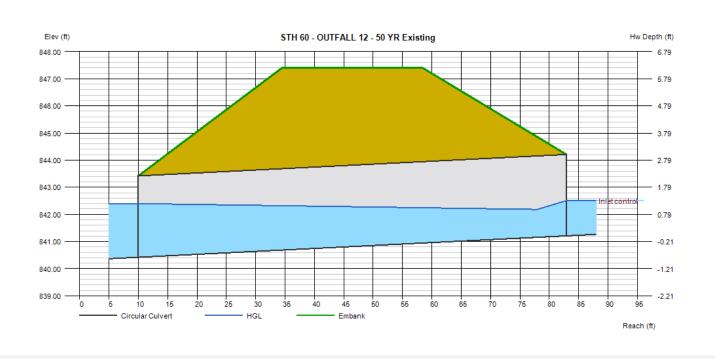
STH 60 - OUTFALL 8 - 100yr Proposed

Invert Elev Dn (ft)	= 863.80	Calculations	
Pipe Length (ft)	= 85.90	Qmin (cfs)	= 12.12
Slope (%)	= 0.42	Qmax (cfs)	= 12.12
Invert Elev Up (ft)	= 864.16	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 12.12
No. Barrels	= 1	Qpipe (cfs)	= 12.12
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 4.43
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 5.87
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 865.43
		HGL Up (ft)	= 865.41
Embankment		Hw Elev (ft)	= 866.01
Top Elevation (ft)	= 871.20	Hw/D (ft)	= 0.92
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



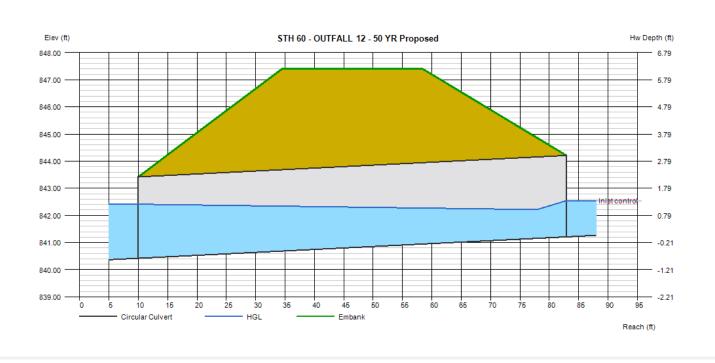
STH 60 - OUTFALL 12 - 50 YR Existing

Invert Elev Dn (ft)	= 840.42	Calculations	
Pipe Length (ft)	= 72.90	Qmin (cfs)	= 9.19
Slope (%)	= 1.08	Qmax (cfs)	= 9.19
Invert Elev Up (ft)	= 841.21	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 9.19
No. Barrels	= 1	Qpipe (cfs)	= 9.19
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 1.86
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.73
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 842.40
		HGL Up (ft)	= 842.17
Embankment		Hw Elev (ft)	= 842.51
Top Elevation (ft)	= 847.40	Hw/D (ft)	= 0.43
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 12 - 50 YR Proposed

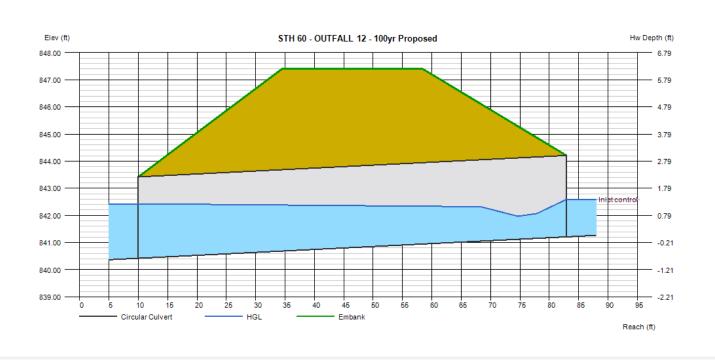
Invert Elev Dn (ft)	= 840.42	Calculations	
Pipe Length (ft)	= 72.90	Qmin (cfs)	= 9.67
Slope (%)	= 1.08	Qmax (cfs)	= 9.67
Invert Elev Up (ft)	= 841.21	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 9.67
No. Barrels	= 1	Qpipe (cfs)	= 9.67
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 1.94
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.76
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 842.41
		HGL Up (ft)	= 842.20
Embankment		Hw Elev (ft)	= 842.54
Top Elevation (ft)	= 847.40	Hw/D (ft)	= 0.44
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



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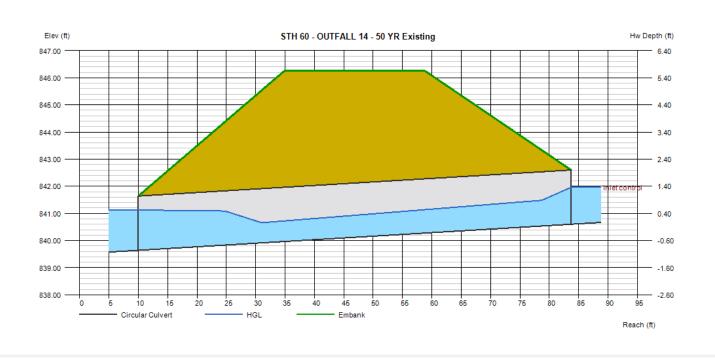
STH 60 - OUTFALL 12 - 100yr Proposed

