SHOULDER CORING DETAIL 19.2' (21.2' if beam-sinard required) STA: 10+000 TO 22+245 STH \$ 178 FINISHED 5.9 TO SUBGRADE SHOULDER POINT VARIES -SHOULDER CORING MATERIAL (10.2' if beam ground/required) EXISTING PAVEMENT 100-000 SALVAGED TOPSOIL 3:1 MAX 60.61.62.63 BORROW OR MATI EXISTING THEF SHOULDER FROM DITCHING (VARIABLE WIDTH) ŝ 58 REMOVE / SHOULDER TO A DEPTH 0F 250 WHERE REQUIRED. EXCAVATED NOTE: THIS OPERATION MUST BE COMPLETED ശ്ശ് MATERIAL WILL BE USED TO WIDEN ADDITI PRIOR TO THE MILL & RELAY OPERATION. SLOPE. ADDITIONAL MATERIAL SHALL BE F FOR AS COMMON EXCAVATION FROM GRADING AREAS OR NOTE/ BORROW EXCAVATION. AND AT THE DIRECTION OF THE MISCELLANEOUS QUANTITIES AND AT THE DIRECTION OF THE PROJECT ENGINEER, CRUSHED ACGREGATE BASE COURSE SHALL BE PLACED ON THE PAVEMENT DUST PRIOR TO THE MILL AND RELAY OPERATION TO HELP ADJUST PROFILE IRREGULARITIES. 889 - 890 H -794-796 Rt. 947 Rt 799 - 802 Rt. ~ 1035-1039 Rt. ~ 999 It. ~ 805 - 806 Rt. 102-1103 Rt. 1048-1050 Rt. 1056 - 1060 Rt. -809 - 810 Rt. 1110 Rt. -814-821 Rt. 810 Lt. 911 Rt 816-817 H. ~ Ë Ř ZONE 959-96114. 791 14 ej, 83 963-96914. 797 H. 2 1075-1083 H. 905-906 1t. 8 1089 - 1107 1t. 911-913 Ht. 949-956 H.DITCHING TYPICAL DETAIL 5.6.7.8. 9.10.11.12.13. 4. 15. 16. 17.18.19.20.21.22. 29 EXISTING GROUND -6-6-MIN. PAID AS COMMON EXC. ABOVE 2 TO DITCH BOTTOM . 1.2.3. From Project 8580-00-70 NOTE: INSLOPES AND BACKSLOPES MAYBE ADJUSTED BY PROJECT ENGINEER. 8 LEVELS TYPICAL SECTIONS - S.T.H. 40 HWY: S.T.H. 40 SCALE: 1: J:2.1 85800000:8580TYP.DGN





























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CORRESPONDENCE/MEMORANDUM DISTRICT #6

Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: **PAVEMENT DESIGN REPORT** Approval Letter

> Project I.D. 8600-02-01 Chippewa Falls - Cornell Road Jim Falls - CTH R STH 178 Chippewa County

Upon review of the attached pavement design documentation, the pavement type selection recommendations are approved for the above mentioned project segments.

Reviewed:

7/14/98

Richard J. Shermo, P.E. Date District #6 Area Supv.-Project Development Section

Approved:

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

COMMENTS Have some concern about the Slight horizontal alignment "shifts" which puts New & over the old the line. Rendy, can you set up meeting so the 4 of us can RJS 7/16/98 Weakot direuss? 3 MSO 7/23 MMH 7/23 '2+ →RWL

COMMENTS

CORRESPONDENCE/MEMORANDUM DISTRICT #6

Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: **PAVEMENT DESIGN REPORT** Approval Letter

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COMMENTS

Richard J. Shermo, P.E. Date District #6 Area Supv.-Project Development Section

Approved:

COMMENTS

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

CORRESPONDENCE/MEMORANDUM

Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: Pavement Design Report Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

EXECUTIVE SUMMARY

This report makes the following recommendations for the proposed reconstruction project.

| LOCATION | PAVEMENT STRUCTURE | THICKNESS |
|---------------------------------|---------------------------------|---|
| STH 178-mainline & bypass lanes | Asphalt/ Base Course/ Sand Lift | 125mm/275mm/275mm (5") /(11") /(11") |
| Side Roads >500 ADT | Asphalt/ Base Course | 100mm/300mm (4") /(12") |
| Side Roads <500 ADT | Asphalt/Base Course | 75mm /225mm (3") /(9") |

Type MV Asphaltic Concrete Pavement mix with PG grade 58-28 should be used for this project. It is anticipated that by the time this plan is let to bid, a different PG graded oil could be the standard. The designer should coordinate the special provisions to reflect the correct AC type.

The 125mm(5") asphalt pavement should be constructed with two lower layers totaling $85\text{mm}(3 \frac{1}{2"})$ and a upper layer of $40\text{mm}(1 \frac{1}{2"})$. The 100mm(4") asphalt pavement should be constructed with a 50mm(2") lower layer and a 50mm(2") upper layer. The 75mm(3") asphalt pavement should be constructed with two layers.

The sand lift should be specified to meet Grade #1 requirements as specified in the Standard Specifications Section 209.2.2 for granular backfill.

EXISTING CONDITIONS

This 11.9km(7.4 mile) project involves the portion of STH 178 from the intersection of CTH Y at Jim Falls northerly along the Chippewa River to the intersection of CTH R. Due to a high accident rate, as stated in the CDR, the roadway will be reconstructed to C3 standards. This roadway is not being reconstructed due to excessive pavement failures or deficiencies. It appears that the roadway was last resurfaced in 1981 with a maintenance type overlay. The 1996 PDI ranged from 28-75 for this section. The 1997 IRI ranged from 1.4-3.6.

In 1993, the roadway core was investigated for a resurfacing type project. Since that time, the concept was revised to a reconstruct type improvement. The 1993 borings are located in the technical services project records.





TRAFFIC PROJECTIONS

The construction year-0 year ADT is 2000 and the 20 year ADT is projected to be 2400.

Truck percentages are as follows:

| TRUCK TYPE | | <u>%</u> |
|---|--------|--|
| 2D 3AX 2SI,2S2 3-S2 DBL.BTM | • • | 3.6 1.3 0.8 2.3 <u>0.0</u> |
| | TOTAL | 8.0 |

PROPOSED IMPROVEMENT

This project is currently scheduled for a reconstruct(RECST) type improvement. The existing roadway will be reconstructed to C3 standards which will include adjustments to the horizontal and vertical alignments.

SOIL ENGINEERING FACTORS

Over the length of this project, many different soil series are located under the roadway. The roadway core itself, as revealed in the 1993 roadway borings, has various amounts of silt and topsoil present along with some granular material in some of the fill locations. With the existing roadway material varying from moist to wet, construction could be a problem. With the existing silty materials in mind, it was agreed to with the Soils Engineer- Lary Hyland that a sand lift would be the best choice in this situation. For further discussion see the "alternative evaluated section". The DGI recommended for this roadway is 14 with a soil support value of 4.0. At the time of this report, due to the uncertainty of the horizontal and vertical alignment only a preliminary soils analysis has been completed.

FRICTION CHARACTERISTICS

The aggregate is expected to be igneous with 0% dolomite and a 20% L.A. wear resulting in a friction number of 44 and 51 for the PCC. Friction is not expected to be a problem.

ALTERNATIVES EVALUATED and RECOMMENDATIONS

Alternative Discussion

Initially, this segment of roadway was scheduled for a maintenance type overlay in 1998. That project was scrapped and the roadway segment is now being evaluated as a reconstruct to C3(100KM/60MPH) standards. In January 1997, the project was explained to me as a typical shoulder widening project on the south end with some short segments of relocation from the middle of the project northward to CTH R. Since that time, evaluation by the development staff has led to a concept of a total reconstruction.

I have numerous concerns that need to be addressed. The horizontal alignment, provided at the time of this report, continually drifts on and off the centerline of the existing road core in a range of 0-8 feet(0-2.5m). We have had past mid lane failures in minor grading areas when part of the old core supports the new lane and new material is added adjacent to support the remaining lane. Besides the obvious heave potential of the different materials, differential settlement occurs in the new material due to different compaction levels of the new material versus the old road core. As shown on the plan sheets and preliminary sections, in many cases, the subgrade point is being moved out over wet silty marshy material in the old ditches. Also in many locations, water is within 2-3 feet of the pavement surface. At this point in the design process, I can only assume that the designer will follow through with his/her responsibility to provide information to and coordinate with the district Soils Engineer to identify and treat these problem areas once the final horizontal and vertical alignment is chosen. In past situations of widening over old ditches, these areas have either been excavated and back-filled or a grid/back-fill combination was used. The high water table is a separate issue, as obviously it is hard to construct a stable subgrade within 1-2 feet of the existing water elevation. There is a reasonable chance that the asphalt/base/sand lift pavement will not perform in this situation . The designer should remember that a sand lift or breaker run platform will typically push the subgrade to 2 feet or greater below the finished profile.

Alternative Discussion-cont.

On other projects/roadways of this type, past experience had led to a district sequence of operations where the horizontal alignment is left in place and the shoulders are widened and raised to the existing profile. If a sag vertical deficiency exists in this area we will typically gravel lift up to a foot to improve the profile. Crest and sag verticals are routinely excepted to standards of 40 mph if there is no accident history at that location. After the widening or lifting is completed the traveled way surface is addressed with some type of overlay or mill/pulverize & relay and overlay combination, always taking care to remain in the middle of the old roadway core. We typically do experience some shoulder distortion but it is not critical to the performance of the pavement. Besides achieving pavement performance, this operation also has the benefit of providing adequate local access because, typically 2 lane traffic can be provided in the off hours and on weekends during the life of the project.

With reconstruction of the existing STH 178 roadway the project option chosen versus the above mentioned scenario, local access and staging of construction activities will both play major roles in the plan development. Since local access will need to be provided, I am assuming a grading operation will need to be completed one half at a time with excavation, EBS, back-fill, borrow, sand lift and base course progressing down the roadway as access permits. The relocation areas are typically completed separately with the old road in these relocated areas being obliterated at the end. For the sand lift to perform in the pavement structure, the sand cannot be placed on a rutted un-rolled subgrade. This typically requires the contractor to exercise care in the placing of the lift material. Some type of drain will be required at the low points in the sand lift profile. A breaker run was not chosen due the availability of local materials.

With this type of work, it is beneficial to work during the dry part of the summer. Even with these precautions, there is a reasonable chance that stage construction grading might not be completed in one year. Soft spots in the base could be common place under the reconstruct option. If the base course and the two lower layers were placed in year one, the surface layer could be placed the following year. This approach would allow some repair of the broken up areas prior to the final surface being placed.

SUMMARY OF COSTS-----LCCA

A twenty year service life was used.

The first alternative is : 175mm(7") PCC over 150mm(6") base over sand lift: \$219008 per KM for initial construction cost

\$ 11463 per KM for Equivalent Uniform Annual Cost

The second alternative is : 125mm(5") AC over 275mm(11") base course over 275mm(11") sand lift:

\$155257 per KM for initial construction cost

\$ 9759 per KM for Equivalent Uniform Annual Cost

The third alternative is : 140mm(5 ¹/₂")AC over 300(12") base course * \$157763 per KM for initial construction cost \$ 9921 per KM for Equivalent Uniform Annual Cost

* Not recommended due to sand lift requirement. For information purposes only

RECOMMENDATIONS

| LOCATION | PAVEMENT STRUCTURE | THICKNESS |
|---------------------------------|---------------------------------|---|
| STH 178-mainline & bypass lanes | Asphalt/ Base Course/ Sand Lift | 125mm/275mm/275mm (5") /(11") /(11") |
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The sand lift should be specified to meet Grade #1 requirements as specified in the Standard Specifications Section 209.2.2 for granular backfill.

The designer should use asphaltic surface items for incidental asphalt work such as driveways, safety islands, etc. as allowed under the 1997 Supplemental Specs.

Randy W. Luedtke, P.E.

PROPOSED TYPICAL $\begin{array}{c} \hline C/L \\ \hline \hline -3+ \\ \hline \hline \cdot \cdot \cdot \\ \hline 12' \\ \hline 12'$

RIGID PAVEMENT DESIGN WORKSHEET

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT DESIGN YEAR DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|--------------|
| 2,000 |
| 2022 |
| 2,400 |
| <u>0</u> .50 |
| 1.00 |
| 20.0 |
| 1,100 |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|--|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL'S |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 1.2 | 17 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.6 | 5 |
| 3S-2 | 2.3 | 1,100 | 25 | 1.6 | 40 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.1 | 0 |
| DESIGN LANE DAILY ESAL's | 8.0 | | | | 74 |
| DESIGN LANE TOTAL LIFE ESAL's | | | | T. T | 540,200 |

SOILS:

MODULUS OF SUBGRADE REACTION (K)

PAVEMENT THICKNESS TO BE USED

30

CALCULATED PAVEMENT THICKNESS

THICKNESSES:



FLEXIBLE PAVEMENT DESIGN WORKSHEET

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT **DESIGN YEAR** DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|-------|
| 2,000 |
| 2022 |
| 2,400 |
| 0.50 |
| 1.00 |
| 20.0 |
| 1,100 |
| |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL's |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 0.8 | 11 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.5 | 4 |
| 3S-2 | 2.3 | 1,100 | 25 | 0.9 | 23 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.0 | 0 |
| DESIGN LANE DAILY ESAL'S | 8.0 | | | | 50 |
| DESIGN LANE TOTAL LIFE ESAL'S | | | | | 365,000 |

SOILS:

DESIGN GROUP INDEX SOIL SUPPORT VALUE FROST INDEX



DESIGN - SN VALUE & MIX TYPE:

SERVICEABILITY INDEX REQUIRED SN VALUE

ASPHALT MIX TYPE: MV 3.0

ALTERNATE DESIGN:

3.49

| | 1 | Asphalt/base/sa | and | Asphalt/base | | | |
|----------------------------|-----------|-----------------|------|--------------|---------|------|--|
| LAYER | THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN | |
| SURFACE: | | SURFACE | | | SURFACE | | |
| ASPHALTIC CONCRETE | 125 | 0.0173 | 2.16 | 140 | 0.0173 | 2.42 | |
| EXISTING ASPHALT | | 0.0100 | 0.00 | | | 0.00 | |
| BASE COURSE: | BAS | E | | | BASE | | |
| CRUSHED AGG. BASE COURSE | 275 | 0.0039 | 1.07 | 300 | 0.0039 | 1.17 | |
| OPEN GRADED BASE COURSE #1 | | | 0.00 | | | 0.00 | |
| OPEN GRADED BASE COURSE #2 | | | 0.00 | | | 0.00 | |
| EXISTING BASE | | 0.0039 | 0.00 | | 0.0039 | 0.00 | |
| EXISTING AC | | | 0.00 | | | 0.00 | |
| PULVERIZED AC | | | 0.00 | | | 0.00 | |
| EXISTING PCC | | | 0.00 | | | 0.00 | |
| RUBBLIZED PCC | | | 0.00 | | | 0.00 | |
| CRACK (BREAK) & SEAT PCC | | | 0.00 | | | 0.00 | |
| SUBBASE COURSE: | SUBBA | SE | | | SUBBASE | | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 | |
| BREAKER RUN | | | 0.00 | | | 0.00 | |
| GRANULAR SUBBASE | 275 | 0.0012 | 0.33 | | | 0.00 | |
| EXISTING SAND LIFT | | 0.0025 | 0.00 | | 0.0025 | 0.00 | |
| TOTAL SN VALUE | | | 3.57 | | | 3.59 | |

FLEXIBLE PAVEMENT DESIGN

ALTERNATE DESIGN:

| | Existing Structu | re | | | |
|-----------|------------------|---|--|---|---|
| THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN |
| | SURFACE | | | Protection and the second second second | |
| 125 | 0.0173 | 2.16 | | CONTRACTOR CONTRACTOR | 0.00 |
| | | 0.00 | | | 0.00 |
| | BASE | | | BASE | |
| | | 0.00 | | 0.0039 | 0.00 |
| | | 0.00 | | | 0.00 |
| | | 0.00 | | | 0.00 |
| 125 | 0.0039 | 0.49 | | | 0.00 |
| | | 0.00 | | | 0.00 |
| | | 0.00 | i i | | 0.00 |
| | | 0.00 | | | 0.00 |
| | | 0.00 | | | 0.00 |
| | | 0.00 | | | 0.00 |
| | SUBBASE | | 1 | SUBBASE | |
| | | 0.00 | | | 0.00 |
| | | 0.00 | | | 0.00 |
| | | 0.00 | | 0.0012 | 0.00 |
| | 0.0025 | 0.00 | | | 0.00 |
| | | 2.65 | | | 0.00 |
| | THICKNESS 125 | THICKNESS COEFF. SURFACE 125 0.0173 BASE BASE 125 0.0039 125 0.0039 SUBBASE SUBBASE | THICKNESS COEFF. SN SURFACE 125 0.0173 2.16 125 0.0173 2.16 BASE 0.00 BASE 0.00 125 0.0039 0.00 125 0.0039 0.49 125 0.0039 0.49 0.00 0.00 0.00 125 0.0039 0.49 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.000 0.00 0.00 0.000 0.00 0.00 0.000 0.00 0.00 0.000 0.00 0.00 | THICKNESS COEFF. SN THICKNESS SURFACE 0.00 0.00 125 0.0173 2.16 BASE 0.00 0.00 BASE 0.00 0.00 125 0.0039 0.49 0.00 0.00 0.00 125 0.0039 0.49 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.000 0.00 0.00 0.000 0.00 0.00 0.000 0.00 0.00 0.000 0.00 | THICKNESS COEFF. SN THICKNESS COEFF. SURFACE SURFACE SURFACE 0.0173 0.00 0.0173 0.0039 0.0039 0.0039 0.00039 0.00039 0.00039 0.00039 0.000 0.0013 0.001 0.001 0.001 0.001 0.001 0.011 0.011 0.011 0.001 0.001 0.001 0.001 0.00112 0.001 0.00112 0.00112 0.001 0.00112 0.00112 0.001 0.00112 0.00112 0.001 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.00112 0.0 |

SN is Less Than SNreq'd

PAVEMENT SURFACE FRICTION DESIGN

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178

Chippewa



AGGREGATE PROPERTIES:

AC MIX AGGREGATES

PCC MIX AGGREGATES





% DOLOMITE % LA WEAR

> AC AGGREGATE SOURCE: PCC AGGREGATE SOURCE:

DESIGN:

ASPHALTIC SURFACE FORMULA

FN40 = 41.4 - 1.45 ln(LAVP) + 0.245(LAWEAR) - 0.00075(DOLOMITE) ^2

FN40 AT SPECIFIED PAVEMENT AGE43.7% PROBABILITY THAT CALCULATED VALUE IS < 35</td>7.9AGE (YR) WHEN FN40=35AGE>50

CONCRETE SURFACE FORMULA

 $\ln(FN40) = 3.99 - 0.0419\ln(LAVP) - 0.00129(DOLOMITE) + 0.00474(HV)$

| FN40 AT SPECIFIED PAVEMENT AGE | 50.9 |
|---|--------|
| % PROBABILITY THAT CALCULATED VALUE IS < 35 | <0.05% |
| AGE (YR) WHEN FN40=35 | AGE>50 |

BID ITEM COSTS

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| | BID ITEM | | UNIT |
|---|----------------|----------|------------------|
| BID ITEM | # | UNITS | COST |
| ASPHALTIC MATERIAL FOR TACK COAT | 40204 | L | \$1.00 |
| ASPHALTIC MATERIAL FOR PLANT MIXES | 40501 | Mg | \$155.00 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE HV | 40712 | Mg | \$22.00 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE MV | 40713 | Mg | \$16.50 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE LV | 40714 | Mg | \$16.50 |
| RECYCLED ASPHALTIC SURFACE, TYPE HV | 90381 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE MV | 90382 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE LV | 90383 | Mg | |
| CONCRETE PAVEMENT, 150 mm | 41506 | sm | \$13.50 |
| CONCRETE PAVEMENT, 175 mm | 41507 | sm ° | \$18.00 |
| CONCRETE PAVEMENT, 200 mm | 41508 | sm | \$18.00 |
| CONCRETE PAVEMENT, 225 mm | 41509 | sm | \$20.25 |
| CONCRETE PAVEMENT, 250 mm | 41510 | sm | |
| CONCRETE PAVEMENT, 275 mm | 41511 | sm | |
| CONCRETE PAVEMENT, 300 mm | 41512 | sm | |
| CONCRETE WIDENING | 41530 | sm | |
| CONTINUOUS CONCRETE PAV'T REINFORCEMENT | 41551 | sm | |
| PAVEMENT TIES | 41571 | EACH | \$5.00 |
| DOWEL BARS | 41572 | EACH | \$5.00 |
| CRUSHED AGGREGATE BASE COURSE | 30404 | Mg | \$7.75 |
| OPEN GRADED BASE COURSE #1 | 30418 | Mg | \$9.00 |
| OPEN GRADED BASE COURSE #2 | 30420 | Mg | \$9.00 |
| ASPHALTIC BASE COURSE | 30601 | Mg | |
| ASPHALTIC BASE COURSE WIDENING | 30606 | Mg | |
| CONCRETE BASE COURSE CONCRETE BASE COURSE WIDENING | 30706-9 | sm | |
| BREAKER RUN | 30751 | sm Ma | 00 70 |
| GRANULAR SUBBASE COURSE | 30426 21201 | Mg | \$7.00 \$3.30 |
| MILL AND RELAY ASPHALTIC CONCRETE PAVEMENT | 21201 | cm | \$3.30 \$0.86 |
| SALVAGED ASPHALTIC PAVEMENT | 41010 | sm Mg | <u>au.au</u> |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | 41020 | Mg | \$7.72 |
| ASPHALTIC SURFACE, PATCHING | 41102 | Mg | φ1.74 |
| PULVERIZING ASPHALTIC CONCRETE PAVEMENT | 41102 | sm | \$0.70 |
| BASE PATCHING, ASPHALTIC | 30810 | sm | |
| BASE PATCHING, CONCRETE | 30820 | sm | \$40.95 |
| CRACKING AND SEATING CONCRETE PAVEMENT | 41040 | sm | ψ+0.55 |
| BREAKING AND SEATING CONCRETE PAVEMENT | +10+0 | sm | |
| CONCRETE PAVEMENT REPAIR | 41574 | cm | \$183.00 |
| CONTINUOUS DIAMOND GRINDING | 41576 | sm | \$2.69 |
| RUBBLIZING CONCRETE PAVEMENT | +10/0 | sm | \$2.00 |
| CONCRETE CURB & GUTTER, 750 mm, TYPE A | 60123 | m | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE D | 60133 | m | |
| GEOTEXTILE FABRIC, TYPE DF | 64503 | sm | \$1.20 |
| PIPE UNDERDRAIN, 150 mm | 61201 | m | \$4,43 |
| PIPE UNDERDRAIN, UNPERFORATED, 150 mm | 61211 | . m | \$22.15 |
| R.C. APRON ENDWALLS FOR UNDERDRAIN | 61254 | EACH | \$125.00 |
| REMOVING PAVEMENT | 20401 | sm | ****** |
| GEO-GRID | '90xxx | sm | \$1.75 |
| | | | |

ALTERNATE DESCRIPTION WORKSHEET

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| PARAMETER | UNITS | ALT 1 VALUE | ALT 2 VALUE | ALT 3 VALUE | ALT 4 VALUE | ALT 5 VALUE | ALT 6 VALUE |
|--|--------------|----------------|----------------|----------------|----------------|----------------|----------------|
| RURAL OR URBAN PROJECT | R/U | ALUL | | VALUE | VALUE | VALUE | VALUE |
| ROADWAY WIDTH | m | 10.80 | 10.80 | 10.80 | | | |
| PAVEMENT STRUCTURE WIDTH | m | 7.20 | | | | | |
| TOTAL PAVED SHOULDER WIDTH | m | 1.80 | 1.80 | 1.80 | | | |
| CONCRETE RDWY PAVEMENT THICKNESS | mm | 175 | | | | | |
| CONCRETE SHOULDER THICKNESS | mm | 175 | | | | | |
| AC RDWY PAVEMENT MIX TYPE | HV/MV/LV | | MV | MV | | | |
| TOTAL AC RDWY PAVEMENT THICKNESS | mm | | 125 | 140 | 125 | | |
| VIRGIN AC RDWY PAVEMENT THICKNESS | mm | | 125 | | | | |
| % OF ASPHALT CEMENT USED RECYCLED AC RDWY PAVEMENT THICKNESS | % | - | 5.0 | 6.0 | | | |
| % OF ASPHALT CEMENT USED | % | - | | | | | · |
| % OF ASPHALT CEMENT USED % RAP | % | | | | | | |
| AC SHOULDER PAVEMENT MIX TYPE | HV/MV/LV | | MV | mv | | | |
| TOTAL AC SHOULDER PAVEMENT THICKNESS | mm | | 125 | 140 | | | |
| VIRGIN AC SHOULDER THICKNESS | mm | | 125 | 140 | | | |
| RECYCLED AC SHOULDER THICKNESS | mm | | | | | | |
| % OF ASPHALT CEMENT USED | % | | 6.0 | 6.0 | | | |
| ASPHALTIC CONCRETE PAVEMENT WT. | kg/sm/mm | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 | |
| TACK COAT COVERAGE WHICH LAYER IS THE DRAINAGE LAYER? | L/sm | 0.113 | 0.113 | 0.113 | 0.113 | | |
| CRUSHED AGG. BASE COURSE THICKNESS | 0-4 mm | 150.00 | 275.00 | 200.00 | 0 | | 0 |
| UNIT WT OF CABCI | Mg/cm | 150.00 | 275.00 2.4 | 300.00 | 0 | l | |
| OPEN GRADED BASE COURSE #1 THICKNESS | mm | 2.4 | 2.4 | 2.4 | 0 | | l |
| UNIT WT OF OGBC #1 | Ma/cm | | ······ | l | v | | |
| OPEN GRADED BASE COURSE #2 THICKNESS | mm | | | 0 | 0 | | |
| UNIT WT OF OGBC #2 | Mg/cm | | | | | | |
| BREAKER RUN THICKNESS | mm | | 0 | 0 | 0 | | |
| UNIT WT OF BREAKER RUN | Mg/cm | | | | | | |
| ASPHALTIC STABILIZED B.C. THICKNESS | mm | | | | | | |
| % OF ASPHALTIC CEMENT USED UNIT WT OF AC STABILIZED BASE COURSE | % | | | | | | |
| P.C. STABILIZED BASE COURSE THICKNESS | Mg/cm mm | | | | | | ****** |
| UNIT WT OF PCC STABILIZED BASE COURSE | Mg/cm | | ******** | | | | |
| GRANULAR SUBBASE COURSE THICKNESS | mm | 275 | 275 | 0 | 0 | | |
| OTHER #1 (STRUCTURE WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| OTHER #2 (ROADWAY WIDTH) | mm | | | | | | |
| EXISTING PAVEMENT WIDTH | Mg/cm | | | | | | |
| EXISTING PAVEMENT WIDTH EXISTING PAVEMENT THICKNESS | m | | 6.70 | 6.70 | | | |
| % OF PROJECT LENGTH FOR CURB & GUTTER | % | | | | | | |
| TYPE OF CURB & GUTTER | A/D | | | | | | |
| % OF PROJECT LENGTH FOR GEOTEXTILE FABRIC | % | | | | | | |
| % OF PROJECT LENGTH FOR UNDERDRAINS | % | | | | | | |
| % OF PROJECT LENGTH FOR TACK COATING | % | | 66 | 66 | | | |
| TOTAL m2 OF CRCP STEEL REINFORCEMENT | sm | | | | | | |
| % OF PROJECT LENGTH FOR MILL & RELAY AC PAV'T | % | | | | | | |
| %OF PROJECT PAV'T AREA FOR AC SURF PATCHING %OF PROJECT LENGTH FOR PULVERIZING AC PAV'T | % | | | | | | |
| MILLING DEPTH | % | | | | | | |
| %OF PROJECT LENGTH FOR SALV AC PAV'T MILLING | % | | | | | | |
| %OF PROJECT LENGTH FOR SALV AC PAV'T | % | | | | | | |
| %OF PROJECT LENGTH FOR DIAMOND GRINDING | % | | | | | | |
| %OF PROJECT LENGTH FOR PCC PAV'T REPAIR | % | | | | | | |
| | EACH | | | | | | |
| #DOWELS PER PATCH JOINT | EACH | | | | | | |
| AVG. LENGTH OF PCC PATCH %OF PROJECT LENGTH FOR CRACK & SEAT | <u>m</u> | | | | | | |
| %OF PROJECT LENGTH FOR BREAK & SEAT | % | | | | | | |
| %OF PROJECT LENGTH FOR RUBBLIZING | <u>~~~</u> % | | | | | | |
| TOTAL AREA FOR ASPHALTIC BASE PATCHING | /8 sm | | | | | | |
| TOTAL AREA FOR CONCRETE BASE PATCHING | sm | | | | | | |
| TOTAL AREA FOR CONCRETE WIDENING | sm | | | | | | |
| TOTAL AREA FOR AC BASE COURSE WIDENING | sm | | | | | | |
| TOTAL AREA FOR PCC BASE COURSE WIDENING | sm | | | | | | |
| %OF PROJECT LENGTH FOR PAVEMENT REMOVAL | % | | | | | | |
| Ļ | | | | | | | |
| | | ····· | | | | | |
| ASE LAYER: (FOR QUANTITY CALCULATIONS) | | | | | | | |
| – NONE E – AC STABILIZED | Г | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |
| | | | | | | | |

| X – NONE | E – AC STABILIZI |
|-----------------|------------------|
| A – CABC | F - PC STABILIZ |
| B – OGBC #1 | g – Granular |
| C – OGBC #2 | H – OTHER #1 |
| D – BREAKER RUN | I – OTHER #2 |
| | |

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| STABILIZED | | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |
|------------|---------|-------|-------|-------|-------|-------|----------|
| STABILIZED | LAYER 1 | a | а | a | x | x | x |
| NULAR | LAYER 2 | g | g | x | x | x | x |
| ER #1 | LAYER 3 | X | x | x | x | X | X |
| R #2 | LAYER 4 | X | X | x | x | x | X |

ALTERNATE QUANTITIES AND COSTS

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

| | | ALTERNATI PCC | VE #1 | ALTERNAT Asphait/base/sand | E #2 | ALTERNATE #3 Asphalt/base | | |
|--------------------------------------|-------|------------------|--------------|-------------------------------|-------------------|------------------------------|-------------|--|
| PARAMETER | UNITS | QUANTITY | COST | QUANTITY | COST | QUANTITY | COST | |
| CONCRETE PAVEMENT (RDWY) | sm | 7,200.0 | \$129,600.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 1,800.0 | \$32,400.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 2.115.0 | \$34,897,50 | 2,368.8 | \$39.085.2 | |
| VIRGIN AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 528.8 | \$8,724.38 | 592.2 | \$9,771.3 | |
| RECYCLED AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| ASPHALT CEMENT | Mg | 0.0 | \$0.00 | 158.6 | \$24,586,88 | 177.7 | \$0.0 | |
| CRUSHED AGG. BASE COURSE | Mg | 5,658.0 | \$43,849.50 | 9,204.0 | \$71,331.00 | 10,239.4 | \$79,355.0 | |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$79,355.0 | |
| OPEN GRADED BASE COURSE #2 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | | |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| GRANULAR SUBBASE COURSE | cm | 3.987.5 | \$13,158.75 | 4.152.5 | \$13,703.25 | 0.0 | \$0.0 | |
| CURB & GUTTER | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| TYPE DF GEOTEXTILE FABRIC | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| 150 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 | |
| 150mm PIPE UNDERDRAINS, UNPERFORATED | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| APRON ENDWALLS FOR UNDERDRAINS | EACH | 0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| TACK COATING | L | 0.0 | \$0.00 | 2,013.7 | \$2,013.66 | 0 | \$0.0 | |
| MILL & RELAY AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | <u>\$2,013.66</u> | 2,013.7 | \$2,013.6 | |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| ASPHALTIC SURFACE PATCHING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| PULVERIZING AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONTINUOUS DIAMOND GRINDING | sm | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.0 | |
| CONCRETE PAVEMENT REPAIR | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CRCP REINFORCEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| PAVEMENT TIES | EACH | 0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| DOWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.0 | |
| CRACK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0 | \$0.0 | |
| BREAK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.0 | |
| RUBBLIZING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| ASPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | .0.0 | \$0.0 | |
| CONCRETE BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| ASPHALTIC BASE COURSE WIDENING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE BASE COURSE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| REMOVING PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| Cost Adjustment-see comps | | 0.0 | <u></u> | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| OTHER BASE #1 | Mg | 0.0 | | 0.0 | | | | |
| OTHER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | | |
| LTERNATIVE TOTAL | | | \$219,008.25 | | \$155,256.66 | | \$157,762.5 | |

| CONCRETE PAVEMENT (RDWY) S CONCRETE PAVEMENT (SHOULDERS) S VIRGIN AC PAVEMENT (RDWY) M VIRGIN AC PAVEMENT (SHOULDERS) M RECYCLED AC PAVEMENT (SHOULDERS) M RECYCLED AC PAVEMENT (SHOULDERS) M ASPHALT CEMENT M CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE M OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #2 M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CONCRETE BASE COURSE M CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS, UNPERFORATED m 150 mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | IITS m | Existing Structure QUANTITY | COST | 0 | | ALTERNATE #6 | | |
|--|-----------|--------------------------------|--------|----------|------------------|---------------|--------|--|
| CONCRETE PAVEMENT (SHOULDERS)sVIRGIN AC PAVEMENT (RDWY)MVIRGIN AC PAVEMENT (SHOULDERS)MRECYCLED AC PAVEMENT (SHOULDERS)MASPHALT CEMENTMCRUSHED AGG. BASE COURSEMOPEN GRADED BASE COURSE #1MOPEN GRADED BASE COURSE #1MOPEN GRADED BASE COURSE #2MBREAKER RUNMASPHALTIC BASE COURSEMCONCRETE BASE COURSEMCONCRETE BASE COURSEGCURB & GUTTERMTYPE DF GEOTEXTILE FABRICSI150 mm PIPE UNDERDRAINS, UNPERFORATEDM150mm PIPE UNDERDRAINS, UNPERFORATEDMMELL & RELAY AC PAVEMENTSALVAGED ASPHALTIC PAVEMENT, MILLINGMILL & RELAY AC PAVEMENTMSALVAGED ASPHALTIC PAVEMENT, MILLINGMBULVERIZING, OR DAVEMENTMBULVERIZING, OR DAVEMENTM | m | | COST | QUANTITY | COST | 0 QUANTITY | 0007 | |
| VIRGIN AC PAVEMENT (RDWY) M VIRGIN AC PAVEMENT (SHOULDERS) M RECYCLED AC PAVEMENT (RDWY) M RECYCLED AC PAVEMENT (SHOULDERS) M ASPHALT CEMENT M CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE M OPEN GRADED BASE COURSE M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CURB & GUTTER M TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS, UNPERFORATED M APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT M SALVAGED ASPHALTIC PAVEMENT, MILLING M SA | | 0.0 | \$0.00 | 0.0 | \$0.00 | | COST | |
| VIRGIN AC PAVEMENT (SHOULDERS) M RECYCLED AC PAVEMENT (RDWY) M RECYCLED AC PAVEMENT (SHOULDERS) M ASPHALT CEMENT M CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE M OPEN GRADED BASE COURSE M OPEN GRADED BASE COURSE M SREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CONCRETE BASE COURSE G CONCRETE BASE COURSE G CURB & GUTTER M TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS, UNPERFORATED M 150 mm PIPE UNDERDRAINS, UNPERFORATED M APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M SPHALTIC SURFACE PATCHING M | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| RECYCLED AC PAVEMENT (RDWY) M RECYCLED AC PAVEMENT (SHOULDERS) M ASPHALT CEMENT M CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CONCRETE BASE COURSE G CURB & GUTTER M TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS M 150 mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M SALVAGED ASPHALTIC PAVEMENT M SHLVERIZING OR ON WALLS FOR M | lg | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.00 | |
| RECYCLED AC PAVEMENT (SHOULDERS) M ASPHALT CEMENT M CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #1 M BREAKER RUN M ASPHALTIC BASE COURSE #2 M CONCRETE BASE COURSE M CONCRETE BASE COURSE SI CONCRETE BASE COURSE G CURB & GUTTER M TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS M 150 mm PIPE UNDERDRAINS, UNPERFORATED M APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M SPHALTIC SURFACE PATCHING M | lg | 0.0 | \$0.00 | 0.0 | \$0.00 \$0.00 | 0.0 | \$0.00 | |
| ASPHALT CEMENT M CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #1 M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE CI CURB & GUTTER T TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS M 150mm PIPE UNDERDRAINS, UNPERFORATED M APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | lg | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.00 | |
| CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #2 M BREAKER RUN M ASPHALTIC BASE COURSE M CONC RETE BASE COURSE M CONC RETE BASE COURSE SI GRANULAR SUBBASE COURSE CI CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAW TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | la | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CRUSHED AGG. BASE COURSE M OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #2 M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE CI CURB & GUTTER T TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS M 150mm PIPE UNDERDRAINS, UNPERFORATED M APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | a | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| OPEN GRADED BASE COURSE #1 M OPEN GRADED BASE COURSE #2 M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE M CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE G CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M SPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| OPEN GRADED BASE COURSE #2 M BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE SI GRANULAR SUBBASE COURSE CI CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 | |
| BREAKER RUN M ASPHALTIC BASE COURSE M CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE CI CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| ASPHALTIC BASE COURSE M CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE CI CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS,UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT,MILLING M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE BASE COURSE SI GRANULAR SUBBASE COURSE CI GRANULAR SUBBASE COURSE CI CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| GRANULAR SUBBASE COURSE CI CURB & GUTTER m TYPE DF GEOTEXTILE FABRIC si 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EAV TACK COATING L MILL & RELAY AC PAVEMENT Si SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CURB & GUTTER In TYPE DF GEOTEXTILE FABRIC sit 150 mm PIPE UNDERDRAINS In 150mm PIPE UNDERDRAINS, UNPERFORATED In APRON ENDWALLS FOR UNDERDRAINS EAV TACK COATING L MILL & RELAY AC PAVEMENT Sr SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| TYPE DF GEOTEXTILE FABRIC SI 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS,UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT,MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| 150 mm PIPE UNDERDRAINS m 150mm PIPE UNDERDRAINS, UNPERFORATED m APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT Sr SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| 150mm PIPE UNDERDRAINS, UNPERFORATED In APRON ENDWALLS FOR UNDERDRAINS EA TACK COATING L MILL & RELAY AC PAVEMENT SI SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| APRON ENDWALLS FOR UNDERDRAINS EAU TACK COATING L MILL & RELAY AC PAVEMENT SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| TACK COATING L MILL & RELAY AC PAVEMENT sr SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M PULL VERTION CONDUCTION M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| MILL & RELAY AC PAVEMENT Sr SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | UH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 | |
| SALVAGED ASPHALTIC PAVEMENT, MILLING M SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| SALVAGED ASPHALTIC PAVEMENT M ASPHALTIC SURFACE PATCHING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONTINUOUS DIAMOND CONTINUES | <u>n</u> | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONTINUOUS DIAMOND GRINDING SI | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | | |
| CONCRETE PAVEMENT REPAIR | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CRCP REINFORCEMENT sr | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| PAVEMENT TIES EAG | СН | 0 | \$0.00 | 0.0 | \$0.00 | | \$0.00 | |
| DOWEL BARS EAG | СН | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 | |
| CRACK & SEATING CONCRETE PAVEMENT | n | 0.0 | \$0.00 | 0.0 | | 0 | \$0.00 | |
| BREAK & SEATING CONCRETE PAVEMENT ST | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| RUBBLIZING CONCRETE PAVEMENT sr | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| ASPHALTIC BASE PATCHING sr | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE BASE PATCHING sr | n | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE WIDENING sr | n | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| ASPHALTIC BASE COURSE WIDENING M | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE BASE COURSE WIDENING Sr | | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| REMOVING PAVEMENT sr | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| Cost Adjustment-see comps | | | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| OTHER BASE #1M | g | 0.0 | | 0.0 | | | | |
| OTHER BASE #2 M | g | 0.0 | | 0.0 | | 0.0 | | |
| ALTERNATIVE TOTAL | | | \$0.00 | | \$0.00 | | \$0.00 | |

ALTERNATE MAINTENANCE Version 3.3

8600-02-01 Chippewa Falls - Comell Jim Falls - CTH R STH 178 Chippewa

MAINTENANCE COSTS: (CURRENT YEAR)

| | FROM | | | | INCREMENT 3 | | INCREMENT 4 | | INCREMENT 5 | |
|------------------|------------|------------|-----------------|------------|------------------|------------|------------------|------------|------------------|------------|
| ALTERNATE TITLE | YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM | TO YEAR |
| Sphalt/base/sand | \$2,400.00 | | \$4,970.00 | 18 | 24 \$4,970.00 | | 27 \$4,970.00 | | 33 | |
| YEARLY COST | \$1.250.00 | | 9 \$1,550.00 | 10 | 16 \$1,250.00 | | 22 \$1,550.00 | 23 | 28 \$1,250,00 | |
| YEARLY COST | \$1,250.00 | | 9 \$1,550.00 | 10 | 16 \$1,250.00 | | \$1,350.00 | 23 | 28 \$1,250.00 | |
| YEARLY COST | | | | | | | | | 47,22010 | |
| YEARLY COST | | | | | | | | | | |
| 0 YEARLY COST | | | | | | | | | | |

07/13/98

MAINTENANCE COSTS: (CURRENT YEAR)

| INCREMENT 6 | | INCREMENT 7 | | INCREMENT 8 | | INCREMENT 9 | | INCREMENT 10 | | |
|----------------------------------|--------------|-------------|--------------------------------|-------------|------------------|-------------|----------|--------------|--------------|------|
| ALTERNATE TITLE | FROM YEAR | TO YEAR | FROM YEAR | TO YÉAR | FROM YEAR | TO | FROM | TO | FROM YEAR | то |
| YEARLY COS sphalt/base/sand | 34 | 38 | 43 \$1,250.00 40 | 44 41 | 47 \$1,550.00 | 48 | | | | YEAR |
| Sphalt/base YEARLY COST | 34 | 35 | \$1,250.00 40 \$1,250.00 | 41 | \$1,550.00 47 | 48 | | | | |
| xisting Structure YEARLY COST | | | | | \$1,550.00 | | <u>į</u> | | | |
| YEARLY COST | | | | | | | | | | |
| YEARLY COST | | | | | | | | | | |

.
ALTERNATE REHABILITATION Version 3.3

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R

STH 178 Chippewa 07/13/98

ASPHALT PAVEMENT REHABILITATION SCHEMES: Mill / Overlay Limits % OF PROJECT 1: RDWY ONLY MILLING for SURF. PATCHING OVERLAY MIX TYPE % AC in OVERLAY MIX SCHEME OTHER DEPTH (mm) 2:RDWY & Shoulders THICKNESS (mm) (HV,MV,LV) COSTS OTHER COST DESCRIPTION AC1 AC2 AC3 . D.O 75 mv 6.0 25 0.D 90 mv 6.0 .97 Ö Q 100 777 5.0 AC4 Similal costs to mill&relay and new asphalt. AC5 AC6 AC7 AC8 AC9 RECONSTRUCT: USING ORIGINAL AC LAYER THICKNESSES