Invert Elev Dn (ft)	= 840.42	Calculations	
Pipe Length (ft)	= 72.90	Qmin (cfs)	= 10.27
Slope (%)	= 1.08	Qmax (cfs)	= 10.27
Invert Elev Up (ft)	= 841.21	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 10.27
No. Barrels	= 1	Qpipe (cfs)	= 10.27
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 2.04
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.84
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 842.43
		HGL Up (ft)	= 842.23
Embankment		Hw Elev (ft)	= 842.59
Top Elevation (ft)	= 847.40	Hw/D (ft)	= 0.46
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



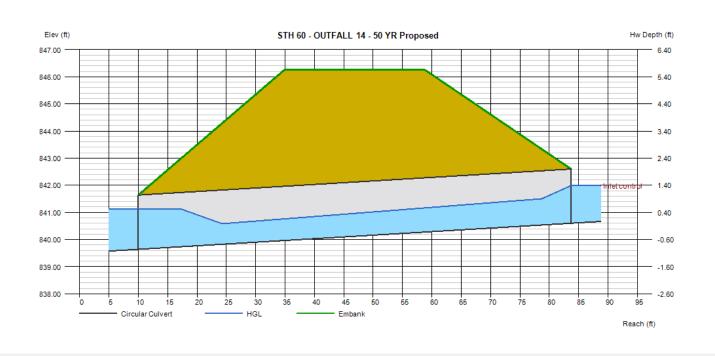
STH 60 - OUTFALL 14 - 50 YR Existing

Invert Elev Dn (ft)	= 839.64	Calculations	
Pipe Length (ft)	= 73.70	Qmin (cfs)	= 7.45
Slope (%)	= 1.30	Qmax (cfs)	= 7.45
Invert Elev Up (ft)	= 840.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 7.45
No. Barrels	= 1	Qpipe (cfs)	= 7.45
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 2.98
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.94
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 841.12
		HGL Up (ft)	= 841.57
Embankment		Hw Elev (ft)	= 841.96
Top Elevation (ft)	= 846.25	Hw/D (ft)	= 0.68
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 73.70		



STH 60 - OUTFALL 14 - 50 YR Proposed

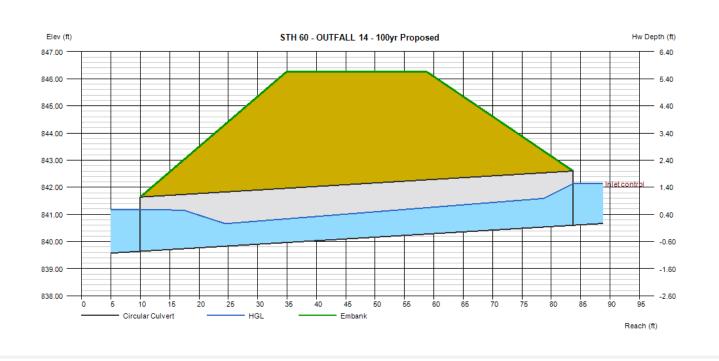
Invert Elev Dn (ft)	= 839.64	Calculations	
Pipe Length (ft)	= 73.70	Qmin (cfs)	= 7.71
Slope (%)	= 1.30	Qmax (cfs)	= 7.71
Invert Elev Up (ft)	= 840.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 7.71
No. Barrels	= 1	Qpipe (cfs)	= 7.71
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 3.06
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.99
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 841.13
		HGL Up (ft)	= 841.59
Embankment		Hw Elev (ft)	= 841.99
Top Elevation (ft)	= 846.25	Hw/D (ft)	= 0.69
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 73.70		



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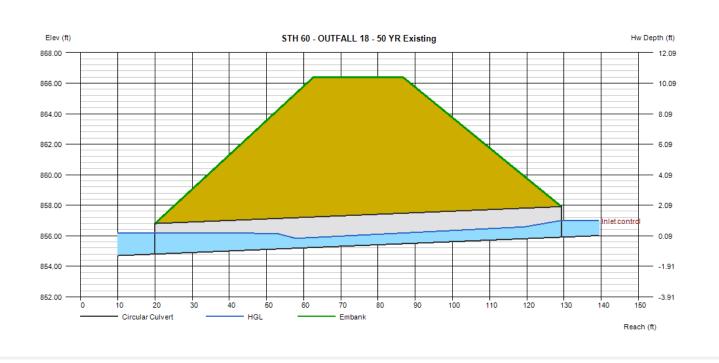
STH 60 - OUTFALL 14 - 100yr Proposed

Invert Elev Dn (ft)	= 839.64	Calculations	
Pipe Length (ft)	= 73.70	Qmin (cfs)	= 9.07
Slope (%)	= 1.30	Qmax (cfs)	= 9.07
Invert Elev Up (ft)	= 840.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 9.07
No. Barrels	= 1	Qpipe (cfs)	= 9.07
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 3.50
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 5.28
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 841.18
		HGL Up (ft)	= 841.67
Embankment		Hw Elev (ft)	= 842.13
Top Elevation (ft)	= 846.25	Hw/D (ft)	= 0.77
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 73.70		