CONCRETE PAVEMENT REHABILITATION SCHEMES:

| Repair – Grind | | | | % OF PROJECT | | | |
|----------------|--------------|------------------|-------|-------------------|--------------------|-------|------------------------|
| SCHEMES | % PCC REPAIR | AVG PATCH LENGTH | | for | | OTHER | |
| PC1 | % PCC HEPAIH | in m | JOINT | PCC Base Patching | | 1 | OTHER COST DESCRIPTION |
| PC2 | 0.0 | 1.6 | | Q.Q | & Continuous Grind | | |
| DOn | U.U. | 18 | \$2 | \$.D | & Continuous Grind | | |
| <u>r vo</u> | | | | | & Continuous Grind | | |
| | | | | | | | |

| Repair – Overlay SCHEMES | % PCC REPAIR | AVG PATCH LENGTH | | % OF PROJECT for PCC Base Patching | % OF PROJECT for AC Base Patching | OVERLAY THICKNESS (mm) | MIX TYPE (HV.MV.LV) | % AC in OVERLAY MIX | OVERLAY LIMITS 1: RDWY ONLY | OTHER | |
|-----------------------------|--------------|------------------|----|--|---|---------------------------|------------------------|------------------------|--------------------------------|-------|------------------------|
| PC4 PC5 | 0.0 0.0 | 18 | 12 | 5.0 | 0.Q | 0 | (10,000,00) | E.Q | 2: RDWY & Shoulders | COSTS | OTHER COST DESCRIPTION |
| PC6 | | | | | | | אחי | 5.0 | 2 | | |

| PC7 | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders 2: | 75 | % PCC REPAIR | AVG PATCH LENGTH in m | JOINT | % OF PROJECT for PCC Base Patching 233 | OVERLAY THICKNESS (mm) | MIX TYPE (HV,MV,LV) | % AC in OVERLAY MIX | OTHER |
|--|---|----|--------------|--------------------------|-------|---|-------------------------------|------------------------|------------------------|-------|
| PC9 | | | | | | | 72 | ttiv | 6.0 | |
| PC7 OTHER COST DESCRIPTION PC8 OTHER COST DESCRIPTION PC9 OTHER COST DESCRIPTION | | | | | | | | | | |
| | _ | | | OTHER | | | | | | |

| SCHEME | | OTHER | |
|--------|--|-------|------------------------|
| | | COSTS | OTHER COST DESCRIPTION |
| PC10 | CONTINUOUS DIAMOND GRIND ONLY | | |
| PC11 | | | |
| | CONTRACTOR CANAL FOC LATER THICKNESSES | | |

ALTERNATE REHABILITATION SCENARIOS:

| HEHABILITATION COSTS | ALT. #1; | PCC | the second state of the se | | | | | | | | | a second constraints and a second second |
|--------------------------------------|----------|----------|--|----------|-------------------|-----------------|----------|--------------|-----------------|----------|---------------------|--|
| (COSTS ARE CURRENT YEAR) | SPACING | TYPE | CUDDENT VD COOT | ALT. #2: | Asphalt/base/sand | | ALT. #3: | Asphalt/base | | ALT. #4: | Eviatian Otoriation | |
| FIRST REHABILITATION | 2000 | IIFE GRA | CURRENT YR COST | | TYPE | CURRENT YR COST | SPACING | TYPE | CURRENT YR COST | SPACING | Existing Structure | |
| SECOND REHABILITATION | | pro | \$14,742.00 | | 4 AC2 | \$57,402.45 | 14 | AC2 | \$57,402.45 | | TYPE | CURRENT YR COST |
| THIRD REHABILITATION | 15 | Dr.7 | \$60,212.25 | <u>1</u> | Z AC3 | \$65,438.90 | 5 | AC3 | \$66,438,90 | | | \$0.00 |
| FOURTH REHABILITATION | | | \$61,101.90 | <u> </u> | 2 409 | \$70,222.41 | 1 | ACO | \$78,407.46 | | | \$0.00 |
| FIFTH REHABILITATION | | | | | | \$0.00 | | | \$0.00 | | | \$0.00 |
| EXPECTED LIFE OF LAST REHABILITATION | 10 | | \$0.00 | | | \$0.00 | | | \$0.00 | | | \$0.00 |
| TOTAL LIFE | 50 | 1 | | | <u> </u> | | | | | | | \$0.00 |
| | | 1 | l | 5 | 2 | | 52 | 2 | | | 24 24 | |
| | | | | | | | | | | | 2 | |

LIFE CYCLE COST ANALYSIS

8600-02-01

Version 3.3

Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa CURRENT YEAR 1998 DISCOUNT RATE (%) 5.0 CONSTRUCTION YEAR 2002 PROJECT LENGTH (Km) 1.00 **DESIGN YEAR** 2022 ANALYSIS BASIS (P/M) M ANALYSIS PERIOD 50.0

| TERMINAL SALVAGE VALUE | AL1. 1 | AL1.2 | ALI.3 | ALT. 4 | ALT.5 | ALT. 6 | i. |
|------------------------|--------|-------|-------|--------|-------|--------|----|
| TERMINAL SALVAGE VALUE | | | | | | | |

PRESENT WORTH COSTS: (CURRENT YEAR)

ALT. 1 ALT. 2 ALT. 3 ALT. 4 ALT.5 ALT. 6 PCC Asphalt/base/sand Asphalt/base Existing Structure 0 0 INITIAL CONSTRUCTION COSTS \$180,178.63 \$127,730.04 \$129,791.60 \$0.00 \$0.00 \$0.00 **REHABILITATION COSTS** \$23,173.16 \$48,271.80 \$49,326.35 \$0.00 \$0.00 \$0.00 MAINTENANCE COSTS \$5,916.56 \$3,441.68 \$3,441.68 \$0.00 \$0.00 \$0.00 TERMINAL SALVAGE VALE \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 REHABILITATION SALVAGE VALUE \$0.00 (\$1,292.49) (\$1,443.14) \$0.00 \$0.00 \$0.00 TOTAL FACILITY COSTS \$209,268.35 \$178,151.02 \$181,116.49 \$0.00 \$0.00 \$0.00

EQUIVALENT UNIFORM ANNUAL COSTS:

(OVER ANALYSIS PERIOD)

| | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
|------------------------------|-------------|---|--------------|--------------------|--------|---|
| | PCC | Asphalt/base/sand | Asphalt/base | Existing Structure | 0 | ٥ |
| INITIAL CONSTRUCTION COSTS | \$9,869.60 | +++++++++++++++++++++++++++++++++++++++ | \$7,109.56 | \$0.00 | \$0.00 | \$0.00 |
| REHABILITATION COSTS | \$1,269.35 | | \$2,701.94 | \$0.00 | \$0.00 | \$0.00 |
| | \$324.09 | +100.0L | \$188.52 | \$0.00 | \$0.00 | \$0.00 |
| | \$0.00 | φ0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 |
| REHABILITATION SALVAGE VALUE | \$0.00 | (\$70.80) | (\$79.05) | \$0.00 | \$0.00 | \$0.00 |
| | | | | | | \ _\\\\\\\\\\\\\\\\\\\\\\\\ |
| TOTAL FACILITY COSTS | \$11,463.04 | \$9,758.53 | \$9,920.97 | \$0.00 | \$0.00 | · \$0.00 |

07/13/98

| Page: 1 Do | cument Na | me: untitled | | | | | | | | | |
|--|----------------|--|-----------------------------|--------------|------------------------------|------------------|--------|------------------------|-----------------------|----------|------------------------------|
| 7/14/98 06:26:33 | | WISCONSIN DEPARTME PAVEMENT IND BROWSE OF CURREN | EX FILE | SY | ISPORTAT STEM SI VALUE | | | | | IF | FMBC |
| District | 6 Coun | ty Name CHIPPEWA | Count | -y | Number | 9 | Н | ighwa | ay 1' | 78N | |
| From | | ld to View Section D | Τc | | | Surf | Eace | * *PI Surv | <i>r</i> ey | | vey |
| Opt RP + 011G + 012K + 014G + | 0.000 | From Feature CTH. Y 182ND. ST. CTH Y INT | RP + 012K 014G 015 | + | | 85 85 | 1 1 | Yr 1 96 96 96 | NO. 28 49 57 | 97 97 | mm/m 1.83 1.40 2.38 |
| 0140 + 015 + 015 + 015 + 017 + 0017 + 00017 + 00017 + 0017 + 00017 + 00017 + 00017 + 00017 + 00017 + 0 | 0.000 0.980 | FINLEY LAKE RD 160TH AVE. 210TH ST. | 015 015 017 018 | + + + | 0.980 0.000 | 81 87 79 | 1 1 | 96 96 96 | 76 34 70 | 97 97 | 2.38 3.08 2.75 3.50 |
| 018 + 018 + | 0.000 0.680 | 215TH ST. SECTION 9 & 10 | 018 020 | + + | 0.680 0.000 | 88 84 | 1 1 | 96 96 | 31 50 | 97 97 | 2.46 2.86 |
| 020 + 022 + Surf Type | 0.000 | 180TH AVE 190TH AVE. B,2=BRM, 3=ACPM/RB, 4 | 022 023 4=JRCP, | + + 5= | 0.000 | 88 83 5 d, | 2 | 96 96 CRCP, | 41 75 8=3 | 97 | 2.97 3.58 /d |

SELECT DATA TO VIEW, OR PRESS ENTER FOR MORE ENTER TO CONTINUE PF3 OR PF15 TO BROWSE MENU PA2 TO CANCE PF2 OR PF14 TO PRIMARY MENU PF12 OR PF24 TO LOGOFF CICS

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| 7/14/98WISCONSIN DEPARTMENT06:26:41PAVEMENT INDEXBROWSE OF CURRENT INDEX | FILE SYSTEM |
| District 6 County Name CHIPPEWA | County Number 9 Highway 178N |
| 023 + 0.000 CTH R INT 024 + 0.000 CTH ZZ INT 024 + 1.250 SECTION 25 & 24 | To Surface Survey Survey RP + Distance Yr Ty Yr No. Yr mm/m 023 + 0.000 83 2 96 75 97 3.58 024 + 0.000 87 1 96 38 97 2.60 024 + 1.250 81 1 96 24 97 2.45 027 + 0.000 84 1 96 66 97 2.57 499E + 0.000 + + + + + + |
| NO MORE SECTIONS FOR COUNTY & HIGHWAY ENTER TO CONTINUE PF3 OR PF PF2 OR PF14 TO PRIMARY MENU PF12 OR F | |

CORRESPONDENCE/MEMORANDUM

Date: July 13, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: Traffic Forecast projection revisions Project 8600-02-01

This project has been in and out of the six year program for the last 5-10 years. There has been no recent specific traffic forecast done for this segment. For structural design purposes, I chose to use a construction year ADT of 2000 and a 20 year ADT of 2400. The truck percentage was rounded to 8%. The following two forecasts done in 1992 and 1995 give volumes for the roadway but are outdated.

TRAFFIC FORECAST

PROJECT ID:8600-02-71COUNTY:ChippewaROUTE:STH 178LOCATION:Int. w/ CTH Y to Int. w/ STH 64

| KEY | |
|--------------------|-------------|
| *000* 1991 Tr | affic Count |
| -000- 1994 Fo | recast |
| (000) 2004 Fo | recast |
| <u>000</u> 2014 Fo | recast |
| DESIGN VAL | UES |
| K100 | 11.6 |
| K50 | 12.4 |
| K30 | 13.1 |
| P(PHV) | 16.9 |
| T(DHV) | 6.2 |
| T(PHV) | 3.5 |
| D | 60/40 |
| K8(ADT) | |
| T(A8HV) | |
| TRUCK CLASS | |
| TRUCK TYPE | % ADT |
| 2D | 3.6 |
| 3AX | 1.4 |
| 2S1+2S2 | 0.7 |
| 3-S2 | 2.0 |
| DBL-BTM | 0.0 |
| TOTAL | 7.7 |

NOTES ON THE ANALYSIS: 1. The functional classification of STH 178 over the project section is COLLECTOR; the seasonal ad –

- justment factor group for the section is group 4.
 In developing this forecast, it was assumed that no new major traffic generators will be developed in
- the vicinity of the project section over the course of the forecast period.4. In developing the forecast for the southern site, the
- the historical traffic count for 1975 was excluded from the analysis because it departed substantially from the trend in the other historical counts.
- 5. Truck percentages of ADT were obtained from a table of vehicle type percentages by functional class and urban/rural area because a vehicle type counter is not located on STH 178.
- Design parameters are calculated using the design year ADT for the northern most forecast location (3100).



veloped by Keith Wendt, Traffic Forecasting and Analysis Section 14-Sep-92

| PROJECT ID: 8191-01 | -01 | ÷ | KEY | | Developed by Scott Erdman, Traffic Analys |
|--|--|---|---|---|---|
| COUNTY: Chippewa ROUTE: STH 64 | | | *000* | 1993 ADT | & Forecasting Sect.; Phone: (608) 266-101 |
| LOCATION: STH 64: C | TILD 4. OTTIOT | | -000- | 1999 ADT | E-Mail ID: ERDMAS |
| DISTRICT: 6 | IH K 10 51H2/ | | (000) | 2009 ADT | Completed: 26-Jul-95 |
| DISTRICTO | | | 000 | 2019 ADT | · · · |
| N | 64 | $ \begin{array}{c} -700-\\(775)\\850\\-200-\\(225)\\250\end{array} $ 178 Detail | 64 | | See Detail *450* -900- (1000) 1100 (78) |
| *990* -1150- (1350) 1550 (64) | | R | ZZ -400- (450) 475 | | (178) -2450 (2900) 3350 *1700* -1950- (2350) |
| | | *580* | -200- (200) 225 | *1500* | 2750 |
| | | -600-/ | (200) | *1500* | |
| | | -600- / (650) | (200) | -1750- | |
| No Build | 1 | -600-/ | (200) | | |
| No Build | | -600-/ (650) 700 | (200) 225 | -1750- (2100) 2500 | 2750 |
| No Build | UCK CLASS | -600-/ (650) 700 Notes on the Forecast: | (200) 225 (178) | -1750- (2100) 2500 RE | 2750 27 FERENCES |
| No Build DESIGN VALUES TR K100 11.5 TR | UCK CLASS | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic | (200) 225 (178) c volumes repres | -1750- (2100) 2500 sent Axle - 1. " | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage cour |
| No Build DESIGN VALUES TR K100 11.5 TR K50 12.3 T | UCK CLASS CUCK TYPE % ADT | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic Adjusted AADT. Pre - 1990 | (200) 225 (178) c volumes representation 0 counts are fact | -1750- (2100) 2500 RE sent Axle - ored using 19 | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage cour 075 – 1993. |
| No Build DESIGN VALUES TR K100 11.5 TR K50 12.3 T K30 12.9 2D | CUCK CLASS CUCK YPE % ADT 3.6 | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic Adjusted AADT. Pre - 199 indicated Axle - Adjustment | (200) 225 (178) c volumes represent 0 counts are fact t Factors (A – A | -1750- (2100) 2500 RE sent Axle - ored using F). 2. " | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage count 075 – 1993. Official Poulation Estimates, Demographic Services |
| No Build DESIGN VALUES TR K100 11.5 TR K50 12.3 T K30 12.9 2D P(PHV) 16.7 3AJ T(DHV) 6.2 2S1 | CLASS CUCK CUCK YPE % ADT 3.6 X 1.4 1+2S2 0.7 | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic Adjusted AADT. Pre - 1990 indicated Axle - Adjustment 2. This forecast assumes that no | (200) 225 (178) c volumes repres 0 counts are fact t Factors (A – A. o signficant new | - 1750- (2100) 2500 sent Axle - ored using F). traffic | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage cour 075 – 1993. |
| No Build DESIGN VALUES TR K100 11.5 TR K50 12.3 T K30 12.9 2D P(PHV) 16.7 3AJ T(DHV) 6.2 2S1 T(PHV) 3.5 3-5 | CLASS CUCK CUCK YPE % ADT 3.6 X 1.4 1+2S2 0.7 S2 2.0 | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic Adjusted AADT. Pre - 199 indicated Axle - Adjustment 2. This forecast assumes that no generators will be developed the forecast period. | (200) 225 (178) c volumes repres 0 counts are fact t Factors (A – A) o significant new in the project an | - 1750- (2100) 2500 sent Axle - ored using F). traffic rea during | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage count 075 – 1993. Official Poulation Estimates, Demographic Services |
| DESIGN VALUES TR K100 11.5 TR K50 12.3 T K30 12.9 2D P(PHV) 16.7 3A2 T(DHV) 6.2 2S1 T(PHV) 3.5 3-5 D 60/40 Db | CUCK CLASS CUCK YPE % ADT 3.6 X 1.4 1+2S2 S2 2.0 1-Btm | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic Adjusted AADT. Pre – 199 indicated Axle – Adjustment 2. This forecast assumes that no generators will be developed the forecast period. 3. STH 64 has an axle – adjust | (200) 225 (178) (1 | - 1750- (2100) 2500 Exent Axle - ored using F). traffic ea during 23 and is | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage count 075 – 1993. Official Poulation Estimates, Demographic Services |
| DESIGN VALUES TR DESIGN VALUES TR K100 11.5 TR K50 12.3 T K30 12.9 2D P(PHV) 16.7 3A2 T(DHV) 6.2 2S1 T(PHV) 3.5 3-5 D 60/40 Db | CLASS CUCK CUCK YPE % ADT 3.6 X 1.4 1+2S2 0.7 S2 2.0 | -600-/ (650) 700 Notes on the Forecast: 1. Historic and projected traffic Adjusted AADT. Pre – 199 indicated Axle – Adjustment 2. This forecast assumes that no generators will be developed the forecast period. 3. STH 64 has an axle – adjust | (200) 225 (178) (1 | - 1750- (2100) 2500 Exent Axle - ored using F). traffic ea during 23 and is | 2750 (27) FERENCES Wisconsin Highway Traffic", available coverage count 075 – 1993. Official Poulation Estimates, Demographic Services |

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CONCEPT DEFINITION REPORT

Date: 07/17/96

To: Michael A. Cass (P.E.)

From: District 6

- I. Design ID: 8600-02-01 Related ID(s): 8600-02-71(Const) Highway No. or Local Road Name: STH 178 8600-02-21 (R/W) Title: CHIPPEWA FALLS - CORNELL ROAD County: CHIPPEWA Length: 7.4 Miles 11.9 km Functional Class: Major Collector Current ADT: 1650 (1993) LOCATION: CTH Y - CTH R
- Roadway Conditions: II. A. Pavement: Type: AC Width: 22 Year: 1981 PSI: 2.69 (1993) PDI: 30 (1994) Shoulder: Type: Gravel Width: 2 Accident Rate: 480 Year: 1995 Vertical: Yes Substandard Alignment: Horizontal: Yes
 - B. Structure: (may be continued on back side) Length: 86.5 ft, 26.4 m Year Constructed: 1942 Type: DECK GIRDER Bridge Number: B-09-0682 Clear Roadway Width: 27.6 SR: 80.5 RS: 89.4

JUSTIFICATION: Accident rate is 480 vs State ave of 222 because of narrow shoulders, sharp horiz curvature and short vertical and horiz sight distance. There are many power poles and trees in clear zone.

PROPOSED IMPROVEMENT: Grade, Base, Asphaltic Surface to C3 standards III. with a 24 ft surface on a 36 ft roadway with a 30 ft clear zone.

> A. Environmental documentation type: III ER PMSID: 98060020201 B. Improvement Type: RECST C. Cost: \$ 3,850,000 Program Year: 2002 Program: 3334 D. Local Participation: \$ No Access Control: No

DISTRÌCT 6 APPROVAL Project Supervisor

Planning Supervisor

Concept Definition Report Project: 8600-02-01 CC: Gerry Feiler - Rm 951, Len Stanek - Rm 651, Bureau of Environment - Rm 451

Gene Hoelker-FHWA

 $\frac{7 - 7}{\text{ate}} = \frac{7}{\sqrt{2}}$

Page: 1 of 2 Date: 07/17/96

District 6 Geographic Information System



State of Wisconsin

CORRESPONDENCE/MEMORANDUM DISTRICT #6

Date: July 16, 1998

To: File

- From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer
- Subject: **PAVEMENT DESIGN REPORT** Approval Letter

Project I.D. 8600-02-01 Chippewa Falls - Cornell Road Jim Falls - CTH R **STH 178** Chippewa County

Upon review of the attached pavement design documentation, the pavement type selection recommendations are approved for the above mentioned project segments.

Reviewed:

COMMENTS

Richard J. Shermo, P.E. Date District #6 Area Supv.-Project Development Section

Approved:

COMMENTS

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

State of Wisconsin Transportation District #6

CORRESPONDENCE/MEMORANDUM

Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: Pavement Design Report Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

EXECUTIVE SUMMARY

This report makes the following recommendations for the proposed reconstruction project.

| <u>LOCATION</u> | PAVEMENT STRUCTURE | THICKNESS |
|---------------------------------|---------------------------------|---|
| STH 178-mainline & bypass lanes | Asphalt/ Base Course/ Sand Lift | 125mm/275mm/275mm (5") /(11") /(11") |
| Side Roads >500 ADT | Asphalt/ Base Course | 100mm/300mm (4") /(12") |
| Side Roads <500 ADT | Asphalt/Base Course | 75mm /225mm (3") /(9") |

Type MV Asphaltic Concrete Pavement mix with PG grade 58-28 should be used for this project. It is anticipated that by the time this plan is let to bid, a different PG graded oil could be the standard. The designer should coordinate the special provisions to reflect the correct AC type.