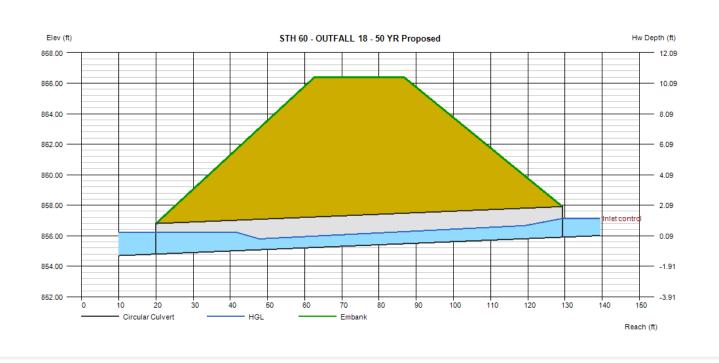
STH 60 - OUTFALL 18 - 50 YR Existing

Invert Elev Dn (ft)	= 854.80	Calculations	
Pipe Length (ft)	= 109.30	Qmin (cfs)	= 5.06
Slope (%)	= 1.02	Qmax (cfs)	= 5.06
Invert Elev Up (ft)	= 855.91	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 5.06
No. Barrels	= 1	Qpipe (cfs)	= 5.06
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 2.16
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.37
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 856.20
		HGL Up (ft)	= 856.70
Embankment		Hw Elev (ft)	= 857.00
Top Elevation (ft)	= 866.40	Hw/D (ft)	= 0.55
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 18 - 50 YR Proposed

Invert Elev Dn (ft)	= 854.80	Calculations	
Pipe Length (ft)	= 109.30	Qmin (cfs)	= 6.18
Slope (%)	= 1.02	Qmax (cfs)	= 6.18
Invert Elev Up (ft)	= 855.91	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 6.18
No. Barrels	= 1	Qpipe (cfs)	= 6.18
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 2.55
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.65
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 856.24
		HGL Up (ft)	= 856.79
Embankment		Hw Elev (ft)	= 857.13
Top Elevation (ft)	= 866.40	Hw/D (ft)	= 0.61
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



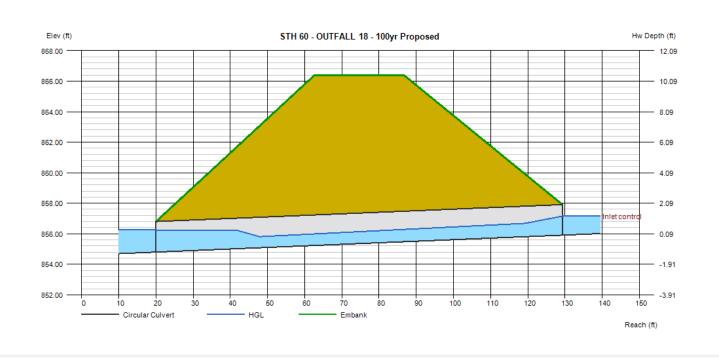
Crest Width (ft)

= 20.00

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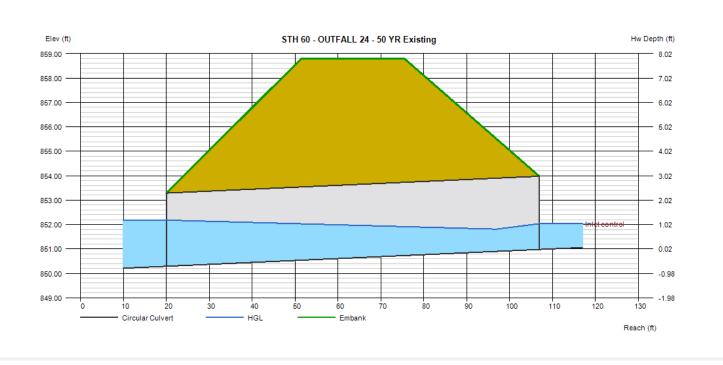
STH 60 - OUTFALL 18 - 100yr Proposed

Invert Elev Dn (ft)	= 854.80	Calculations	
Pipe Length (ft)	= 109.30	Qmin (cfs)	= 6.40
Slope (%)	= 1.02	Qmax (cfs)	= 6.40
Invert Elev Up (ft)	= 855.91	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 6.40
No. Barrels	= 1	Qpipe (cfs)	= 6.40
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 2.63
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.70
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 856.25
		HGL Up (ft)	= 856.80
Embankment		Hw Elev (ft)	= 857.16
Top Elevation (ft)	= 866.40	Hw/D (ft)	= 0.62
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control