The $125 \text{mm}(5^{"})$ asphalt pavement should be constructed with two lower layers totaling $85 \text{mm}(3 \frac{1}{2}^{"})$ and a upper layer of $40 \text{mm}(1 \frac{1}{2}^{"})$. The $100 \text{mm}(4^{"})$ asphalt pavement should be constructed with a $50 \text{mm}(2^{"})$ lower layer and a $50 \text{mm}(2^{"})$ upper layer. The $75 \text{mm}(3^{"})$ asphalt pavement should be constructed with two layers.

The sand lift should be specified to meet Grade #1 requirements as specified in the Standard Specifications Section 209.2.2 for granular backfill.

EXISTING CONDITIONS

This 11.9km(7.4 mile) project involves the portion of STH 178 from the intersection of CTH Y at Jim Falls northerly along the Chippewa River to the intersection of CTH R. Due to a high accident rate, as stated in the CDR, the roadway will be reconstructed to C3 standards. This roadway is not being reconstructed due to excessive pavement failures or deficiencies. It appears that the roadway was last resurfaced in 1981 with a maintenance type overlay. The 1996 PDI ranged from 28-75 for this section. The 1997 IRI ranged from 1.4-3.6.

In 1993, the roadway core was investigated for a resurfacing type project. Since that time, the concept was revised to a reconstruct type improvement. The 1993 borings are located in the technical services project records.



TRAFFIC PROJECTIONS

The construction year-0 year ADT is 2000 and the 20 year ADT is projected to be 2400.

Truck percentages are as follows:

| <u>TRUCK TYPE</u> | | <u>%</u> |
|----------------------|-------|-------------------|
| 2D 3AX 2SI,2S2 | | 3.6 1.3 0.8 |
| 3-S2 DBL.BTM | | 2.3 0.0 |
| | TOTAL | 8.0 |

PROPOSED IMPROVEMENT

This project is currently scheduled for a reconstruct(RECST) type improvement. The existing roadway will be reconstructed to C3 standards which will include adjustments to the horizontal and vertical alignments.

SOIL ENGINEERING FACTORS

Over the length of this project, many different soil series are located under the roadway. The roadway core itself, as revealed in the 1993 roadway borings, has various amounts of silt and topsoil present along with some granular material in some of the fill locations. With the existing roadway material varying from moist to wet, construction could be a problem. With the existing silty materials in mind, it was agreed to with the Soils Engineer- Lary Hyland that a sand lift would be the best choice in this situation. For further discussion see the "alternative evaluated section". The DGI recommended for this roadway is 14 with a soil support value of 4.0. At the time of this report, due to the uncertainty of the horizontal and vertical alignment only a preliminary soils analysis has been completed.

FRICTION CHARACTERISTICS

The aggregate is expected to be igneous with 0% dolomite and a 20% L.A. wear resulting in a friction number of 44 and 51 for the PCC. Friction is not expected to be a problem.

ALTERNATIVES EVALUATED and RECOMMENDATIONS

Alternative Discussion

Initially, this segment of roadway was scheduled for a maintenance type overlay in 1998. That project was scrapped and the roadway segment is now being evaluated as a reconstruct to C3(100KM/60MPH) standards. In January 1997, the project was explained to me as a typical shoulder widening project on the south end with some short segments of relocation from the middle of the project northward to CTH R. Since that time, evaluation by the development staff has led to a concept of a total reconstruction.

I have numerous concerns that need to be addressed. The horizontal alignment, provided at the time of this report, continually drifts on and off the centerline of the existing road core in a range of 0-8 feet(0-2.5m). We have had past mid lane failures in minor grading areas when part of the old core supports the new lane and new material is added adjacent to support the remaining lane. Besides the obvious heave potential of the different materials, differential settlement occurs in the new material due to different compaction levels of the new material versus the old road core. As shown on the plan sheets and preliminary sections, in many cases, the subgrade point is being moved out over wet silty marshy material in the old ditches. Also in many locations, water is within 2-3 feet of the pavement surface. At this point in the design process, I can only assume that the designer will follow through with his/her responsibility to provide information to and coordinate with the district Soils Engineer to identify and treat these problem areas once the final horizontal and vertical alignment is chosen. In past situations of widening over old ditches, these areas have either been excavated and back-filled or a grid/back-fill combination was used. The high water table is a separate issue, as obviously it is hard to construct a stable subgrade within 1-2 feet of the existing water elevation. There is a reasonable chance that the asphalt/base/sand lift pavement will not perform in this situation. The designer should remember that a sand lift or breaker run platform will typically push the subgrade to 2 feet or greater below the finished profile.

Alternative Discussion-cont.

On other projects/roadways of this type, past experience had led to a district sequence of operations where the horizontal alignment is left in place and the shoulders are widened and raised to the existing profile. If a sag vertical deficiency exists in this area we will typically gravel lift up to a foot to improve the profile. Crest and sag verticals are routinely excepted to standards of 40 mph if there is no accident history at that location. After the widening or lifting is completed the traveled way surface is addressed with some type of overlay or mill/pulverize & relay and overlay combination, always taking care to remain in the middle of the old roadway core. We typically do experience some shoulder distortion but it is not critical to the performance of the pavement. Besides achieving pavement performance, this operation also has the benefit of providing adequate local access because, typically 2 lane traffic can be provided in the off hours and on weekends during the life of the project.

With reconstruction of the existing STH 178 roadway the project option chosen versus the above mentioned scenario, local access and staging of construction activities will both play major roles in the plan development. Since local access will need to be provided, I am assuming a grading operation will need to be completed one half at a time with excavation, EBS, back-fill, borrow, sand lift and base course progressing down the roadway as access permits. The relocation areas are typically completed separately with the old road in these relocated areas being obliterated at the end. For the sand lift to perform in the pavement structure, the sand cannot be placed on a rutted un-rolled subgrade. This typically requires the contractor to exercise care in the placing of the lift material. Some type of drain will be required at the low points in the sand lift profile. A breaker run was not chosen due the availability of local materials.

With this type of work, it is beneficial to work during the dry part of the summer. Even with these precautions, there is a reasonable chance that stage construction grading might not be completed in one year. Soft spots in the base could be common place under the reconstruct option. If the base course and the two lower layers were placed in year one, the surface layer could be placed the following year. This approach would allow some repair of the broken up areas prior to the final surface being placed.

SUMMARY OF COSTS-----LCCA

A twenty year service life was used.

The first alternative is : 175mm(7") PCC over 150mm(6") base over sand lift: \$219008 per KM for initial construction cost \$ 11463 per KM for Equivalent Uniform Annual Cost

The second alternative is : 125mm(5") AC over 275mm(11") base course over 275mm(11") sand lift:

\$155257 per KM for initial construction cost

\$ 9759 per KM for Equivalent Uniform Annual Cost

The third alternative is : $140 \text{mm}(5 \frac{1}{2}) \text{AC}$ over 300(12) base course *

\$157763 per KM for initial construction cost

\$ 9921 per KM for Equivalent Uniform Annual Cost

* Not recommended due to sand lift requirement. For information purposes only

RECOMMENDATIONS

| LOCATION | PAVEMENT STRUCTURE | THICKNESS |
|---------------------------------|---------------------------------|---|
| STH 178-mainline & bypass lanes | Asphalt/ Base Course/ Sand Lift | 125mm/275mm/275mm (5") /(11") /(11") |
| Side Roads >500 ADT | Asphalt/ Base Course | 100mm/300mm (4") /(12") |
| Side Roads <500 ADT | Asphalt/Base Course | 75mm /225mm (3") /(9") |

Type MV Asphaltic Concrete Pavement mix with PG grade 58-28 should be used for this project. It is anticipated that by the time this plan is let to bid, a different PG graded oil could be the standard. The designer should coordinate the special provisions to reflect the correct AC type.

The 125 mm(5") asphalt pavement should be constructed with two lower layers totaling $85 \text{mm}(3 \frac{1}{2"})$ and a upper layer of $40 \text{mm}(1 \frac{1}{2"})$. The 100 mm(4") asphalt pavement should be constructed with a 50 mm(2") lower layer and a 50 mm(2") upper layer. The 75 mm(3") asphalt pavement should be constructed with two layers.

The sand lift should be specified to meet Grade #1 requirements as specified in the Standard Specifications Section 209.2.2 for granular backfill.

The designer should use asphaltic surface items for incidental asphalt work such as driveways, safety islands, etc. as allowed under the 1997 Supplemental Specs.

Randy W. Luedtke, P.E.



RIGID PAVEMENT DESIGN WORKSHEET

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT DESIGN YEAR DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|-------|
| 2,000 |
| 2022 |
| 2,400 |
| 0.50 |
| 1.00 |
| 20.0 |
| 1,100 |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL'S |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 1.2 | 17 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.6 | 5 |
| 3S-2 | 2.3 | 1,100 | 25 | 1.6 | 40 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.1 | 0 |
| DESIGN LANE DAILY ESAL's | 8.0 | | | | 74 |
| DESIGN LANE TOTAL LIFE ESAL'S | | | | Ē | 540,200 |

SOILS:

MODULUS OF SUBGRADE REACTION (K)

30

THICKNESSES:

CALCULATED PAVEMENT THICKNESS PAVEMENT THICKNESS TO BE USED



FLEXIBLE PAVEMENT DESIGN WORKSHEET

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT DESIGN YEAR DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|-------|
| 2,000 |
| 2022 |
| 2,400 |
| 0.50 |
| 1.00 |
| 20.0 |
| 1,100 |
| |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL's |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 0.8 | 11 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.5 | 4 |
| 3S-2 | 2.3 | 1,100 | 25 | 0.9 | 23 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.0 | 0 |
| DESIGN LANE DAILY ESAL'S | 8.0 | | | | 50 |
| DESIGN LANE TOTAL LIFE ESAL'S | | | | | 365,000 |

SOILS:

DESIGN GROUP INDEX SOIL SUPPORT VALUE FROST INDEX



DESIGN - SN VALUE & MIX TYPE:

3.0

3.49

SERVICEABILITY INDEX REQUIRED SN VALUE

ASPHALT MIX TYPE: MV

ALTERNATE DESIGN:

| | Asphalt/base/sand | | Asphalt/base | | | |
|----------------------------|-------------------|---------|--------------|-----------|---------|-----------------|
| LAYER | THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN |
| SURFACE: | | SURFACE | | | SURFACE | <u>Declines</u> |
| ASPHALTIC CONCRETE | 125 | 0.0173 | 2.16 | 140 | 0.0173 | 2.42 |
| EXISTING ASPHALT | | 0.0100 | 0.00 | | | 0.00 |
| BASE COURSE: | BAS | E | | | BASE | |
| CRUSHED AGG. BASE COURSE | 275 | 0.0039 | 1.07 | 300 | 0.0039 | 1.17 |
| OPEN GRADED BASE COURSE #1 | | | 0.00 | | | 0.00 |
| OPEN GRADED BASE COURSE #2 | | | 0.00 | | | 0.00 |
| EXISTING BASE | | 0.0039 | 0.00 | | 0.0039 | 0.00 |
| EXISTING AC | | | 0.00 | | | 0.00 |
| PULVERIZED AC | | | 0.00 | | | 0.00 |
| EXISTING PCC | | | 0.00 | | | 0.00 |
| RUBBLIZED PCC | | | 0.00 | | | 0.00 |
| CRACK (BREAK) & SEAT PCC | | | 0.00 | | | 0.00 |
| SUBBASE COURSE: | SUBB/ | ASE | | | SUBBASE | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 |
| BREAKER RUN | | | 0.00 | | | 0.00 |
| GRANULAR SUBBASE | 275 | 0.0012 | 0.33 | | | 0.00 |
| EXISTING SAND LIFT | | 0.0025 | 0.00 | | 0.0025 | 0.00 |
| TOTAL SN VALUE | | | 3.57 | | | 3.59 |

FLEXIBLE PAVEMENT DESIGN

ALTERNATE DESIGN:

| | | Existing Struct | ure | | ······································ | |
|----------------------------|--------------------|-----------------|------|-----------|--|------|
| LAYER | THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN |
| SURFACE: | | SURFACE | | | SURFACE | |
| ASPHALTIC CONCRETE | 125 | 0.0173 | 2.16 | | 0.0173 | 0.00 |
| EXISTING ASPHALT | | | 0.00 | | | 0.00 |
| BASE COURSE: | | BASE | | | BASE | 0.00 |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | 0.0039 | 0.00 |
| OPEN GRADED BASE COURSE #1 | | | 0.00 | | | 0.00 |
| OPEN GRADED BASE COURSE #2 | | | 0.00 | | | 0.00 |
| EXISTING BASE | 125 | 0.0039 | 0.49 | | | 0.00 |
| EXISTING AC | | | 0.00 | | | 0.00 |
| PULVERIZED AC | | | 0.00 | 1 | | 0.00 |
| EXISTING PCC | | | 0.00 | | | 0.00 |
| RUBBLIZED PCC | | | 0.00 | | | 0.00 |
| CRACK (BREAK) & SEAT PCC | | | 0.00 | | | 0.00 |
| SUBBASE COURSE: | | SUBBASE | | | SUBBASE | 0.00 |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 |
| BREAKER RUN | | | 0.00 | | | 0.00 |
| GRANULAR SUBBASE | | | 0.00 | | 0.0012 | 0.00 |
| EXISTING SAND LIFT | | 0.0025 | 0.00 | | 0.0012 | |
| TOTAL SN VALUE | | ····· | 2.65 | | | 0.00 |
| | SN is Less Tha | n China artat | 2.00 | | L | 0.00 |

SN is Less Than SNreq'd

PAVEMENT SURFACE FRICTION DESIGN

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178

Chippewa

| CONSTRUCTION YEAR ADT | 2,000 | | |
|--|--------|------------------|-------|
| DESIGN YEAR ADT | 2,400 | EXP. GROWTH RATE | 0.92% |
| DIRECTIONAL FACTOR (DF) | 0.50 | | |
| LANE DISTRIBUTION FACTOR (LDF) | 1.00 | | |
| % HEAVY VEHICLES (HV) | 8.0 | | |
| AC PAVEMENT AGE OR SERVICE LIFE (YR) | 15.0 | AC "AGE" ADT | 2,293 |
| AC LAVP AT SPECIFIED AGE (IN MILLIONS) | 5.876 | | |
| PC PAVEMENT AGE OR SERVICE LIFE (YR) | 25.0 | PC "AGE" ADT | 2,512 |
| PC LAVP AT SPECIFIED AGE (IN MILLIONS) | 10.293 | | |

AGGREGATE PROPERTIES:

| | AC MIX AGGREGATES | PCC MIX AGGREGATES |
|------------|-------------------|--------------------|
| % DOLOMITE | 0 | 0 |
| % LA WEAR | 20 | 20 |

AC AGGREGATE SOURCE: PCC AGGREGATE SOURCE:

DESIGN:

ASPHALTIC SURFACE FORMULA

FN40 = 41.4 - 1.45 ln(LAVP) + 0.245(LAWEAR) - 0.00075(DOLOMITE) ^2

| FN40 AT SPECIFIED PAVEMENT AGE | 43.7 |
|---|--------|
| % PROBABILITY THAT CALCULATED VALUE IS < 35 | 7.9 |
| | |
| AGE (YR) WHEN FN40=35 | AGE>50 |

CONCRETE SURFACE FORMULA

 $\ln(FN40) = 3.99 - 0.0419\ln(LAVP) - 0.00129(DOLOMITE) + 0.00474(HV)$

| FN40 AT SPECIFIED PAVEMENT AGE | 50.9 |
|---|--------|
| % PROBABILITY THAT CALCULATED VALUE IS < 35 | <0.05% |
| AGE (YR) WHEN FN40=35 | AGE>50 |

BID ITEM COSTS

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| | BID ITEM | 1 | UNIT |
|---|-------------------------|-----------------|-----------------|
| BID ITEM | # | UNITS | COST |
| ASPHALTIC MATERIAL FOR TACK COAT | 40204 | L | \$1.00 |
| ASPHALTIC MATERIAL FOR PLANT MIXES | 40501 | Mg | \$155.00 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE HV | 40712 | Mg | \$22.00 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE MV | 40713 | Mg | \$16.50 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE LV | 40714 | Mg | \$16.50 |
| RECYCLED ASPHALTIC SURFACE, TYPE HV | 90381 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE MV | 90382 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE LV | 90383 | Mg | |
| CONCRETE PAVEMENT, 150 mm | 41506 | sm | \$13.50 |
| CONCRETE PAVEMENT, 175 mm | 41507 | sm | \$18.00 |
| CONCRETE PAVEMENT, 200 mm | 41508 | sm | \$18.00 |
| CONCRETE PAVEMENT, 225 mm | 41509 | sm | \$20.25 |
| CONCRETE PAVEMENT, 250 mm | 41510 | sm | |
| CONCRETE PAVEMENT, 275 mm | 41511 | sm | |
| CONCRETE PAVEMENT, 300 mm | 41512 | sm | |
| | 41530 | sm | |
| CONTINUOUS CONCRETE PAV'T REINFORCEMENT | 41551 | sm | |
| PAVEMENT TIES | 41571 | EACH | \$5.00 |
| | 41572 | EACH | \$5.00 |
| CRUSHED AGGREGATE BASE COURSE | 30404 | Mg | \$7.75 |
| OPEN GRADED BASE COURSE #1 | 30418 | Mg | \$9.00 |
| OPEN GRADED BASE COURSE #2 | 30420 | Mg | \$9.00 |
| ASPHALTIC BASE COURSE ASPHALTIC BASE COURSE WIDENING | 30601 | Mg | |
| CONCRETE BASE COURSE WIDENING | 30606 | Mg | |
| CONCRETE BASE COURSE WIDENING | <u>30706-9</u> 30751 | sm | |
| BREAKER RUN | 30426 | sm Ma | \$7.00 |
| GRANULAR SUBBASE COURSE | 21201 | Mg | <u> </u> |
| MILL AND RELAY ASPHALTIC CONCRETE PAVEMENT | 21201 | <u>cm</u> sm | \$0.86 |
| SALVAGED ASPHALTIC PAVEMENT | 41010 | Mg | <u></u> |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | 41020 | Mg | \$7.72 |
| ASPHALTIC SURFACE, PATCHING | 41102 | Mg | <i>Ψ1.14</i> |
| PULVERIZING ASPHALTIC CONCRETE PAVEMENT | 41102 | sm | \$0.70 |
| BASE PATCHING, ASPHALTIC | 30810 | sm | ψυ.ιυ |
| BASE PATCHING, CONCRETE | 30820 | sm | \$40.95 |
| CRACKING AND SEATING CONCRETE PAVEMENT | 41040 | sm | \$\$0.00 |
| BREAKING AND SEATING CONCRETE PAVEMENT | 11010 | sm | |
| CONCRETE PAVEMENT REPAIR | 41574 | cm | \$183.00 |
| CONTINUOUS DIAMOND GRINDING | 41576 | sm | \$2.69 |
| RUBBLIZING CONCRETE PAVEMENT | | sm | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE A | 60123 | m | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE D | 60133 | m | |
| GEOTEXTILE FABRIC, TYPE DF | 64503 | sm | \$1.20 |
| PIPE UNDERDRAIN, 150 mm | 61201 | m | \$4.43 |
| PIPE UNDERDRAIN, UNPERFORATED, 150 mm | 61211 | m | \$22.15 |
| R.C. APRON ENDWALLS FOR UNDERDRAIN | 61254 | EACH | \$125.00 |
| REMOVING PAVEMENT | 20401 | sm | |
| GEO-GRID | '90xxx | sm | \$1.75 |
| | | | |