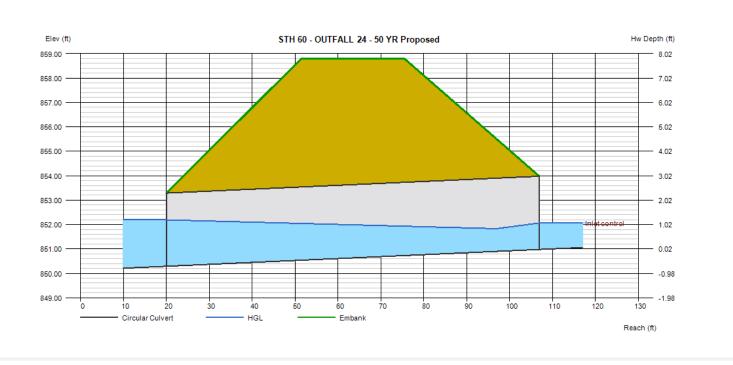
STH 60 - OUTFALL 24 - 50 YR Existing

= 6.23
= 6.23
= (dc+D)/2
= 6.23
= 6.23
= 0.00
= 1.33
= 4.24
= 852.18
= 851.76
= 852.03
= 0.35
= Inlet Control



STH 60 - OUTFALL 24 - 50 YR Proposed

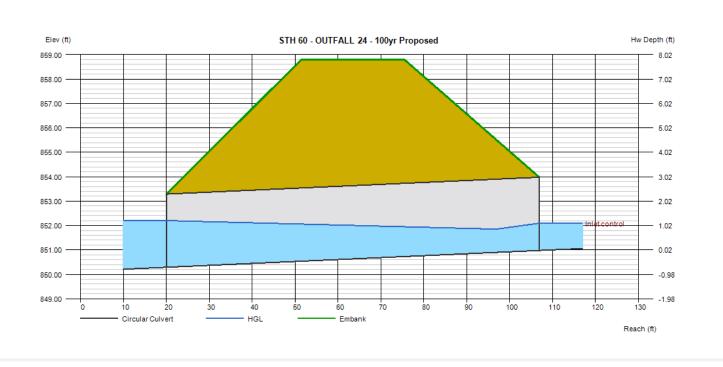
Invert Elev Dn (ft)	= 850.29	Calculations	
Pipe Length (ft)	= 86.90	Qmin (cfs)	= 6.55
Slope (%)	= 0.79	Qmax (cfs)	= 6.55
Invert Elev Up (ft)	= 850.98	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 36.0	. ,	, ,
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 6.55
No. Barrels	= 1	Qpipe (cfs)	= 6.55
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 1.39
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.30
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 852.19
		HGL Up (ft)	= 851.78
Embankment		Hw Elev (ft)	= 852.06
Top Elevation (ft)	= 858.80	Hw/D (ft)	= 0.36
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



Wednesday, Mar 18 2015

STH 60 - OUTFALL 24 - 100yr Proposed

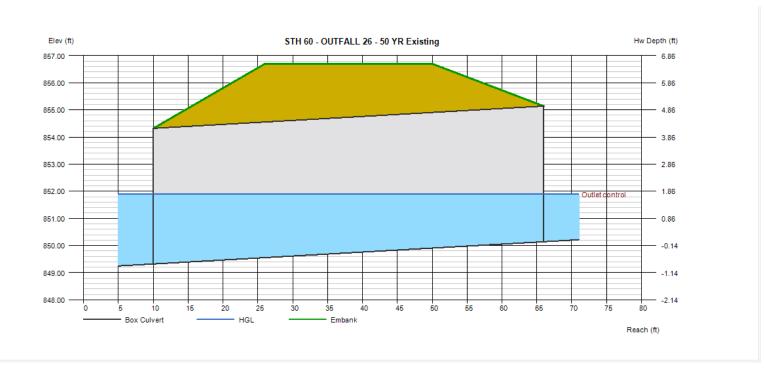
Invert Elev Dn (ft)	= 850.29	Calculations	
Pipe Length (ft)	= 86.90	Qmin (cfs)	= 6.92
Slope (%)	= 0.79	Qmax (cfs)	= 6.92
Invert Elev Up (ft)	= 850.98	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 6.92
No. Barrels	= 1	Qpipe (cfs)	= 6.92
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 1.45
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 4.37
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 852.20
		HGL Up (ft)	= 851.81
Embankment		Hw Elev (ft)	= 852.10
Top Elevation (ft)	= 858.80	Hw/D (ft)	= 0.37
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



Friday, Apr 1 2016

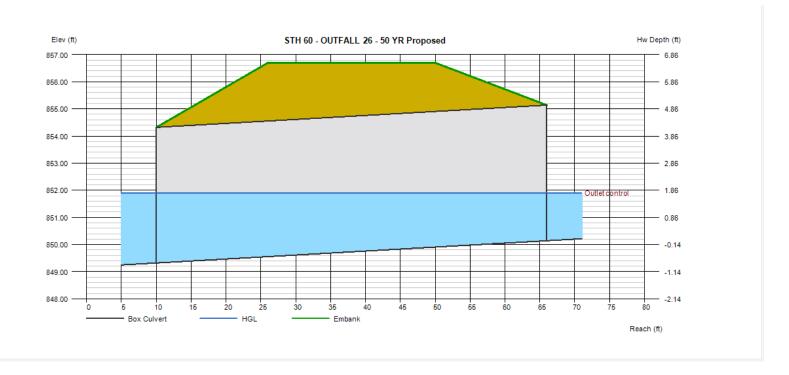
STH 60 - OUTFALL 26 - 50 YR Existing

Invert Elev Dn (ft)	= 849.32	Calculations	
Pipe Length (ft)	= 56.00	Qmin (cfs)	= 5.40
Slope (%)	= 1.46	Qmax (cfs)	= 5.40
Invert Elev Up (ft)	= 850.14	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 60.0	. ,	, ,
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 5.40
No. Barrels	= 2	Qpipe (cfs)	= 5.40
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.13
Culvert Entrance	= 0D wingwall flares	Veloc Up (ft/s)	= 0.19
Coeff. K,M,c,Y,k	= 0.061, 0.75, 0.0423, 0.82, 0.7	HGL Dn (ft)	= 851.90
		HGL Up (ft)	= 851.90
Embankment		Hw Elev (ft)	= 851.90
Top Elevation (ft)	= 856.70	Hw/D (ft)	= 0.35
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00	-	
Crest Width (ft)	= 20.00	-	



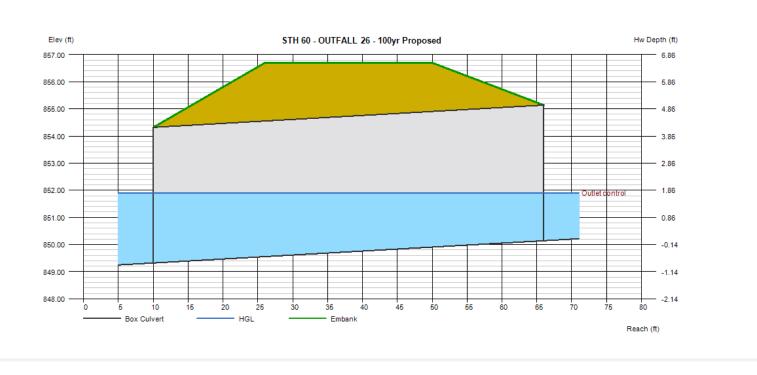
STH 60 - OUTFALL 26 - 50 YR Proposed

Invert Elev Dn (ft)	= 849.32	Calculations	
Pipe Length (ft)	= 56.00	Qmin (cfs)	= 5.78
Slope (%)	= 1.46	Qmax (cfs)	= 5.78
Invert Elev Up (ft)	= 850.14	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 60.0		
Shape	= Box	Highlighted	
Span (in)	= 96.0	Qtotal (cfs)	= 5.78
No. Barrels	= 2	Qpipe (cfs)	= 5.78
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Flared Wingwalls	Veloc Dn (ft/s)	= 0.14
Culvert Entrance	= 0D wingwall flares	Veloc Up (ft/s)	= 0.21
Coeff. K,M,c,Y,k	= 0.061, 0.75, 0.0423, 0.82, 0.7	HGL Dn (ft)	= 851.90
		HGL Up (ft)	= 851.90
Embankment		Hw Elev (ft)	= 851.90
Top Elevation (ft)	= 856.70	Hw/D (ft)	= 0.35
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



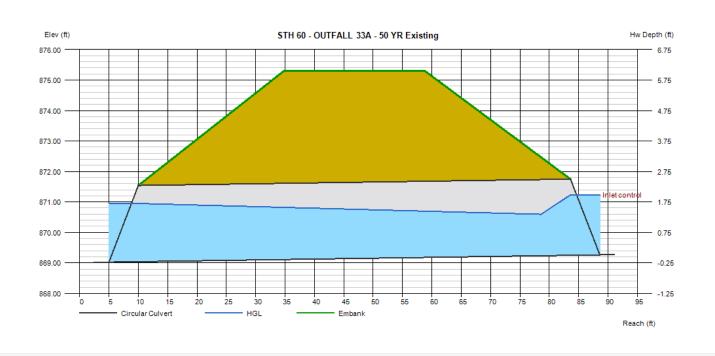
Wednesday, Mar 18 2015

STH 60 - OUTFALL 26 - 100yr Proposed



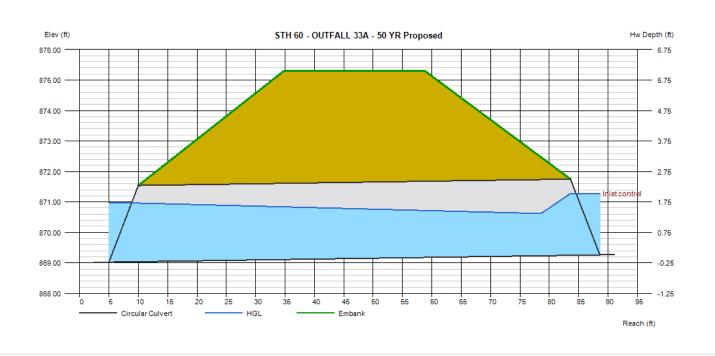
STH 60 - OUTFALL 33A - 50 YR Existing

Invert Elev Dn (ft)	= 869.04	Calculations	
Pipe Length (ft)	= 73.60	Qmin (cfs)	= 15.32
Slope (%)	= 0.29	Qmax (cfs)	= 15.32
Invert Elev Up (ft)	= 869.25	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 15.32
No. Barrels	= 1	Qpipe (cfs)	= 15.32
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 3.81
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 5.83
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 870.95
		HGL Up (ft)	= 870.57
Embankment		Hw Elev (ft)	= 871.23
Top Elevation (ft)	= 875.30	Hw/D (ft)	= 0.79
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