ALTERNATE DESCRIPTION WORKSHEET

Version 3.3

07/13/98

8600–02–01 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| PARAMETER | UNITS | ALT 1 VALUE | ALT 2 VALUE | ALT 3 VALUE | ALT 4 VALUE | ALT 5 VALUE | ALT 6 VALUE |
|---|--------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| RURAL OR URBAN PROJECT | R/U | 1 | 1 | 1 | | */1EUE | VALUL |
| ROADWAY WIDTH | m | 10.80 | 10.80 | 10.80 | 1 | | |
| PAVEMENT STRUCTURE WIDTH | m | 7.20 | | | | | |
| TOTAL PAVED SHOULDER WIDTH | m | 1.80 | 1.80 | 1.BC | | | |
| CONCRETE RDWY PAVEMENT THICKNESS | mm | 175 | | | | | |
| CONCRETE SHOULDER THICKNESS | mm | 175 | | | | | |
| AC RDWY PAVEMENT MIX TYPE | HV/MV/LV | | MV | MV | | | |
| TOTAL AC RDWY PAVEMENT THICKNESS | mm | | 125 | | 125 | | |
| VIRGIN AC RDWY PAVEMENT THICKNESS | mm | | 125 | | | | |
| % OF ASPHALT CEMENT USED | % | | 6.0 | | | | |
| RECYCLED AC RDWY PAVEMENT THICKNESS | mm | | | | | | |
| % OF ASPHALT CEMENT USED | % | | | | | | |
| % RAP | % | | | | | | |
| AC SHOULDER PAVEMENT MIX TYPE | HV/MV/LV | | MV | mv | | | |
| TOTAL AC SHOULDER PAVEMENT THICKNESS | mm | | 125 | 140 | | | |
| VIRGIN AC SHOULDER THICKNESS | mm | | 125 | 140 | | | |
| RECYCLED AC SHOULDER THICKNESS | mm | | | | | | |
| % OF ASPHALT CEMENT USED | % | | 6.0 | 6.0 | | | |
| ASPHALTIC CONCRETE PAVEMENT WT. | kg/sm/mm | 2.35 | 2.35 | 2.35 | | | 2.35 |
| TACK COAT COVERAGE | L/sm | 0.113 | 0.113 | | | | 0.113 |
| WHICH LAYER IS THE DRAINAGE LAYER? | 0-4 | 0 | 0 | 0 | <u> </u> | | |
| CRUSHED AGG. BASE COURSE THICKNESS | mm | 150.00 | 275.00 | 300.00 | 0 | I | |
| UNIT WT OF CABC OPEN GRADED BASE COURSE #1 THICKNESS | Mg/cm | 2.4 | 2.4 | 2.4 | | | |
| UNIT WT OF OGBC #1 | mm | | 0 | 0 | 0 | | |
| OPEN GRADED BASE COURSE #2 THICKNESS | <u>Mg/cm</u> mm | - | | 0 | | | |
| UNIT WT OF OGBC #2 | Mg/cm | | | | 0 | | |
| BREAKER RUN THICKNESS | mm | | 0 | 0 | 0 | | |
| UNIT WT OF BREAKER RUN | Mg/cm | | ······ | 0 | v | | |
| ASPHALTIC STABILIZED B.C. THICKNESS | mm | | | | | | |
| % OF ASPHALTIC CEMENT USED | % | | | | | | |
| UNIT WT OF AC STABILIZED BASE COURSE | Mg/cm | | | | | | |
| P.C. STABILIZED BASE COURSE THICKNESS | mm | | | | | | |
| UNIT WT OF PCC STABILIZED BASE COURSE | Mg/cm | | | | | | |
| GRANULAR SUBBASE COURSE THICKNESS | mm | 275 | 275 | 0 | 0 | | |
| OTHER #1 (STRUCTURE WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| OTHER #2 (ROADWAY WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| EXISTING PAVEMENT WIDTH EXISTING PAVEMENT THICKNESS | m | | 6.70 | 6.70 | | | |
| % OF PROJECT LENGTH FOR CURB & GUTTER | mm | | | | | | |
| TYPE OF CURB & GUTTER | <u>%</u> | | | | | | |
| % OF PROJECT LENGTH FOR GEOTEXTILE FABRIC | A/D | | | | | | |
| % OF PROJECT LENGTH FOR UNDERDRAINS | % | | | | | | |
| % OF PROJECT LENGTH FOR TACK COATING | % | | | | | | |
| TOTAL m2 OF CRCP STEEL REINFORCEMENT | /o sm | | 66 | 66 | | | |
| %OF PROJECT LENGTH FOR MILL & RELAY AC PAV'T | <u>%</u> | | | | | | |
| %OF PROJECT PAV'T AREA FOR AC SURF PATCHING | % | | | | | | |
| %OF PROJECT LENGTH FOR PULVERIZING AC PAV'T | % | | | | | | |
| MILLING DEPTH | mm | | | | | | |
| %OF PROJECT LENGTH FOR SALV AC PAV'T MILLING | % | | | | | | |
| %OF PROJECT LENGTH FOR SALV AC PAV'T | % | | | | | | |
| % OF PROJECT LENGTH FOR DIAMOND GRINDING | % | | | | | | |
| %OF PROJECT LENGTH FOR PCC PAV'T REPAIR | % | | | | | | |
| #OF PAV'T TIES PER METER OF LONGIT. LENGTH | EACH | | | | | | |
| #DOWELS PER PATCH JOINT | EACH | | | | | | |
| AVG. LENGTH OF PCC PATCH | m | | | | | | |
| %OF PROJECT LENGTH FOR CRACK & SEAT | % | | | | | | |
| %OF PROJECT LENGTH FOR BREAK & SEAT | % | | | | | | |
| 60F PROJECT LENGTH FOR RUBBLIZING | % | | | | | | |
| | sm | | | | | | |
| TOTAL AREA FOR CONCRETE BASE PATCHING | sm | | | | | | |
| | sm | | | | | | |
| | sm | | | | | | |
| | sm | | | |] | | |
| 6OF PROJECT LENGTH FOR PAVEMENT REMOVAL | % | | | | | | |
| | | | | | | | |
| | | | | | | | |
| ASE LAYER: (FOR QUANTITY CALCULATIONS) | | | | | | | |
| – NONE E – AC STABILIZED | Г | | | | ALT 4 | ALT - | |
| | | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |

 X - NONE
 E - AC STABIL

 A - CABC
 F - PC STABIL

 B - OGBC #1
 G - GRANULAI

 C - OGBC #2
 H - OTHER #1

 D - BREAKER RUN
 I - OTHER #2

4

| E – AC STABILIZED | | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |
|-------------------|---------|-------|-------|---|-------|-------|-------|
| F – PC STABILIZED | LAYER 1 | а | а | | x | ••• | x |
| G – GRANULAR | LAYER 2 | g | g | ••••••••••••••••••••••••••••••••••••••• | * | | |
| H – OTHER #1 | LAYER 3 | X | x | | | | |
| I – OTHER #2 | LAYER 4 | X | X | · A · · · · · · · · · · · · · · · · · · | X | | x |

ALTERNATE QUANTITIES AND COSTS

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

| | | ALTERNATI | /E #1 | ALTERNAT | E #2 | ALTERNAT | E #3 |
|---------------------------------------|----------|-----------|--------------|-------------------------------|--------------|--------------|-------------|
| PARAMETER | UNITS | QUANTITY | COST | Asphalt/base/sand QUANTITY | | Asphalt/base | |
| CONCRETE PAVEMENT (RDWY) | sm | 7.200.0 | \$129,600.00 | | COST | QUANTITY | COST |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 1,800.0 | \$32,400.00 | . 0.0 | \$0.00 | 0.0 | \$0. |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0. |
| VIRGIN AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 2,115.0 | \$34,897.50 | 2,368.8 | \$39,085. |
| RECYCLED AC PAVEMENT (RDWY) | Mg | | \$0.00 | 528.8 | \$8,724.38 | 592.2 | \$9,771.3 |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. |
| ASPHALT CEMENT | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CRUSHED AGG. BASE COURSE | Mg | | \$0.00 | 158.6 | \$24,586.88 | 177.7 | \$27,537.3 |
| OPEN GRADED BASE COURSE #1 | Mg | 5,658.0 | \$43,849.50 | 9,204.0 | \$71,331.00 | 10,239,4 | \$79,355.0 |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| GRANULAR SUBBASE COURSE | cm | 3,987.5 | \$13,158.75 | 4,152.5 | \$13,703.25 | 0.0 | |
| CURB & GUTTER | m | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| TYPE DF GEOTEXTILE FABRIC | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| 150 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.0 |
| 50mm PIPE UNDERDRAINS, UNPERFORATED | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| APRON ENDWALLS FOR UNDERDRAINS | EACH | 0 | \$0.00 | | \$0.00 | 0.0 | \$0.0 |
| ACK COATING | <u>I</u> | 0.0 | \$0.00 | 0 | \$0.00 | 0 | \$0.0 |
| MILL & RELAY AC PAVEMENT | sm | 0.0 | | 2,013.7 | \$2,013.66 | 2,013.7 | \$2,013.6 |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | Ma | | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC SURFACE PATCHING | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| PULVERIZING AC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONTINUOUS DIAMOND GRINDING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE PAVEMENT REPAIR | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CRCP REINFORCEMENT | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| PAVEMENT TIES | EACH | 0 | \$0.00 | 0 | \$0.00 | 0.0 | |
| DOWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.0 |
| CRACK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| BREAK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| UBBLIZING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.0 |
| ASPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE WIDENING | sm | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC BASE COURSE WIDENING | Mg | · 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE COURSE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| EMOVING PAVEMENT | sm | | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ost Adjustment-see comps | 3111 | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| · · · · · · · · · · · · · · · · · · · | | | | | | | |
| THER BASE #1 | | | | | | | |
| THER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | |
| | Mg | 0.0 | | 0.0 | | 0.0 | |
| TERNATIVE TOTAL | | | | | | | |
| | | | \$219,008.25 | | \$155,256.66 | | \$157,762.5 |

| D D D D D D D D D D | | ALTERNAT Existing Structure | E#4 | ALTERNAT 0 | E#5 | ALTERNAT 0 | E#6 |
|--------------------------------------|-------|--------------------------------|--------|---|--------|---------------|-------|
| PARAMETER | UNITS | QUANTITY | COST | QUANTITY | COST | QUANTITY | COST |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| /IRGIN AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | |
| RECYCLED AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALT CEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| CRUSHED AGG. BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| OPEN GRADED BASE COURSE #2 | Mg | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.0 |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | the second se | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| GRANULAR SUBBASE COURSE | cm | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CURB & GUTTER | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| YPE DF GEOTEXTILE FABRIC | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| 50 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| 50mm PIPE UNDERDRAINS, UNPERFORATED | m | | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| PRON ENDWALLS FOR UNDERDRAINS | EACH | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ACK COATING | 1 | 0 | \$0.00 | 0 | \$0.00 | | \$0.0 |
| AILL & RELAY AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | Ma | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| | M | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONTINUOUS DIAMOND GRINDING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE PAVEMENT REPAIR | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| PAVEMENT TIES | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| DOWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.0 |
| | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.0 |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| UBBLIZING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| SPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| ONCRETE BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ONCRETE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| SPHALTIC BASE COURSE WIDENING | Mg | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.0 |
| ONCRETE BASE COURSE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| EMOVING PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ost Adjustment-see comps | | | | 0.0 | \$0.00 | 0.0 | \$0.0 |
| THER BASE #1 | Mg | 0.0 | | 0.0 | | | |
| THER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | |
| TERNATIVE TOTAL | | | \$0.00 | | \$0.00 | | \$0.0 |

ALTERNATE MAINTENANCE Version 3.3

8600-02-01 Chippewa Falls – Comell Jim Falls – CTH R STH 178 Chippewa

MAINTENANCE COSTS: (CURRENT YEAR)

| | INCREM | | INCREM | ENT 2 | INCREME | ENT 3 | INCREM | -NT 4 | INCREME | NTC |
|-----------------------------------|--------------|------------|--------------|------------|------------------|------------|------------------|------------|------------------|-----|
| ALTERNATE TITLE | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM | TO YEAR | FROM | TO |
| Asphalt/base/sand | | | \$4,970.00 | 18 | 24 \$4.970.00 | | 27 \$4,970.00 | 28 | 33 \$1,250.00 | |
| YEARLY COST Asphalt/base | \$1,250,00 | 3 | \$1,550.00 | 10 | 16 \$1,250.00 | | 22 \$1,550.00 | 23 | 28 \$1,250.00 | |
| YEARLY COST Existing Structure | \$1,250.00 | | \$1,550.00 | | 16 \$1,250.00 | 17 | \$1,550.00 | 23 | 28 \$1,250.00 | |
| YEARLY COST | | | | | | | | | | |
| YEARLY COST 0 | | | | | | | | | | |
| YEARLY COST | | | | | | | | | | |

07/13/98

MAINTENANCE COSTS: (CURRENT YEAR)

.

| | INCREME | | INCREME | NT 7 | INCREME | NT 8 | INCREM | AENT 9 | INCREM | |
|----------------------------------|-------------------|------------|------------------|-------------|------------------|------------|--------|------------|--------|------|
| ALTERNATE TITLE | FROM YEAR | TO YEAR | FROM YEAR | TO. YEAR | FROM YEAR | TO YEAR | FROM | TO YEAR | FROM | то |
| YEARLY COST | 37 \$1,550.00 | 38 | 43 \$1,250.00 | 44 | 47 \$1,550.90 | 48 | | | YEAR | YEAR |
| sphalt/base/sand YEARLY COST | 34 \$1,550.00 | | 40 \$1,250.00 | 41 | 47 | 48 | | | | |
| sphalt/base YEARLY COST | \$4 \$1,550.00 | 35 | 40 \$1,250.00 | 41 | 47 \$1,550.00 | 48 | | | | |
| xisting Structure YEARLY COST | | | | | | | | | | |
| 0 YEARLY COST | | | | | | | | | | |
| 0 YEARLY COST | | | | | | | | | | |

ALTERNATE REHABILITATION Version 3.3

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

ASPHALT PAVEMENT REHABILITATION SCHEMES:

| | | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders | MILUNG DEPTH (mm) | % OF PROJECT for SURF. PATCHING | OVERLAY THICKNESS (mm) | MIX TYPE (HV,MV,LV) | % AC in OVERLAY MIX | OTHER COSTS | OTHER COST DESCRIPTION |
|---|------------|---|----------------------|---------------------------------------|---------------------------|------------------------|------------------------|----------------|--|
| • | AC2 AC3 | 2 | 25 | 0.0 0.0 | 75 90 | <u>rav</u> nav | <u>6.0</u> | | |
| | AC4 | 2 | | 0.0 | 100 | <u>IUN</u> | 5.0 | | Similar costs to millårelay and nave asphalt |
| | AC5 AC6 | | | | | | | | |
| | AC7 | | | | | | | | |
| L | AC8 AC9 | RECONSTRUCT: USI | | FR THICKNESSES | | | | | |
| | | | | EN INIORAE33E3 | | | 8 | | |

CONCRETE PAVEMENT REHABILITATION SCHEMES:

| Repair – Grind | | | | % OF PROJECT | | | |
|----------------|--------------|------------------|-------|-------------------|--------------------|--------|------------------------|
| SCHEMES | | AVG PATCH LENGTH | | for | | OTHER | |
| DO4 | % PCC REPAIR | in m | JOINT | PCC Base Patching | | | OTHER COST DESCRIPTION |
| PC1 PC2 | <u></u> 0.0 | 1.6 | 32 | 0.0 | & Continuous Grind | ****** | OTTENOOST DESCRIPTION |
| DCO | 0.0 | 1.8 | 52 | 10 | & Continuous Grind | | |
| FC3 | | | | | & Continuous Grind | | |
| | | | | | | | |

| Repair – Overlav | | | | % OF PROJECT | % OF PROJECT | | | 1 | OVERLAY LIMITS | | |
|------------------|--------------|------------------|-----------------------|-------------------|------------------|----------------|------------|-------------|---------------------|-------|------------------------|
| SCHEMES | % PCC REPAIR | AVG PATCH LENGTH | # DOWELS PER JOINT | for | for | OVERLAY | MIX TYPE | % AC in | 1: RDWY ONLY | OTHER | |
| PC4 | 0. | 0 | JUINI | PCC Base Patching | AC Base Patching | THICKNESS (mm) | (HV,MV,LV) | OVERLAY MIX | 2: RDWY & Shoulders | | OTHER COST DESCRIPTION |
| PC5 | | 0 | 10 | | 6.0 | 0 | | 5.0 | 2 | | |
| PC6 | | | | | <u></u> | 75 | 107 | 5.0 | 2 | | |
| | | | | | | | | | | | |

| .Mill – Repair – Overlay SCHEMES PC7 PC8 PC9 | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders 2:RDWY & Shoulders | mm) % PCC REPAIR 75 0.0 | AVG PATCH LENGTH in m | JOINT | % OF PROJECT for PCC Base Patching 2.05 | 0.0 | OVERLAY THICKNESS (mm) 75 | MIX TYPE (HV,MV,LV) | % AC n OVERLAY MIX 8.0 | OTHER COSTS |
|--|---|----------------------------|--------------------------|-------|--|-----|---------------------------------|------------------------|------------------------------|----------------|
| PC7 OTHER COST DESCRIPTION | | | | | | | i | | | |

PC8 OTHER COST DESCRIPTION PC9 OTHER COST DESCRIPTION

| | A | | |
|--------|-------------------------------|-------|------------------------|
| SCHEME | | OTHER | |
| | CONTINUOUS DIAMOND GRIND ONLY | COSTS | OTHER COST DESCRIPTION |
| | | | |
| | | | |

ALTERNATE REHABILITATION SCENARIOS:

REHABILITATION COSTS Т ALT #1.

| | | PUL | | | | | | | | | | |
|--------------------------------------|---------|------|-----------------|----------|-------------------|-----------------|----------|--------------|-----------------|----------|--------------------|-----------------|
| (COSTS ARE CURRENT YEAR) | SPACING | TYPE | CURRENT YR COST | ALT. #2: | Asphalt/base/sand | | ALT. #3: | Asphalt/base | | ALT, #4: | Existing Structure | |
| FIRST REHABILITATION | | | | SPACING | TYPE | CURRENT YR COST | SPACING | TYPE | CURRENT YR COST | | | |
| SECOND REHABILITATION | | 1564 | \$14,742.00 | | AC2 | \$57,402.45 | | A A CO. | | | TYPE | CURRENT YR COST |
| THIRD REHABILITATION | 31 | PC5 | \$60,212.25 | | ACS | \$66,438,90 | | | \$57,402.45 | | | \$0.00 |
| | 10 | PG7 | \$61,101,90 | | 47.8 | | | 2 803 | \$66,438.90 | | | \$0.00 |
| FOURTH REHABILITATION | | | | | - // Sec. 8 | \$70,222.41 | <u></u> | 2 409 | \$78,407.46 | | | \$0.00 |
| FIFTH REHABILITATION | | 1 | \$0.00 | | + | \$0.00 | | | \$0.00 | | | |
| EXPECTED LIFE OF LAST REHABILITATION | 10 | 5 | | | | \$0.00 | | | \$0.00 | | | \$0.00 |
| TOTAL LIFE | | 4 | | | <u>E</u> | | | 2 | | | <u></u> | \$0.00 |
| TOTALLIFE | u 50 | 1 | | 52 | 2 | | | 끰 | | | 2 | |
| | | | - | | | | 13 | <u> </u> | | 1 1 | al | |

07/13/98

LIFE CYCLE COST ANALYSIS

8600-02-01

Version 3.3

| | | Chippewa Falls – Cor Jim Falls – CTH R STH 178 Chippewa | rnell | | | |
|---|-------------------------------|--|---|------------------------------|------------|--------|
| CURRENT YEAR CONSTRUCTION YEAR DESIGN YEAR ANALYSIS PERIOD | 1998 2002 2022 50.0 | PROJECT L ANALYSIS | T RATE (%) ENGTH (Km) BASIS (P/M) | 5.0 1.00 M | | |
| TERMINAL SALVAGE VALUE | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
| PRESENT WORTH COSTS: (CURRENT YEAR) | | | | | | |
| INITIAL CONSTRUCTION COSTS | ALT. 1 PCC \$180,178,63 | ALT. 2 Asphalt/base/sand \$127,730,04 | | ALT. 4 Existing Structure | ALT.5 0 | ALT. 6 |
| | \$100,170.03 | φ127,730.04 | \$129,791.60 | \$0.00 | \$0.00 | \$0 |

| | | +200;200:00 | φ170,151.0Z | \$101,110.49 | \$0.00 | \$0.00 | \$0.00 | 4 |
|-------|------------------------------|--------------|--------------|--------------|--------------|--------|--------|---|
| | TOTAL FACILITY COSTS | \$209,268.35 | \$178,151.02 | \$181,116.49 | #0.00 | | | |
| 12000 | | | | | | | | |
| | | | (\$1,292.49) | (\$1,443.14) | \$0.00 | \$0.00 | \$0.00 | |
| | REHABILITATION SALVAGE VALUE | \$0.00 | | \$0.00 | +0.00 | | | |
| | TERMINAL SALVAGE VALE | \$0.00 | \$0.00 | \$0,00 | \$0.00 | | | |
| | | \$5,916.56 | +-, | \$3,441.68 | \$0.00 | \$0.00 | \$0.00 | |
| | MAINTENANCE COSTS | E OIC FO | | | +0.00 | | \$0.00 | |
| | REHABILITATION COSTS | \$23,173,16 | \$48,271.80 | \$49,326.35 | \$0.00 | | | |
| | INITIAL CONSTRUCTION COSTS | \$180,178.63 | + | \$129,791.60 | \$0.00 | \$0.00 | \$0.00 | |
| | | | | | | | | |

EQUIVALENT UNIFORM ANNUAL COSTS:

(OVER ANALYSIS PERIOD)

| | | 0 | | | | |
|------------------------------|-------------|-------------------|--------------|--------------------|--------|------------------|
| | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
| | PCC | Asphalt/base/sand | Asphalt/base | Existing Structure | 0 | |
| INITIAL CONSTRUCTION COSTS | \$9,869.60 | \$6,996.63 | \$7,109.56 | | \$0.00 | \$0.00 |
| REHABILITATION COSTS | \$1,269.35 | \$2,644.17 | \$2,701.94 | | \$0.00 | \$0.00 |
| MAINTENANCE COSTS | \$324.09 | \$188.52 | \$188.52 | | \$0.00 | \$0.00 |
| TERMINAL SALVAGE VALE | \$0.00 | \$0.00 | \$0.00 | | | \$0.00 \$0.00 |
| REHABILITATION SALVAGE VALUE | \$0.00 | (\$70.80) | | +0100 | \$0.00 | \$0.00 |
| | | | | | ψ0.00 | <u> </u> |
| TOTAL FACILITY COSTS | \$11,463.04 | \$9,758.53 | \$9,920.97 | \$0.00 | ¢0.00 | |
| | | | \$0,020.07 | \$0.00 | \$0.00 | \$0.00 |

07/13/98

| 7/14/98 | WISCONSIN DEPARTMENT OF TRANSPORTATION |
|----------|--|
| 06:26:33 | PAVEMENT INDEX FILE SYSTEM |
| | BROWSE OF CURRENT PDI & PSI VALUES |

| District 6 County Name CHIPPEWA | County | Number | 9 H: | ighway 1 | 78N |
|--|---|--|--|---|---|
| Enter S in Opt Field to View Section Data From Opt RP + Distance From Feature 011G + 0.000 CTH. Y 012K + 0.000 182ND. ST. 014G + 0.000 CTH Y INT 015 + 0.000 FINLEY LAKE RD | - To RP + 012K + 014G + 015 + 015 + | Distance 0.000 0.000 0.000 0.980 | Current ⁷ Surface Yr Ty 85 1 85 1 81 1 81 1 | * *PDI* Survey Yr No. 96 28 96 49 96 57 96 76 | *IRI* Survey Yr mm/m 97 1.83 97 1.40 97 2.38 97 3.08 |
| 015 + 0.980 160TH AVE. 017 + 0.000 210TH ST. 018 + 0.000 215TH ST. 018 + 0.680 SECTION 9 & 10 020 + 0.000 180TH AVE 022 + 0.000 190TH AVE. Surf Type 1=ACPM/FB,2=BRM, 3=ACPM/RB, 4=5 | 017 + 018 + 018 + 020 + 022 + 023 + JRCP, 5 | 0.000 0.680 0.000 0.000 0.000 | 87 1 79 1 88 1 84 1 88 1 83 2 0 d, 6=0 | 96 34 96 70 96 31 96 50 96 41 96 75 CRCP, 8=0 | 97 2.75 97 3.50 97 2.46 97 2.86 97 2.97 97 3.58 JPCP /d |

SELECT DATA TO VIEW, OR PRESS ENTER FOR MORE ENTER TO CONTINUEPF3 OR PF15 TO BROWSE MENUPA2 TO CANCEPF2 OR PF14 TO PRIMARY MENUPF12 OR PF24 TO LOGOFF CICSPA2 TO CANCE

IPFMBC

| Page: 1 Document Name: untitled | |
|---|---|
| 06:26:41 PAVEMENT INDE | T OF TRANSPORTATION IPFMBC X FILE SYSTEM PDI & PSI VALUES |
| District 6 County Name CHIPPEWA | County Number 9 Highway 178N |
| 024 + 0.000 CTH ZZ INT 024 + 1.250 SECTION 25 & 24 | To Surface Survey Survey RP + Distance Yr Ty Yr No. Yr mm/m 023 + 0.000 83 2 96 75 97 3.58 024 + 0.000 87 1 96 38 97 2.60 024 + 1.250 81 1 96 24 97 2.45 027 + 0.000 84 1 96 66 97 2.57 499E + 0.000 + + + + + |
| NO MORE SECTIONS FOR COUNTY & HIGHWAY ENTER TO CONTINUE PF3 OR PF2 OR PF14 TO PRIMARY MENU PF12 OR | |

CORRESPONDENCE/MEMORANDUM

Date: July 13, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: Traffic Forecast projection revisions Project 8600-02-01

This project has been in and out of the six year program for the last 5-10 years. There has been no recent specific traffic forecast done for this segment. For structural design purposes, I chose to use a construction year ADT of 2000 and a 20 year ADT of 2400. The truck percentage was rounded to 8%. The following two forecasts done in 1992 and 1995 give volumes for the roadway but are outdated.

TRAFFIC FORECAST

| PROJECT ID: | 8600-02-71 |
|---------------|-----------------------|
| COUNTY: | Chippewa |
| ROUTE: | STH 178 |
| LOCATION: | Int. w/ CTH Y to Int. |

| KEY | |
|----------------|------------|
| *000* 1991 Tra | ffic Count |
| -000-1994 For | ecast |
| (000) 2004 For | ecast |
| 000 2014 For | ecast |
| DESIGN VALU | JES |
| K100 | 11.6 |
| K50 | 12.4 |
| K30 | 13.1 |
| P(PHV) | 16.9 |
| T(DHV) | 6.2 |
| T(PHV) | 3.5 |
| D | 60/40 |
| K8(ADT) | |
| T(A8HV) | |
| TRUCK CLASS | |
| TRUCK TYPE | % ADT |
| 2D | 3.6 |
| 3AX | 1.4 |
| 2S1+2S2 | 0.7 |
| 3-S2 | 2.0 |
| DBL-BTM | 0.0 |
| TOTAL | 7.7 |

- NOTES ON THE ANALYSIS: 1. The functional classification of STH 178 over the
- project section is COLLECTOR; the seasonal ad justment factor group for the section is group 4.
- In developing this forecast, it was assumed that no new major traffic generators will be developed in the vicinity of the project section over the course of the forecast period.
- 4. In developing the forecast for the southern site, the the historical traffic count for 1975 was excluded from the analysis because it departed substantially
- from the trend in the other historical counts. 5. Truck percentages of ADT were obtained from a
- table of vehicle type percentages by functional class and urban/rural area because a vehicle type counter is not located on STH 178.
- Design parameters are calculated using the design year ADT for the northern most forecast location (3100).



| COUNTY ROUTE: | ON: STH 6 | 78 | o STH27 | • | <u>KEY</u> *000* -000- (000) 000 | 1993 AD 1999 AD 2009 AD 2019 AD | T& Forecasting SeTE-Mail ID: ERLTCompleted: 26- | |
|------------------|-----------------------------|---------------|--------------|--|--|--|---|-----------------------------------|
| N | | | | $ \begin{array}{c} -700-\\(775)\\\underline{850}\\-200-\\(225)\\250\end{array} $ 178 | 64 | | See Detail *450* -900- (1000) 1100 | Cornell |
| -1 (1 | 990* 150– 350) 550 | | | Detail R *580* | -400- (450) 475 -200- (200) 225 | *1500* | 178 *1700* -1950- (2350) 2750 | -2450- (2900) 3350 |
| | No Bu | ild | | -600-/ (650) 700 | (178) | -1750- (2100) 2500 | | (27) |
| ESIGN | VALUES | TRUCK C | LASS | Notes on the Forecast: | | | REFERENCES | |
| 100 50 | | TRUCK | | 1. Historic and projected t | raffic volumes repres | ent Axle – | 4 | flic", available coverage counts, |
| 10 | 12.3 12.9 | TYPE 2D | % ADT 3.6 | Adjusted AADT. Pre - | 1990 counts are fact | ored using | 1975 - 1993. | |
| ° PHV) | | 3AX | | indicated Axle – Adjust 2. This forecast assumes th | nent ractors (A-Al | 1). traffic | 2. "Official Poulation Estim | ates, Demographic Services |
| DHÝ) | | 2S1+2S2 | 0.7 | generators will be develo | ped in the project ar | uamo ea durina | Center, DOA. | |
| PHV) | 3.5 | 3– <i>S</i> 2 | 2.0 | the forecast period. | | | | |
| | | | 0.0 | 3. STH 64 has an axle – ac | ljustment factor of .9 | 3 and is | | |
| B(ADT) A8HV) | NA NA | TOTAL | 7.7 | in Factor Group 4, indica | ting moderate seaso | nal traffic | | |
| | | | | fluctuation. | | | | |

CONCEPT DEFINITION REPORT

Date: 07/17/96

To: Michael A. Cass (P.E.) From: District 6

- Related ID(s): 8600-02-71(Const) I. Design ID: 8600-02-01 Highway No. or Local Road Name: STH 178 8600-02-21 (R/W) Title: CHIPPEWA FALLS - CORNELL ROAD County: CHIPPEWA Length: 7.4 Miles 11.9 km Functional Class: Major Collector Current ADT: 1650 (1993) LOCATION: CTH Y - CTH R
- Roadway Conditions: II. A. Pavement: Type: AC Width: 22 Year: 1981 PSI: 2.69 (1993) PDI: 30 (1994) Shoulder: Type: Gravel Width: 2 Accident Rate: 480 Year: 1995 Substandard Alignment: Horizontal: Yes Vertical: Yes
 - Β. Structure: (may be continued on back side) Length: 86.5 ft, 26.4 m Year Constructed: 1942 SR: 80.5 Type: DECK GIRDER Bridge Number: B-09-0682 Clear Roadway Width: 27.6 RS: 89.4

JUSTIFICATION: Accident rate is 480 vs State ave of 222 because of narrow shoulders, sharp horiz curvature and short vertical and horiz sight distance. There are many power poles and trees in clear zone.

PROPOSED IMPROVEMENT: Grade, Base, Asphaltic Surface to C3 standards III. with a 24 ft surface on a 36 ft roadway with a 30 ft clear zone.

> A. Environmental documentation type: III ER B. Improvement Type: RECST PMSID: 98060020201 C. Cost: \$ 3,850,000 Program Year: 2002 Program: 3334 D. Local Participation: \$ No Access Control: No

DISTRICT 6 APPROVAL Project pervisor

Planning Supervisor

Concept Definition Report Project: 8600-02-01

Date: 07/17/96 CC: Gerry Feiler - Rm 951, Len Stanek - Rm 651, Bureau of Environment - Rm 451

Gene Hoelker-FHWA

District 6 Geographic Information System

- Page: 1 of 2
- $\frac{17}{\sqrt{22}} \frac{1-16}{\sqrt{22}}$



Page: 1 Document Name: untitled

| 7/14/98 06:26:08 | PAVEMENT IN | ENT OF TRANSPORTATION DEX FILE SYSTEM NT PDI & PSI VALUES | IP |
|---------------------|---------------------------|---|-----------------|
| District 6 | County Name CHIPPEWA | County Number 9 | Highway 178N |
| Enter S in Op | t Field to View Section I | Data *Curi | rent* *PDI* *IR |

| From | | То | Surface | Survey | Survey |
|--------------------|------------------------|------------------|----------|----------|---------|
| Opt RP + Distance | From Feature | RP + Distance | e Yr Ty | Yr No. | Yr mm/m |
| 001 + 0.000 | BAY ST INT | 002 + 0.000 | 55 1 | 96 91 | 97 5.16 |
| 002 + 0.000 | FRONT ST INT | 003 + 0.000 | 81 1 | 96 34 | 97 3.17 |
| 003 + 0.000 | CTH I (KENNEDY ST) | 004 + 0.000 | 85 1 | 96 54 | 97 2.00 |
| 004 + 0.000 | CTH S INT | 005K + 0.000 | 85 1 | 96 33 | 97 1.80 |
| 005K + 0.000 | 93rd ave | 006G + 0.000 | 85 1 | 96 33 | 97 1.75 |
| 006G + 0.000 | 101ST AVE | 007D + 0.000 | 85 1 | 96 33 | 97 1.96 |
| 007D + 0.000 | 110TH AVE | 008G + 0.000 | 85 1 | 96 85 | 97 2.15 |
| 008G + 0.000 | 120TH AVE | 009K + 0.000 | 85 1 | 96 54 | 97 2.00 |
| 009K + 0.000 | 170TH ST | 011G + 0.000 | 85 1 | 96 21 | 97 1.85 |
| 011G + 0.000 | СТН. Ү | 012K + 0.000 | 85 1 | 96 28 | 97 1.83 |
| Surf Type 1=ACPM/F | B,2=BRM, 3=ACPM/RB, 4= | =JRCP, 5=JPCP w/ | o d, 6=0 | CRCP, 8= | JPCP /d |

SELECT DATA TO VIEW, OR PRESS ENTER FOR MOREENTER TO CONTINUEPF3 OR PF15 TO BROWSE MENUPF2 OR PF14 TO PRIMARY MENUPF12 OR PF24 TO LOGOFF CICS

PA2 TO CANCE

IPFMBC

IRI

CORRESPONDENCE/MEMORANDUM

| Date: | June 24, 1998 |
|----------|---|
| To: | File |
| From: | Randy W. Luedtke, P.E. District#6 Pavement Design Engineer |
| Subject: | Pavement Documentation Project I.D. 8600-03-31 or 01 Chippewa - Cornell Road CTH I - CTH Y STH 178 Chippewa County |

This project was initially scoped or programmed as a Rut Fill type project. Since that time, after in-house discussion and coordination with county officials, it was agreed that a thin overlay is a better choice. Due to the existing rutting a lower leveling course will need to be placed to fill in the ruts before a surface layer is placed. The contractor *should not* be allowed to place the total plan asphalt thickness in one lift.

At this point in time this pavement treatment is considered as a roadway maintenance type project. No formal documentation of the pavement selection or LCCA is required beyond what is stated in the Design Study Report.

The following typical should be done:

- A. A lower level should be initially placed to fill in the ruts(pavement distortion) in the wheel paths. It should be stated as a variable depth layer ranging from ³/₄" to 1". This note may cause a red flag but it can be achieved with a grade #3 surface mix.
- B. The upper layer or surface pass should be constructed of $1\frac{1}{4} 1\frac{1}{2}$ ". If the programming designation or RDMNT threshold of $2\frac{1}{2}$ " is waived the surface lift should be increased to 2 inches.
- C. Designate the mix as MV grade #3(surface mix) for both layers.

It is assumed that this treatment will provide an additional 8-10 years of service versus 3-5 years for the typical rut fill.

There is a possibility that some areas may be excavated to alleviate frost heave areas. A typical depth of 5" asphalt over 12" of base course should be used for those areas. The surface thickness should match the adjacent segments.

Reviewed:

Approved:

Michael S. Ostrowski, P.E. PD Manager

LAST -> RWL <u>8/10</u> MSO <u>8/4</u> Sin Koening <u>8/3</u>

Richard J. Shermo, P.E. PD Area Supervisor
| State of Wisconsin | |
|--------------------|--|
|--------------------|--|

| Date: | June 24, 1998 |
|----------|---|
| To: | File |
| From: | Randy W. Luedtke, P.E. District#6 Pavement Design Engineer |
| Subject: | Pavement Documentation Project I.D. 8600-03-31 or 01 Chippewa - Cornell Road CTH I - CTH Y STH 178 Chippewa County |

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Reviewed:

Approved:

Michael S. Ostrowski, P.E. PD Manager

LAST -> RWL <u>8/10</u> MSO <u>8/4</u> Sin Koening <u>8/3</u>

Richard J. Shermo, P.E. PD Area Supervisor Date: January 7, 1997

To: File

From: Randy W. Luedtke, P.E. District Pavement Design Engineer

Subject: VERY PRELIMINARY PAVEMENT OPTIONS Project 8600-02-31 Chippewa Falls-Cornell CTH Y - CTH R STH 178 Chippewa County

This project involves the portion of STH 178 from Jim Falls northerly to CTH R. This project area was designated previously for a roadway maintenance type project in 1998, but now the roadway is re-evaluated in comparision to 100km/hr(60 m.p.h.) standards. To facilitate preliminary design work, a preliminary depth to subgrade was requested. This document was prepared for preliminary project costing analysis and preliminary template design.

TRAFFIC PROJECTIONS

THE FOLLOWING TRAFFIC PROJECTIONS USED MAY NOT BE VALID FOR FINAL PAVEMENT DESIGN.---PRELIMINARY ONLY!!

STH 178

The construction year (0 year) ADT is 2000 and the 20 year ADT is 2400.

Truck percentages are as follows:

| TRUCK TYPE | | <u>%</u> |
|------------|-------|------------|
| 2D | | 3.6 |
| 3AX | | 1.3 |
| 281,282 | | 0.8 |
| 3-S2 | - | 2.3 |
| DBL. BTM | | <u>0.0</u> |
| | TOTAL | 8.0 |

PROPOSED IMPROVEMENT

This project is being evaluated to be brought up to 60 mph standards.

SOIL ENGINEERING FACTORS

The soils on this project consist of Chetek soils. The DGI is 14 with a soil support value of 4.0.

ALTERNATES EVALUATED VERY PRELIMINARY ONLY!!!

A twenty year service life was used.

For the relocation situation, a rigid and a flexible structure has been provided.

Relocation:

- J - P

The first alternate is: 175mm(7") PCC over 150mm(6") of DGBC over 225mm(9") sand lift

DEPTH TO SUBGRADE: 750mm(30")

The second alternate is: 125mm(5") MV Asphalt over 275mm(11")DGBC over 275mm(11") sand lift DEPTH TO SUBGRADE: 675mm(27")

Shoulder widening areas: 115mm(4.5") MV Asphalt over 150mm(6") of milled & relayed of the existing surface*

*short areas of gravel lifts may be an option to correct slight vertical profile deficiencies.

No Life Cycle Cost Analysis has been done at this time. Other pavement options may be evaluated at a later date.

Randy W. Luedtke, P.E.

RIGID PAVEMENT DESIGN WORKSHEET

Version 3.3

8600–02–31 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa





TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT DESIGN YEAR DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|-------|
| 2,000 |
| 2022 |
| 2,400 |
| 0.50 |
| 1.00 |
| 20.0 |
| 1,100 |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL'S |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 1.2 | 17 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.6 | 5 |
| 3S-2 | 2.3 | 1,100 | 25 | 1.6 | 40 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.1 | 0 |
| DESIGN LANE DAILY ESAL'S | 8.0 | | | | 74 |
| DESIGN LANE TOTAL LIFE ESAL's | | | | | 540,200 |

SOILS:

MODULUS OF SUBGRADE REACTION (K)

30

THICKNESSES:

CALCULATED PAVEMENT THICKNESS PAVEMENT THICKNESS TO BE USED

155 175

FLEXIBLE PAVEMENT DESIGN WORKSHEET

Version 3.3

01/06/97

8600-02-31 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT **DESIGN YEAR DESIGN YEAR ADT** DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|-------|
| 2,000 |
| 2022 |
| 2,400 |
| 0.50 |
| 1.00 |
| 20.0 |
| 1,100 |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL's |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3-SU | 1.3 | 1,100 | 14 | 0.8 | 11 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.5 | 4 |
| 3S-2 | 2.3 | 1,100 | 25 | 0.9 | 23 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.0 | 0 |
| DESIGN LANE DAILY ESAL'S | 8.0 | | | | 50 |
| DESIGN LANE TOTAL LIFE ESAL'S | | | | | 365,000 |

SOILS:

DESIGN GROUP INDEX SOIL SUPPORT VALUE FROST INDEX

| | 14 |
|-----|-----|
| | 4.0 |
| F-3 | |

3.0

DESIGN - SN VALUE & MIX TYPE:

SERVICEABILITY INDEX REQUIRED SN VALUE

ASPHALT MIX TYPE: MV 3.49

ALTERNATE DESIGN:

| | Asphalt/surface mill | | | Asphalt/Pulverize&Relay | | |
|----------------------------|----------------------|---------|------|-------------------------|-----------|------|
| LAYER | THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN |
| SURFACE: | | SURFACE | | | SURFACE | |
| ASPHALTIC CONCRETE | 100 | 0.0173 | 1.73 | 115 | 0.0173 | 1.99 |
| EXISTING ASPHALT | 100 | 0.0100 | 1.00 | | | 0.00 |
| BASE COURSE: | BAS | E | | | BASE | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 |
| OPEN GRADED BASE COURSE #1 | | | 0.00 | | | 0.00 |
| OPEN GRADED BASE COURSE #2 | | | 0.00 | | | 0.00 |
| EXISTING BASE | | 0.0039 | 0.00 | | 0.0039 | 0.00 |
| EXISTING AC | | | 0.00 | | | 0.00 |
| PULVERIZED AC | | | 0.00 | 150 | 0.0100 | 1.50 |
| EXISTING PCC | | | 0.00 | | | 0.00 |
| RUBBLIZED PCC | | | 0.00 | | | 0.00 |
| CRACK (BREAK) & SEAT PCC | | | 0.00 | | | 0.00 |
| SUBBASE COURSE: | SUBB/ | ASE | | | SUBBASE | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 |
| BREAKER RUN | | | 0.00 | | | 0.00 |
| GRANULAR SUBBASE | | | 0.00 | | | 0.00 |
| EXISTING SAND LIFT | | 0.0025 | 0.00 | | 0.0025 | 0.00 |
| TOTAL SN VALUE | | | 2.73 | | L | 3.49 |
| | SN is Less Than | SNrea'd | | SN is Less Tha | n SNreq'd | |

N is Less Than SNreq'd

FLEXIBLE PAVEMENT DESIGN

ALTERNATE DESIGN:

| | Existing Structure | | | Asphalt/base/sand | | |
|----------------------------|--------------------|---------|------|-------------------|---------|------|
| LAYER | THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN |
| SURFACE: | | SURFACE | | | SURFACE | |
| ASPHALTIC CONCRETE | 125 | 0.0173 | 2.16 | 125 | 0.0173 | 2.16 |
| EXISTING ASPHALT | | | 0.00 | | | 0.00 |
| BASE COURSE: | | BASE | | | BASE | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | 275 | 0.0039 | 1.07 |
| OPEN GRADED BASE COURSE #1 | | | 0.00 | | | 0.00 |
| OPEN GRADED BASE COURSE #2 | | | 0.00 | | | 0.00 |
| EXISTING BASE | 125 | 0.0039 | 0.49 | | | 0.00 |
| EXISTING AC | | | 0.00 | | | 0.00 |
| PULVERIZED AC | | | 0.00 | | | 0.00 |
| EXISTING PCC | | | 0.00 | | | 0.00 |
| RUBBLIZED PCC | | | 0.00 | | | 0.00 |
| CRACK (BREAK) & SEAT PCC | | | 0.00 | | | 0.00 |
| SUBBASE COURSE: | | SUBBASE | | | SUBBASE | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 |
| BREAKER RUN | | | 0.00 | | | 0.00 |
| GRANULAR SUBBASE | | | 0.00 | 275 | 0.0012 | 0.33 |
| EXISTING SAND LIFT | | 0.0025 | 0.00 | | | 0.00 |
| TOTAL SN VALUE | | | 2.65 | | L | 3.57 |