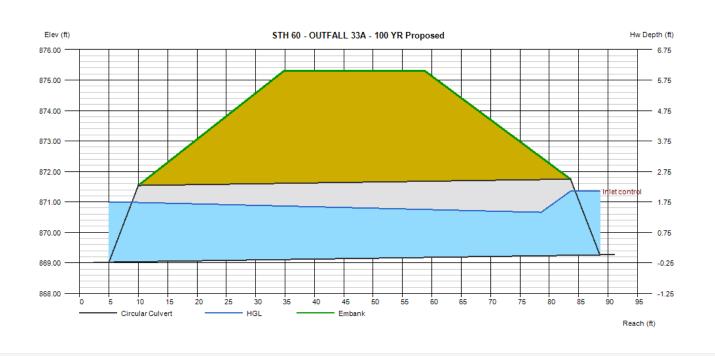
STH 60 - OUTFALL 33A - 50 YR Proposed

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft)	= 869.04 = 73.60 = 0.29 = 869.25	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 15.89 = 15.89 = (dc+D)/2
Rise (in) Shape	= 30.0 = Circular	Highlighted	
Span (in) No. Barrels n-Value Culvert Type Culvert Entrance Coeff. K,M,c,Y,k	= 30.0 = 1 = 0.024 = Circular Corrugate Metal Pipe = Mitered to slope (C) = 0.021, 1.33, 0.0463, 0.75, 0.7	Qtotal (cfs) Qpipe (cfs) Qovertop (cfs) Veloc Dn (ft/s) Veloc Up (ft/s) HGL Dn (ft)	= 15.89 = 15.89 = 0.00 = 3.92 = 5.90 = 870.96
Embankment Top Elevation (ft) Top Width (ft) Crest Width (ft)	= 875.30 = 24.00 = 20.00	HGL Up (ft) Hw Elev (ft) Hw/D (ft) Flow Regime	= 870.60 = 871.28 = 0.81 = Inlet Control



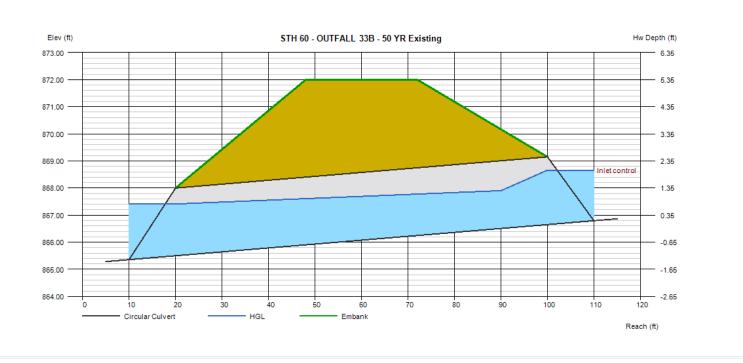
STH 60 - OUTFALL 33A - 100 YR Proposed

Invert Elev Dn (ft)	= 869.04	Calculations	
Pipe Length (ft)	= 73.60	Qmin (cfs)	= 16.84
Slope (%)	= 0.29	Qmax (cfs)	= 16.84
Invert Elev Up (ft)	= 869.25	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 16.84
No. Barrels	= 1	Qpipe (cfs)	= 16.84
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 4.11
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 6.03
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 870.98
		HGL Up (ft)	= 870.64
Embankment		Hw Elev (ft)	= 871.35
Top Elevation (ft)	= 875.30	Hw/D (ft)	= 0.84
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



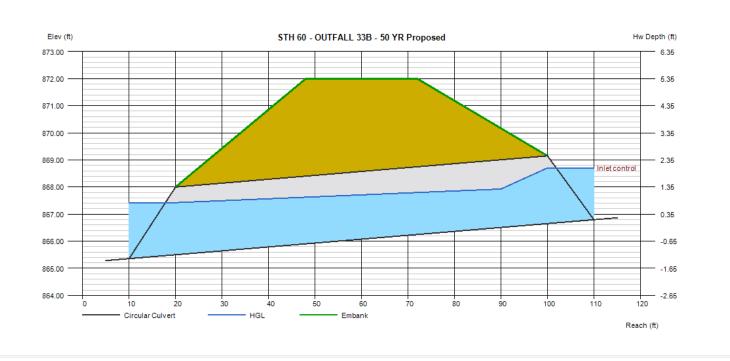
STH 60 - OUTFALL 33B - 50 YR Existing

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 865.50 = 80.00 = 1.44 = 866.65 = 30.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 15.39 = 15.39 = (dc+D)/2
Shape	= Circular	Highlighted	
Span (in) No. Barrels n-Value Culvert Type Culvert Entrance	 = 30.0 = 1 = 0.024 = Circular Corrugate Metal Pipe = Mitered to slope (C) 	Qtotal (cfs) Qpipe (cfs) Qovertop (cfs) Veloc Dn (ft/s) Veloc Up (ft/s)	= 15.39 = 15.39 = 0.00 = 3.82 = 5.84
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft) HGL Up (ft)	= 867.41 = 867.97
Embankment		Hw Elev (ft)	= 868.66
Top Elevation (ft) Top Width (ft) Crest Width (ft)	= 872.00 = 24.00 = 20.00	Hw/D (ft) Flow Regime	= 0.80 = Inlet Control