SN is Less Than SNreq'd

PAVEMENT SURFACE FRICTION DESIGN

Version 3.3

01/06/97

8600-02-31 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

TRAFFIC:

| CONSTRUCTION YEAR ADT | 2,000 | | |
|--|--------|------------------|-------|
| DESIGN YEAR ADT | 2,400 | EXP. GROWTH RATE | 0.92% |
| DIRECTIONAL FACTOR (DF) | 0.50 | | |
| LANE DISTRIBUTION FACTOR (LDF) | 1.00 | | |
| % HEAVY VEHICLES (HV) | 8.0 | | |
| AC PAVEMENT AGE OR SERVICE LIFE (YR) | 15.0 | AC "AGE" ADT | 2,293 |
| AC LAVP AT SPECIFIED AGE (IN MILLIONS) | 5.876 | · | |
| PC PAVEMENT AGE OR SERVICE LIFE (YR) | 25.0 | PC "AGE" ADT | 2,512 |
| PC LAVP AT SPECIFIED AGE (IN MILLIONS) | 10.293 | | |

AGGREGATE PROPERTIES:



CONCRETE SURFACE FORMULA

In(FN40) = 3.99 - 0.0419In(LAVP) - 0.00129(DOLOMITE) + 0.00474(HV)

| FN40 AT SPECIFIED PAVEMENT AGE | 50.9 |
|---|--------|
| % PROBABILITY THAT CALCULATED VALUE IS < 35 | <0.05% |
| | |
| AGE (YR) WHEN FN40=35 | AGE>50 |

BID ITEM COSTS

١

0

Version 3.3

01/06/97

8600–02–31 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| | BID ITEM | | UNIT |
|--|----------|-------|----------|
| BID ITEM | # | UNITS | COST |
| ASPHALTIC MATERIAL FOR TACK COAT | 40204 | L | \$0.29 |
| ASPHALTIC MATERIAL FOR PLANT MIXES | 40501 | Mg | \$154.32 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE HV | 40712 | Mg | \$22.05 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE MV | 40713 | Mg | \$18.75 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE LV | 40714 | Mg | \$16.75 |
| RECYCLED ASPHALTIC SURFACE, TYPE HV | 90381 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE MV | 90382 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE LV | 90383 | Mg | |
| CONCRETE PAVEMENT, 150 mm | 41506 | sm | |
| CONCRETE PAVEMENT, 175 mm | 41507 | sm | \$18.00 |
| CONCRETE PAVEMENT, 200 mm | 41508 | sm | \$18.00 |
| CONCRETE PAVEMENT, 225 mm | 41509 | sm | \$20.25 |
| CONCRETE PAVEMENT, 250 mm | 41510 | sm | |
| CONCRETE PAVEMENT, 275 mm | 41511 | sm | |
| CONCRETE PAVEMENT, 300 mm | 41512 | sm | |
| CONCRETE WIDENING | 41530 | sm | |
| CONTINUOUS CONCRETE PAV'T REINFORCEMENT | 41551 | sm | |
| PAVEMENT TIES | 41571 | EACH | \$5.00 |
| DOWEL BARS | 41572 | EACH | \$5.00 |
| CRUSHED AGGREGATE BASE COURSE | 30404 | Mg | \$6.75 |
| OPEN GRADED BASE COURSE #1 | 30418 | Mg | \$8.25 |
| OPEN GRADED BASE COURSE #2 | 30420 | Mg | \$8.30 |
| ASPHALTIC BASE COURSE | 30601 | Mg | \$7.25 |
| ASPHALTIC BASE COURSE WIDENING | 30606 | Mg | |
| CONCRETE BASE COURSE | 30706-9 | sm | |
| CONCRETE BASE COURSE WIDENING | 30751 | sm | |
| BREAKER RUN | 30426 | Mg | \$6.00 |
| GRANULAR SUBBASE COURSE | 21201 | cm | \$3.30 |
| MILL AND RELAY ASPHALTIC CONCRETE PAVEMENT | | sm | \$0.86 |
| SALVAGED ASPHALTIC PAVEMENT | 41010 | Mg | |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | 41020 | Mg | \$7.72 |
| ASPHALTIC SURFACE, PATCHING | 41102 | Mg | |
| PULVERIZING ASPHALTIC CONCRETE PAVEMENT | | sm | \$0.86 |
| BASE PATCHING, ASPHALTIC | 30810 | sm | |
| BASE PATCHING, CONCRETE | 30820 | sm | \$40.95 |
| CRACKING AND SEATING CONCRETE PAVEMENT | 41040 | sm | |
| BREAKING AND SEATING CONCRETE PAVEMENT | | sm | |
| CONCRETE PAVEMENT REPAIR | 41574 | cm | \$183.00 |
| CONTINUOUS DIAMOND GRINDING | 41576 | sm | \$2.69 |
| RUBBLIZING CONCRETE PAVEMENT | | sm | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE A | 60123 | m | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE D | 60133 | m | |
| GEOTEXTILE FABRIC, TYPE DF | 64503 | sm | \$1.20 |
| PIPE UNDERDRAIN, 150 mm | 61201 | m | \$4.43 |
| PIPE UNDERDRAIN, UNPERFORATED, 150 mm | 61211 | m | \$22.15 |
| R.C. APRON ENDWALLS FOR UNDERDRAIN | 61254 | EACH | \$125.00 |
| REMOVING PAVEMENT | 20401 | sm | |
| GEO-GRID | '90xxx | sm | \$1.75 |
| ace unit | ~~~~ | | |
| | | | <u></u> |

ALTERNATE DESCRIPTION WORKSHEET

Version 3.3

01/06/97

8600–02–31 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| | | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |
|--|----------------|----------|-------------------|-------------------|--------|------------|-------|
| PARAMETER RUBAL OR URBAN PROJECT | UNITS R/U | VALUE | VALUE | VALUE | VALUE | VALUE | VALUE |
| ROADWAY WIDTH | R/U | 10.80 | 10.80 | 10.80 | | 10,80 | |
| PAVEMENT STRUCTURE WIDTH | m | 7 20 | | 7 20 | | 7.20 | |
| TOTAL PAVED SHOULDER WIDTH | m | 1.80 | | 1.80 | | 1.80 | |
| CONCRETE RDWY PAVEMENT THICKNESS | mm | 175 | | | | L | L |
| CONCRETE SHOULDER THICKNESS | mm | 175 | | | | | |
| AC RDWY PAVEMENT MIX TYPE | HV/MV/LV | | MV | MV | | MV | |
| TOTAL AC RDWY PAVEMENT THICKNESS | mm | | 100 | 115 | 125 | 125 | |
| VIRGIN AC RDWY PAVEMENT THICKNESS | % | | 100 6.0 | 115 6.0 | | 125 6.0 | |
| % OF ASPHALT CEMENT USED RECYCLED AC RDWY PAVEMENT THICKNESS | mm | | 6.0 | 0.0 | | 5.5 | |
| % OF ASPHALT CEMENT USED | % | | | | | | |
| % RAP | % | | | | | | |
| AC SHOULDER PAVEMENT MIX TYPE | HV/MV/LV | | MV | mv | | | |
| TOTAL AC SHOULDER PAVEMENT THICKNESS | mm | | <u>125</u> 125 | <u>115</u> 115 | | | |
| VIRGIN AC SHOULDER THICKNESS RECYCLED AC SHOULDER THICKNESS | mm mm | | 120 | 118 | | | |
| % OF ASPHALT CEMENT USED | % | | 6.0 | 6.0 | | | |
| ASPHALTIC CONCRETE PAVEMENT WT. | kg/sm/mm | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 |
| TACK COAT COVERAGE | L/sm | 0.113 | 0.113 | 0.113 | 0.113 | 0.113 | 0.113 |
| WHICH LAYER IS THE DRAINAGE LAYER? | 0-4 | 0.01 | 0.01 | 0.01 | 0 0 | 0 275 | 0 |
| CRUSHED AGG. BASE COURSE THICKNESS UNIT WT OF CABC | mm Mg/cm | 0.01 | 0.01 2.4 | 0.01 | 0 | 2/5 | |
| OPEN GRADED BASE COURSE #1 THICKNESS | mm | <u>7</u> | | 0 | 0 | 0 | |
| UNIT WT OF OGBC #1 | Mg/cm | | | | | | |
| OPEN GRADED BASE COURSE #2 THICKNESS | mm | | | 0 | 0 | 0 | |
| UNIT WT OF OGBC #2 | Mg/cm | | | | 0 | 0 | |
| BREAKER RUN THICKNESS UNIT WT OF BREAKER RUN | mm Mg/cm | | 0 | 0 | 0 | 0 | |
| ASPHALTIC STABILIZED B.C. THICKNESS | mm | | | | | | |
| % OF ASPHALTIC CEMENT USED | % | | | | | | |
| UNIT WT OF AC STABILIZED BASE COURSE | Mg/cm | | | | | | |
| P.C. STABILIZED BASE COURSE THICKNESS | mm | | | | | | |
| UNIT WT OF PCC STABILIZED BASE COURSE GRANULAR SUBBASE COURSE THICKNESS | Mg/cm mm | | 0 | 0 | 0 | 275 | |
| OTHER #1 (STRUCTURE WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| OTHER #2 (ROADWAY WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| EXISTING PAVEMENT WIDTH EXISTING PAVEMENT THICKNESS | m mm | | 6.70 | 6.70 | | | |
| % OF PROJECT LENGTH FOR CURB & GUTTER | % | | | | | | |
| TYPE OF CURB & GUTTER | A/D | | | | | | |
| % OF PROJECT LENGTH FOR GEOTEXTILE FABRIC | % | | | | | | |
| % OF PROJECT LENGTH FOR UNDERDRAINS | % | | | 50 | | 66 | |
| % OF PROJECT LENGTH FOR TACK COATING | % | | 66 | 50 | | 00 | |
| TOTAL m2 OF CRCP STEEL REINFORCEMENT %OF PROJECT LENGTH FOR MILL & RELAY AC PAV'T | <u>sm</u> % | | | | | | |
| %OF PROJECT PAV'T AREA FOR AC SURF PATCHING | % | | | | | | |
| %OF PROJECT LENGTH FOR PULVERIZING AC PAV'T | % | | | 100 | | | |
| MILLING DEPTH | mm | | 13 | | | | |
| %OF PROJECT LENGTH FOR SALV AC PAV'T MILLING | % | | 100 | | | | |
| %OF PROJECT LENGTH FOR SALV AC PAV'T %OF PROJECT LENGTH FOR DIAMOND GRINDING | % | | | | | | |
| % OF PROJECT LENGTH FOR PCC PAV'T REPAIR | % | | | | | | |
| #OF PAV'T TIES PER METER OF LONGIT. LENGTH | EACH | | | | | | |
| #DOWELS PER PATCH JOINT | EACH | | | | | | |
| AVG. LENGTH OF PCC PATCH %OF PROJECT LENGTH FOR CRACK & SEAT | <u>m</u> % | | | | | | |
| % OF PROJECT LENGTH FOR CRACK & SEAT | % | | | | | | |
| %OF PROJECT LENGTH FOR RUBBLIZING | % | | | | | | |
| TOTAL AREA FOR ASPHALTIC BASE PATCHING | sm | | | | | | |
| TOTAL AREA FOR CONCRETE BASE PATCHING | sm | | | | | | |
| TOTAL AREA FOR CONCRETE WIDENING | sm | | | | | | |
| TOTAL AREA FOR AC BASE COURSE WIDENING | sm sm | | | | | | |
| %OF PROJECT LENGTH FOR PAVEMENT REMOVAL | % % | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |

BASE LAYER: (FOR QUANTITY CALCULATIONS)

\$

ę

| X - NONE | E – AC STABILIZED | • | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |
|-----------------|-------------------|---------|-------|-------|-------|-------|-------|----------|
| A – CABC | F – PC STABILIZED | LAYER 1 | a | a | a | x | а | * |
| B – OGBC #1 | g – granular | LAYER 2 | X | X | | x | g | * |
| C – OGBC #2 | H – OTHER #1 | LAYER 3 | X | X | X | | X | X |
| D – BREAKER RUN | I – OTHER #2 | LAYER 4 | | X | X | | X | X |

ALTERNATE QUANTITIES AND COSTS

Version 3.3

01/06/97

8600-02-31 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

| | | ALTERNATI | /E #1 | ALTERNA Asphalt/surface mill | TE #2 | ALTERN/ Asphalt/Pulverize&Rela | |
|-------------------------------------|-------|-----------|--------------|---------------------------------|-------------|-----------------------------------|-------------------------|
| PARAMETER | UNITS | QUANTITY | COST | QUANTITY | COST | QUANTITY | COST |
| CONCRETE PAVEMENT (RDWY) | sm | 7,200.0 | \$129,600.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 1,800.0 | \$32,400.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 1.692.0 | \$31,725.00 | 1,945.8 | \$36,483.7 |
| VIRGIN AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 528.8 | \$9,914.06 | 486.5 | \$9,120.9 |
| RECYCLED AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALT CEMENT | Mg | 0.0 | \$0.00 | 133.2 | \$20,562.37 | 145.9 | \$22,520.6 |
| CRUSHED AGG. BASE COURSE | Ma | 1.050.3 | \$7.089.48 | 420.3 | \$2,836.88 | 624.0 | \$4,212.2 |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| OPEN GRADED BASE COURSE #2 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| GRANULAR SUBBASE COURSE | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CURB & GUTTER | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| TYPE DF GEOTEXTILE FABRIC | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| 150 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| 150mm PIPE UNDERDRAINS.UNPERFORATED | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| APRON ENDWALLS FOR UNDERDRAINS | EACH | 0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| TACK COATING | L | 0.0 | \$0.00 | 1,476.7 | \$428.24 | 1.017.0 | \$294.9 |
| MILL & RELAY AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | <u>\$294.9</u> \$0.0 |
| SALVAGED ASPHALTIC PAVEMENT.MILLING | Mg | 0.0 | \$0.00 | 204.7 | \$1.580.17 | 0.0 | \$0.0 |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC SURFACE PATCHING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| PULVERIZING AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 6.700.0 | \$5,762.0 |
| CONTINUOUS DIAMOND GRINDING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | <u>\$0.0</u> |
| CONCRETE PAVEMENT REPAIR | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| CRCP REINFORCEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| PAVEMENT TIES | EACH | 0 | \$0.00 | 0 | \$0.00 | | \$0.0 |
| DOWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.0 |
| CRACK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| BREAK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| RUBBLIZING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| ASPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| CONCRETE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.0 |
| ASPHALTIC BASE COURSE WIDENING | Mg | 0.0 | \$0.00 | | \$0.00 | | \$0.0 |
| CONCRETE BASE COURSE WIDENING | sm | 0.0 | \$0.00 | | \$0.00 | | \$0.0 |
| REMOVING PAVEMENT | sm | 0.0 | \$0.00 | | \$0.00 | | \$0.0 |
| Cost Adjustment-see comps | | | (\$528.00) | | \$0.00 | 1 | \$0.0 |
| OTHER BASE #1 | Mg | 0.0 | | 0.0 | | 0.0 | |
| OTHER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | |
| ALTERNATIVE TOTAL | | | \$168,561.48 | | \$67,078.72 | | \$77,900.5 |

| | | ALTERNAT Existing Structure | E#4 | ALTERNATI Asphalt/base/sand | E#5 | ALTERNAT | E#6 |
|--------------------------------------|-------|--------------------------------|--------|--------------------------------|-------------|----------|--------|
| PARAMETER | UNITS | QUANTITY | COST | QUANTITY | COST | QUANTITY | COST |
| CONCRETE PAVEMENT (RDWY) | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 2,115.0 | \$39,656.25 | 0.0 | \$0.00 |
| VIRGIN AC PAVEMENT (SHOULDERS) | Ma | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| RECYCLED AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 |
| ASPHALT CEMENT | Ma | 0.0 | \$0.00 | | \$19,583.21 | 0.0 | \$0.00 |
| CRUSHED AGG. BASE COURSE | Mg | 0.0 | \$0.00 | | . \$0.00 | 0.0 | \$0.00 |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 |
| OPEN GRADED BASE COURSE #2 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| GRANULAR SUBBASE COURSE | cm | 0.0 | \$0.00 | 4,152.5 | \$13,703.25 | 0.0 | \$0.00 |
| CURB & GUTTER | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| TYPE DF GEOTEXTILE FABRIC | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| 150 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| 150mm PIPE UNDERDRAINS, UNPERFORATED | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| APRON ENDWALLS FOR UNDERDRAINS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 |
| TACK COATING | L | 0.0 | \$0.00 | 1,610.9 | \$467.17 | 0.0 | \$0.00 |
| MILL & RELAY AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| ASPHALTIC SURFACE PATCHING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| PULVERIZING AC PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| CONTINUOUS DIAMOND GRINDING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| CONCRETE PAVEMENT REPAIR | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| PAVEMENT TIES | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 |
| DOWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 |
| CRACK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| BREAK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| RUBBLIZING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| ASPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETEWIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| ASPHALTIC BASE COURSE WIDENING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 |
| CONCRETE BASE COURSE WIDENING | sm | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 |
| REMOVING PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 |
| Cost Adjustment-see comps | | | | | | | |
| OTHER BASE #1 | Mg | 0.0 | | 0.0 | | 0.0 | |
| OTHER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | |
| ALTERNATIVE TOTAL | | | \$0.00 | | \$73,409.88 | | \$0.0 |

ALTERNATE MAINTENANCE Version 3.3

8600—02—31 Chippewa Falls — Comell Jim Falls — CTH R STH 178 Chippewa

MAINTENANCE COSTS: (CURRENT YEAR)

| | INCREM | MENT 1 | INCREM | ENT 2 | INCREME | ENT 3 | INCREME | INT 4 | INCREM | ENT 5 |
|--------------------------------------|---------------|------------|------------------|------------|------------------|------------|--------------------------------|------------|------------------|------------|
| ALTERNATE TITLE | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM | TO YEAR |
| PCC YEARLY CO | ST \$2,400.00 | 13 | 19 \$4,970.00 | 20 | 24 \$4,970.00 | 25 | 28 | 29 | | |
| Asphalt/surface mill YEARLY CO | 2 | 3 | 9 \$1,550.00 | 10 | 16 \$1,250.00 | 17 | \$4,570.00 22 \$1,550.00 | 23 | 28 | |
| Asphalt/Pulverize&Relay YEARLY CO | 2 | 9 | 9 | 10 | 16 \$1,260,00 | 17 | 22 | 23 | \$1,250.00 28 | |
| Existing Structure YEARLY CO | | | | | 31,200 00 | | \$1,550,00 | | \$1,250.00 | |
| Asphalt/base/sand YEARLY CO | | | | | | | | | | |
| YEARLY CO | 0 ST | | | | | | | | | |

01/06/97

MAINTENANCE: COSTS: (CURRENT YEAR)

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| · | INCREME | NT 6 | INCREM | ENT 7 | INCREM | ENT 8 | INCREM | MENT 9 | INCREM | ENT 10 |
|-------------------------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|--------------|------------|
| ALTERNATE TITLE | FROM YEAR | TO YEAR |
| PCC | 36 | 39 | 43 | 44 | 46 | 49 | | 10011 | | |
| YEARLY COST | \$4,970.00 | | \$1,250.00 | | \$1,550.00 | | | | | |
| Asphalt/surface mill | 34 | 35 | 40 | 41 | 47 | 48 | £ | | | |
| YEARLY COST | \$1,550.00 | | \$1,250.00 | | \$1.550.00 | | | | | |
| Asphalt/Pulverize&Relay | 34 | 35 | 40 | 41 | 47 | 48 | 3 | | | |
| YEARLY COST | \$1,550.00 | | \$1,250.00 | | \$1.550.00 | | | | | |
| Existing Structure | | | | | | | | | | |
| YEARLY COST | r i | | | | | | | | | |
| Asphalt/base/sand | | | | | | | | | | |
| YEARLY COST | I | | | | | | | | | |
| (| | | | | | | | | | |
| YEARLY COST | r l | | | | | | | | | |

ALTERNATE REHABILITATION Version 3.3

01/06/97

8600–02–31 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| SCHEME | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders | MILUNG DEPTH (mm) | % OF PROJECT for SURF. PATCHING | OVERLAY THICKNESS (mm) | MIX TYPE (HV,MV,LV) | % AC in OVERLAY MIX | OTHER COSTS | OTHER COST DESCRIPTION |
|--------|---|----------------------|---------------------------------------|---------------------------|------------------------|------------------------|----------------|---|
| AC1 | | 0 | 6.0 | 50 | FRE | 6.0 | \$570.0 | 0. cost adjustment program error~see comp sheets |
| AC2 | 2 | 13 | 0.0 | 50 | m | 6.0 | \$949.0 | 2 COST adjustment - program wron - see cross sheets |
| AC3 | | 50 | Q.Q | 50 | TTN- | 6.0 | 56-0 | 0 cost adjustment - program extersee comp sheets |
| AC4 | | | | | | | | |
| AC5 | | | | | | | | |
| AC6 | | | | | | | | |
| AC7 | | | | | | | | |
| ACB | | | | | | | | |

CONCRETE PAVEMENT REHABILITATION SCHEMES

| | | | | % OF PROJECT | 1 | | |
|----------------|--------------|------------------|--------------|-------------------|--------------------|-----------|---------------------------------|
| Repair – Grind | | AVG PATCH LENGTH | # DOWELS PER | for | | OTHER | |
| SCHEMES | % PCC REPAIR | in m | JOINT | PCC Base Patching | | COSTS | OTHER COST DESCRIPTION |
| PC1 | 0.0 | 1.8 | 52 | 0.0 | & Continuous Grind | | |
| PC2 | 0.0 | 18 | 32 | 1.0 | & Continuous Grind | \$5,959.9 | cost adjustment see comp ateens |
| PC3 | | | | | & Continuous Grind | | |