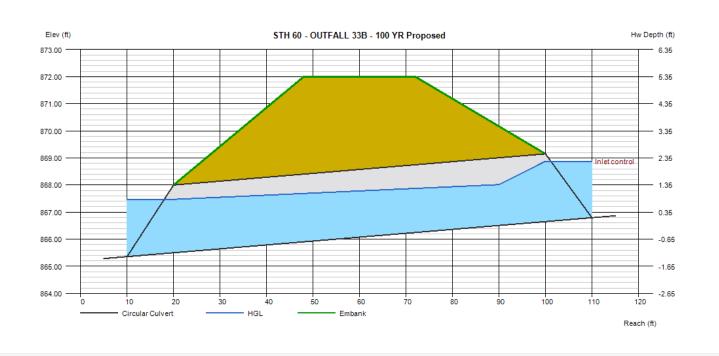
STH 60 - OUTFALL 33B - 50 YR Proposed

Invert Elev Dn (ft)	= 865.50	Calculations	
Pipe Length (ft)	= 80.00	Qmin (cfs)	= 15.96
Slope (%)	= 1.44	Qmax (cfs)	= 15.96
Invert Elev Up (ft)	= 866.65	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 15.96
No. Barrels	= 1	Qpipe (cfs)	= 15.96
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 3.94
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 5.92
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 867.42
		HGL Up (ft)	= 868.00
Embankment		Hw Elev (ft)	= 868.70
Top Elevation (ft)	= 872.00	Hw/D (ft)	= 0.82
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



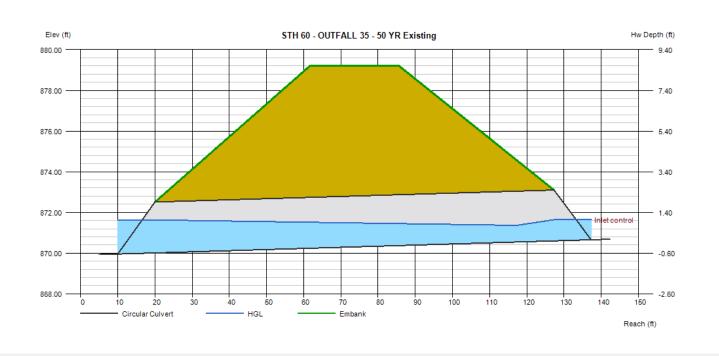
STH 60 - OUTFALL 33B - 100 YR Proposed

Invert Elev Dn (ft)	= 865.50	Calculations	
Pipe Length (ft)	= 80.00	Qmin (cfs)	= 18.16
Slope (%)	= 1.44	Qmax (cfs)	= 18.16
Invert Elev Up (ft)	= 866.65	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 18.16
No. Barrels	= 1	Qpipe (cfs)	= 18.16
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 4.37
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 6.19
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 867.47
		HGL Up (ft)	= 868.09
Embankment		Hw Elev (ft)	= 868.88
Top Elevation (ft)	= 872.00	Hw/D (ft)	= 0.89
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 35 - 50 YR Existing

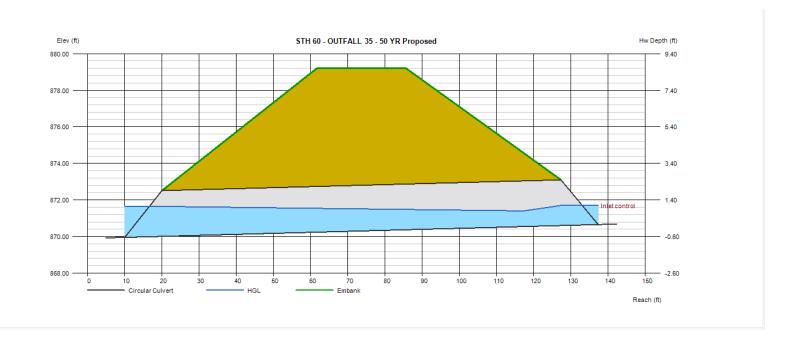
Invert Elev Dn (ft)	= 870.01	Calculations	
Pipe Length (ft)	= 107.30	Qmin (cfs)	= 4.99
Slope (%)	= 0.55	Qmax (cfs)	= 4.99
Invert Elev Up (ft)	= 870.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 4.99
No. Barrels	= 1	Qpipe (cfs)	= 4.99
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 1.48
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 4.14
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 871.63
		HGL Up (ft)	= 871.34
Embankment		Hw Elev (ft)	= 871.64
Top Elevation (ft)	= 879.20	Hw/D (ft)	= 0.42
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



Thursday, Nov 21 2019

STH 60 - OUTFALL 35 - 50 YR Proposed

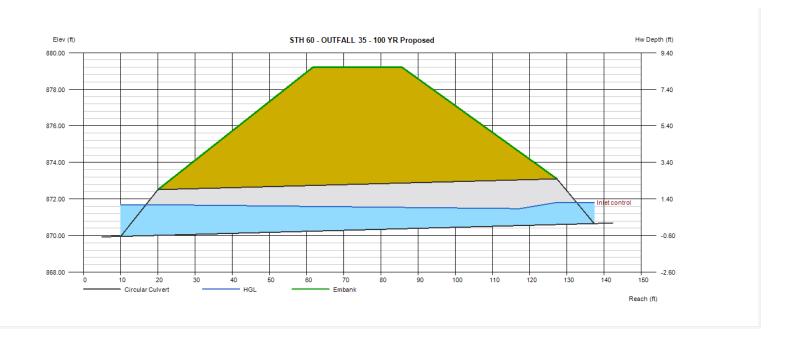
Invert Elev Dn (ft)	= 870.01	Calculations	
Pipe Length (ft)	= 107.30	Qmin (cfs)	= 5.51
Slope (%)	= 0.55	Qmax (cfs)	= 5.51
Invert Elev Up (ft)	= 870.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 5.51
No. Barrels	= 1	Qpipe (cfs)	= 5.51
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 1.62
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 4.25
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 871.65
		HGL Up (ft)	= 871.38
Embankment		Hw Elev (ft)	= 871.70
Top Elevation (ft)	= 879.20	Hw/D (ft)	= 0.44
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



Friday, Nov 22 2019

STH 60 - OUTFALL 35 - 100 YR Proposed

Invert Elev Dn (ft)	= 870.01	Calculations	
Pipe Length (ft)	= 107.30	Qmin (cfs)	= 6.56
Slope (%)	= 0.55	Qmax (cfs)	= 6.56
Invert Elev Up (ft)	= 870.60	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 30.0		
Shape	= Circular	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 6.56
No. Barrels	= 1	Qpipe (cfs)	= 6.56
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 1.88
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 4.47
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 871.68
		HGL Up (ft)	= 871.45
Embankment		Hw Elev (ft)	= 871.81
Top Elevation (ft)	= 879.20	Hw/D (ft)	= 0.48
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



STH 60 - OUTFALL 37 - 50 YR Existing

Invert Elev Dn (ft)	= 863.13	Calculations	
Pipe Length (ft)	= 106.70	Qmin (cfs)	= 7.44
Slope (%)	= 0.09	Qmax (cfs)	= 7.44
Invert Elev Up (ft)	= 863.23	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 42.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 66.0	Qtotal (cfs)	= 7.44
No. Barrels	= 1	Qpipe (cfs)	= 7.44
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 0.76
Culvert Entrance	= Groove end projecting (H)	Veloc Up (ft/s)	= 0.84
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 865.16
		HGL Up (ft)	= 865.19
Embankment		Hw Elev (ft)	= 865.20
Top Elevation (ft)	= 871.40	Hw/D (ft)	= 0.56
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



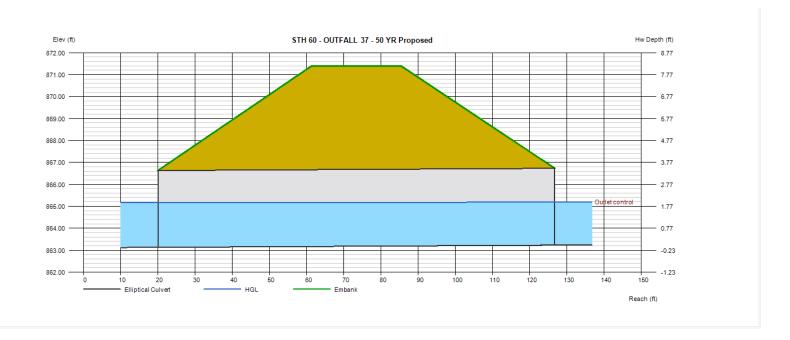
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Nov 22 2019

STH 60 - OUTFALL 37 - 50 YR Proposed

Invert Elev Dn (ft)	= 863.13	Calculations	
Pipe Length (ft)	= 106.70	Qmin (cfs)	= 7.86
Slope (%)	= 0.09	Qmax (cfs)	= 7.86
Invert Elev Up (ft)	= 863.23	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 42.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 66.0	Qtotal (cfs)	= 7.86
No. Barrels	= 1	Qpipe (cfs)	= 7.86
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 0.81
Culvert Entrance	= Groove end projecting (H)	Veloc Up (ft/s)	= 0.89
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 865.16
		HGL Up (ft)	= 865.19
Embankment		Hw Elev (ft)	= 865.20
Top Elevation (ft)	= 871.40	Hw/D (ft)	= 0.56
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		



Friday, Nov 22 2019

STH 60 - OUTFALL 37 - 100 YR Proposed

Invert Elev Dn (ft)	= 863.13	Calculations	
Pipe Length (ft)	= 106.70	Qmin (cfs)	= 9.74
Slope (%)	= 0.09	Qmax (cfs)	= 9.74
Invert Elev Up (ft)	= 863.23	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 42.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 66.0	Qtotal (cfs)	= 9.74
No. Barrels	= 1	Qpipe (cfs)	= 9.74
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 1.00
Culvert Entrance	= Groove end projecting (H)	Veloc Up (ft/s)	= 1.00
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 865.23
		HGL Up (ft)	= 865.33
Embankment		Hw Elev (ft)	= 865.35
Top Elevation (ft)	= 871.40	Hw/D (ft)	= 0.61
Top Width (ft)	= 24.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 20.00		