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| Repair – Overlay SCHEMES | % PCC REPAIR | AVG PATCH LENGTH | # DOWELS PER JOINT | % OF PROJECT for PCC Base Patching | % OF PROJECT for AC Base Patching | OVERLAY THICKNESS (mm) | MIX TYPE (HV.MV.LV) | % AC in OVERLAY MIX | OVERLAY LIMITS 1: RDWY ONLY 2: RDWY & Shoulders | OTHER | OTHER COST DESCRIPTION |
|-----------------------------|--------------|------------------|-----------------------|--|---|---------------------------|------------------------|------------------------|---|-----------|-------------------------------------|
| PC4 | DQ | | 32 | 1.0 | ĎŎ | ŚĊ | rpv. | | e | SS BOX OF | Fost additioned to the more encoded |
| PC5 | 0.0 | 0.0 | 9 | 0.0 | 0.0 | 50 | mv | 6.0 | 1 | | |
| PC6 | | | | | | | | | 1 | | |

| Mill – Repair – Overlay SCHEMES | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders | MILLING DEPTH (mm) | % PCC REPAIR | AVG PATCH LENGTH | # DOWELS PER JOINT | % OF PROJECT for PCC Base Patching | % OF PROJECT for AC Base Patching | OVERLAY | MIX TYPE (HV.MV.LV) | % AC in OVERLAY MIX | OTHER COSTS |
|------------------------------------|---|-----------------------|--------------|------------------|-----------------------|--|---|---------|------------------------|---|----------------|
| PC7 | t | 50 | GĐ | 6.0 | A | 0.0 | | | | | |
| PC8 | | | | | | | | | -FIG | 5.0 | |
| PC9 | | | | | | | | | | | |
| | | | | | | | •••••••• | | | 100000000000000000000000000000000000000 | |

PC7 OTHER COST DESCRIPTION PC8 OTHER COST DESCRIPTION PC9 OTHER COST DESCRIPTION

| | | OTHER | |
|--------|---|---|------------------------|
| SCHEME | | COSTS | OTHER COST DESCRIPTION |
| PC10 | CONTINUOUS DIAMOND GRIND ONLY | | |
| PC11 | RECONSTRUCT: USING ORIGINAL PCC LAYER THICKNESSES | *************************************** | |

ALTERNATE REHABILITATION SCENARIOS:

| REHABILITATION COSTS | ALT. #1: | PCC | | ALT. #2: | Asphalt/surface mill | | ALT. #3: | Asphalt/Pulverize&Rel | ау | ALT. #4: | Existing Structure | |
|--------------------------------------|----------|-------|-----------------|--------------------|----------------------|-----------------|-----------|-----------------------|---|----------|--------------------|-----------------|
| (COSTS ARE CURRENT YEAR) | SPACING | TYPE | CURRENT YR COST | SPACING | TYPE | CURRENT YR COST | SPACING | TYPE | CURRENT YR COST | SPACING | TYPE | CURRENT YR COST |
| FIRST REHABILITATION | | PC2 | \$27,375.40 | ····· | AC1 | \$31,942.66 | **** | 4 AC1 | restance in the second s | | | \$0.00 |
| SECOND REHABILITATION | | 0 PC4 | \$39,925.06 | ****************** | AC2 | \$34,065,19 | | 2 AC2 | \$34.065.10 | | | \$0.00 |
| THIRD REHABILITATION | | | \$39 925 06 | | 1 473 | \$34.065.10 | | | \$04,000.19 | | | \$0.00 |
| FOURTH REHABILITATION | | 0 PC4 | \$0.00 | | AC2 | \$34,003.19 | | 2 AC2 | \$34,065.19 | | | \$0.00 |
| | | | | | | φυ.υυ | | | \$0.00 | | | \$0.00 |
| EXPECTED LIFE OF LAST REHABILITATION | | 0 | \$0.00 | | | \$0.00 | | | \$0.00 | | | \$0.00 |
| | | 0. | | <u>t</u> | 24 | | <u></u> t | 2 | | | 8 | |
| TOTAL LIFE | L | 50 | | 50 | บ | | 5 | 0 | | | 0 | |

ALTERNATE REHABILITATION

ALTERNATE REHABILITATION SCENARIOS

| REHABILITATION COSTS | ALT. #5: | Asphalt/base/sand | | ALT. #6; | 0 | |
|--------------------------------------|--|-------------------|-----------------|----------|------|-----------------|
| (COSTS ARE CURRENT YEAR) | SPACING | TYPE | CURRENT YR COST | SPACING | TYPE | CURRENT YR COST |
| FIRST REHABILITATION | | | \$0.00 | | | \$0.00 |
| | | | | | | \$0.00 |
| THIRD REHABILITATION | I ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | | ¢0.00 | | | \$0.00 |
| FOURTH REHABILITATION | | | \$0.00 | | | · \$0.00 |
| FIFTH REHABILITATION | | | \$0.00 | | | ** |
| EXPECTED LIFE OF LAST REHABILITATION | | | | | | 40.00 |
| TOTAL LIFE | 0 | | | 0 | · | |

× ,

LIFE CYCLE COST ANALYSIS

Version 3.3

01/06/97

8600–02–31 Chippewa Falls – Cornell Jim Falls – CTH R STH 178 Chippewa

| CURRENT YEAR CONSTRUCTION YEAR DESIGN YEAR ANALYSIS PERIOD | 1994 2002 2022 50.0 | DISCOUNT RATE (%) PROJECT LENGTH (Km) ANALYSIS BASIS (P/M) | | 5.0 1.00 M | | |
|---|------------------------------|--|--------|------------------|-------|--------|
| | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
| TERMINAL SALVAGE VALUE | | | | | | |

PRESENT WORTH COSTS: (CURRENT YEAR)

| | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
|------------------------------|--------------|----------------------|--------------------|--------------------|-------------------|--------|
| | PCC | Asphalt/surface mill | Asphalt/Pulverizeℜ | Existing Structure | Asphalt/base/sand | 0 |
| INITIAL CONSTRUCTION COSTS | \$114,089.04 | \$45,401.52 | \$52,726.18 | \$0.00 | \$49,686.69 | \$0.00 |
| REHABILITATION COSTS | \$17,074.25 | \$21,014.86 | \$21,014.86 | \$0.00 | \$0.00 | |
| MAINTENANCE COSTS | \$5,508.70 | \$2,831.48 | \$2,831.48 | \$0.00 | \$0.00 | |
| TERMINAL SALVAGE VALE | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| REHABILITATION SALVAGE VALUE | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | |
| | | | | | | |
| TOTAL FACILITY COSTS | \$136,671.99 | \$69,247.86 | \$76,572.52 | \$0.00 | \$49,686.69 | \$0.00 |

EQUIVALENT UNIFORM ANNUAL COSTS: (OVER ANALYSIS PERIOD)

| | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
|------------------------------|------------|----------------------|--------------------|--------------------|-------------------|--------|
| | PCC | Asphalt/surface mill | Asphalt/Pulverizeℜ | Existing Structure | Asphalt/base/sand | 0 |
| INITIAL CONSTRUCTION COSTS | \$6,249.43 | \$2,486.95 | \$2,888.17 | \$0.00 | \$2,721.67 | \$0.00 |
| REHABILITATION COSTS | \$935.27 | \$1,151.13 | \$1,151.13 | \$0.00 | \$0.00 | \$0.00 |
| MAINTENANCE COSTS | \$301.75 | \$155.10 | \$155.10 | \$0.00 | \$0.00 | \$0.00 |
| TERMINAL SALVAGE VALE | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 |
| REHABILITATION SALVAGE VALUE | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 | \$0.00 |
| | | | | | | |
| TOTAL FACILITY COSTS | \$7,486.45 | \$3,793.17 | \$4,194.39 | \$0.00 | \$2,721.67 | \$0.00 |

State of Wisconsin

Date: 1 July 1996

To:

From: Lary A. Hyland, P.E. District Soils Engineer

File

Subject: SOILS ENGINEERING COST ESTIMATE Project 8600-02-01 CTH "Y" to CTH "R" STH 178 Chippewa County

Because of the somewhat unusual nature of the project (winding along the river, rock, marsh pockets etc.) it is particularly difficult to tie cost down this early. Based on guidance that we've been given by CO and our own experience, however, my best estimate would be \$20,000. This is about 10% of the design-engineering costs. We may well need marsh borings and lab. work and rock borings/seismograph work in addition to other, more common, borings and soil analysis. Much depends on the amount of substantial relocation required. This would not include structure borings - bridges, culverts, retaining walls - which I assume that we would not have a handle on at this point.

June 28, 1996 Date:

To: file

From: Randy W. Luedtke, P.E.

Subject:

PROJECT -8600-02-01 Chippewa Falls-Cornell CTH Y-CTH R STH 178 Chippewa County



PROJECTED BUDGET COSTS

Total Project Cost: \$3,200,000

Total Project Engineering Cost(6%) : \$192000

Projected Pavement Item Cost(pavement,base,sub-base,etc.) Initial construction : \$1,950,000

% engineering cost applied to Pavements: 1,950,000 @ 6% = 117,000

| District Pavement design | Assume that 20% of pavement cost er from the Materials Section \$117000 | ngineering total i *20%=\$23400 | s charged |
|----------------------------|--|------------------------------------|---|
| | COSTS Pavements charged to "79" Function C (includes charges to "741", "742", & " constructability reviews, P.S.&E comp | 748", | etc.) |
| | salary charges | \$ 8,400 | LARY, AMOUNT |
| ι. | Consultant pavement borings & cores | \$15,000 | LARY, I LIST THIS AMOUNT, BUT SINCE THIS PROJECT IS RELOCATION PROJECT IS WINAT |
| | TOTAL | \$23,400 | WITH REFY |
| Assume that design "19" fu | unction code uses other 80%\$93600 | | THIS TOTAL IS A SAFETY NET. RANGY |

Assume that design "19" function code uses other 80%--\$93600

This breakdown of costs leaves \$ 93600 for other overlapping design pavement related charges such as typicals, quantities, specials, estimates, etc. separate from the "79" function code.

STH 178 7.3 miles = 11.7 Km 1500 vehicles assume SN = 3.5 English cost/km Metric 5" ASPHALT = 2,2 10" BASE 1.0 10" sand .35 MV MIX 2650 TUNE \$20= 53000 3.55 MAT'L 159 TON @ 160=25440 TACK = 600 BASE 8400 TON C 7,00 = 58800 SAND 4000 m³C4,50 = 18,000 155840 km 1,823,328 plus Side Roads = 1,95 million 1,950,000 @ 6% = \$117,000 TOTAL \$117,000 = \$23,400 168 168 HRS FOR ME Consultant pavement boring à corres 15,000 + 8400

| State of Wisconsir | ı |
|--------------------|---|
|--------------------|---|

| Date: | June 24, 1998 |
|----------|---|
| To: | File |
| From: | Randy W. Luedtke, P.E. District#6 Pavement Design Engineer |
| Subject: | Pavement Documentation Project I.D. 8600-03-31 or 01 Chippewa - Cornell Road CTH I - CTH Y STH 178 Chippewa County |

This project was initially scoped or programmed as a Rut Fill type project. Since that time, after in-house discussion and coordination with county officials, it was agreed that a thin overlay is a better choice. Due to the existing rutting a lower leveling course will need to be placed to fill in the ruts before a surface layer is placed. The contractor *should not* be allowed to place the total plan asphalt thickness in one lift.

At this point in time this pavement treatment is considered as a roadway maintenance type project. No formal documentation of the pavement selection or LCCA is required beyond what is stated in the Design Study Report.

The following typical should be done:

- A. A lower level should be initially placed to fill in the ruts(pavement distortion) in the wheel paths. It should be stated as a variable depth layer ranging from ³/₄" to 1". This note may cause a red flag but it can be achieved with a grade #3 surface mix.
- B. The upper layer or surface pass should be constructed of $1 \frac{1}{4} 1 \frac{1}{2}$ ". If the programming designation or RDMNT threshold of $2 \frac{1}{2}$ " is waived the surface lift should be increased to 2 inches.
- C. Designate the mix as MV grade #3(surface mix) for both layers.

It is assumed that this treatment will provide an additional 8-10 years of service versus 3-5 years for the typical rut fill.

There is a possibility that some areas may be excavated to alleviate frost heave areas. A typical depth of 5" asphalt over 12" of base course should be used for those areas. The surface thickness should match the adjacent segments.

Reviewed:

Approved:

Michael S. Ostrowski, P.E. PD Manager

LAST -> RWL <u>8/10</u> MSO <u>8/4</u> Sin Koening <u>8/2</u>

Richard J. Shermo, P.E. PD Area Supervisor

| Date: | 03/30/93 | | |
|----------|-----------------------------|--------|--------|
| From: | Norm Ewert | EWERTN | - HFRC |
| To: | Lary Hyland | HYLANL | - HFRC |
| | Richard Gosnell | GOSNER | - HFRC |
| | George McLeod | MCLEOG | - HFRC |
| | Bruce Eastenson | EASTEB | - HFRC |
| | Richard Pauser | PAUSER | - HFRC |
| Subject: | STH 178 - CTH 'Y' to STH 64 | | |
| | | | |

Reference: Your note of 03/26/93 15:16 attached below

I have not problem with this. Lets get the plans to show what Lary recommends. If the PS&E is already submitted, I would assume the short short section of deeper milling can be done in the field without a C.O.

Pauser, I would like you to call Bruce Stelzner and tell him what we will be doing and why.

Dick G, has the PS&E been submitted ?

----- ATTACHED NOTE -----

| Date: | 03/26/93 | | |
|----------|-----------------------------|--------|--------|
| From: | LARY HYLAND | HYLANL | - HFRC |
| To: | Richard Gosnell | GOSNER | - HFRC |
| | Norman Ewert | EWERTN | - HFRC |
| cc: | George McLeod | MCLEOG | - HFRC |
| | Bruce Eastenson | EASTEB | - HFRC |
| | Richard Pauser | PAUSER | - HFRC |
| Subject: | STH 178 - CTH 'Y' to STH 64 | | |

Some thoughts on the subject project - mostly based on recent events - to be sure we are all of the same thinking/impression/intention:

1. The overall project concept that prevailed in our pavement design interaction was that we should stay with the Maintenance Resurfacing intention. That, as Bruce put it, "We are preserving a nice, 45 MPH highway - that will continue to require maintenance".

2. We all agree, I think, that total recontruction, with a raised roadway and/or good ditches are the ultimate solution to a good job here, as with any road. However, this is, apparently, not cost effective in this case.

3. Our nominal 1 1/2-inch mill with a 2-inch overlay should go a fair way in true-ing thins up.

The overlay will provide a good riding surface for a time but, it is recognized that it will need continued manintenance in a number of areas.

4. We recently looked at a five areas that Design (Dick Pauser) had quetioned us on and, that Maintenance and the County had also evaluated

based on maintenance history. In the final analysis, we decided that in most of those areas the solution to the problem was not worth the expenditure. I.e. continued maintenance was more cost-effective than the total repair effort. There was one exception: an area of several hundred feet, where we recommended that we full-depth mill (3 1/2 inches) and put 4 inches back, if we can fit it in.

5. I suspect that we will receive some critism, particularly from the County because of the continued maitenance but, I certainly don't disagree that this is the way to go with this section of highway.

| Date: | 02/10/93 | | | |
|------------|--|------------|---|------|
| From: | Norm Ewert | EWERTN | - | HFRC |
| To: | Richard Pauser | PAUSER | - | HFRC |
| | Bruce Eastenson | EASTEB | - | HFRC |
| | Marlin Beekman | BEEKMM | - | HFRC |
| Subject: | STH 178 Maintenance Resurface | | | |
| Reference: | Your note of 02/06/93 13:43 attached below | | | |

I don't think we should get into an expensive pavement structure, unless we could get wider shoulders and safety improvements. I don't think we are ready this time around, to talk about widening shoulders by grading ditches etc. So its my opinion we need to keep the improvement this time, to a 'cheap maint' type. The next time around we may need to do a scenic road improvement type of project. I think we should put in the minimum beam guard as you suggest.

I have no problem with coming up with a method of taking care of the four areas of severe longitudinal cracking.

It would be nice if we had some sections to see what shoulder width we can accomplish without grading. It was my hope that we could get a 22-foot pavement with 2 or 3 foot paved shoulders.

Lets meet with Bruce, Marty and Lary and discuss the project. Please set up a meeting for this job and Medford. I am available tomorrow, Thur am or before the 2:00 programming meeting, Fri at 2:30, or anytime Monday the 15th.

| Date: | 02/06/93 | | |
|----------|-------------------------------|--------|--------|
| From: | Richard Pauser | PAUSER | - HFRC |
| To: | Norman Ewert | EWERTN | - HFRC |
| | Michael Lenroot | LENROM | - HFRC |
| Subject: | STH 178 Maintenance Resurface | | |

Mohamd and I met with Bruce Stelzner and someone from the Sheriff's Dept. According to the Sheriff, Hwy 178 has the least problem with accidents in Chippewa County. We reviewed the accident record with him and the conclusion was that none were the fault of the highway in regard to curvature or sight distance. Low shoulders were probably a factor if any.

We then drove the route and four areas along the outside of curves next to the Chippewa River were suggested as needing beam guard if we can install it. Mohamed will have to take some hand level x-sections to find out what it will take. It would appear that a small amount of fill will be required at two of th e locations and at the other two locations it appears that the shoulder would be wide enough.

This was the first time that I really observed the shoulders. They appear wide enough to have 3 ft. of paving. However, they slope away so much including along the outside of curves it appears that we will need to do considerable work to bring them up so we can pave. If we do that, then we are also affecting the inslopes and subsequently the ditches. There are also four areas with lengthy longitudinal cracks where the roadway is sloughing out. Bruce has overlaid these areas to bring them back up. It would seem that if we are going to spend \$ 700,000 to have a decent pavement for the next 10 to 15 years that we should do something with these areas. Bruce suggested undercutting and and placing geo-grid. The question is, how far do we want to go with this project? Just from field observation it would seem that a deep mill and relay as salvaged asphalt base might be worthy of consideration. The roadway could be reshaped and it would take care of the shoulder work at the same time. There could be as much as a foot of black already in place which would give us a problem with a deep mill.

Any comments on this?

| Date: | 03/26/93 | | |
|----------|-----------------------------|--------|--------|
| From: | LARY HYLAND | HYLANL | - HFRC |
| To: | Richard Gosnell | GOSNER | - HFRC |
| | Norman Ewert | EWERTN | - HFRC |
| cc: | George McLeod | MCLEOG | - HFRC |
| | Bruce Eastenson | EASTEB | - HFRC |
| | Richard Pauser | PAUSER | - HFRC |
| Subject: | STH 178 - CTH 'Y' to STH 64 | | |

Some thoughts on the subject project - mostly based on recent events - to be sure we are all of the same thinking/impression/intention:

1. The overall project concept that prevailed in our pavement design interaction was that we should stay with the Maintenance Resurfacing intention. That, as Bruce put it, "We are preserving a nice, 45 MPH highway - that will continue to require maintenance".

2. We all agree, I think, that total recontruction, with a raised roadway and/or good ditches are the ultimate solution to a good job here, as with any road. However, this is, apparently, not cost effective in this case.

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The overlay will provide a good riding surface for a time but, it is recognized that it will need continued manintenance in a number of areas.

4. We recently looked at a five areas that Design (Dick Pauser) had quetioned us on and, that Maintenance and the County had also evaluated based on maintenance history. In the final analysis, we decided that in most of those areas the solution to the problem was not worth the expenditure. I.e. continued maintenance was more cost-effective than the total repair effort. There was one exception: an area of several hundred feet, where we recommended that we full-depth mill (3 1/2 inches) and put 4 inches back, if we can fit it in.

5. I suspect that we will receive some critism, particularly from the County because of the continued maitenance but, I certainly don't disagree that this is the way to go with this section of highway.

(AD-75)

CORRESPONDENCE/MEMORANDUM-

STATE OF WISCONSIN

| Date: | | File Ref: |
|----------|---|-----------|
| То: | July 7, 1992 | |
| | File | |
| From: | Lary A. Hyland, P.E. District Soils Engineer By: Jeffrey L. Glass | |
| Subject: | Pavement Design Memo Project 8600-02-31 Chippewa Falls - Cornell Road (N. Int. CTH Y - STH 64) STH 178 Chippewa County | • |

The following is recommended for this 10.49 mile project of STH 178:

Mill a nominal 1/2" along entire project length and overlay with 2" of AC. The compromise shoulder thickness for the 12th foot should be 3 1/2" AC, which will cover 25% of the 18kip wheeloads.

Because of the narrow shoulders on this highway and being close to the Chippewa River it is recommended to pave the shoulders as wide as possible, which will mean 2 ft in some areas and 3 ft or more in others, along with marking the lane widths at 11 feet, leaving more shoulder width.

The recommended milling depth is based on the overall condition of the pavement. There is rutting in most places, no measurement of depth has been taken.

12 -Wie

Traffic requires Type C asphalt mix for this project.

Lary I Dick G 4/28/92 ON our trip to Cornell Jin Whaten & Norm Ewert agreed to the following on the STH 178 MHRes. project. (1) Pave the shoulders (3'if possible, although it appears 2' may be as much as you can get in certain situations). Should be checked in the field. (2) May want to paint the lanes at 22', f only z' of the shoulders can be paved. (W. 11 give room to the b, Kers). Allem

CONCEPT DEFINITION REPORT

| Date:March 27, 1992 To: J. W. Dresser From: District Six (| (6) |
|--|---|
| | EGEIVE NR 3 1992 C.O.DEC |
| LOCATION: See Title Above II. A. Roadway Conditions: - Pavement: Type: Asphaltic Width: 22 Ft. Year: 1975 PSI: 2.60 PDI: 46 | Dist. 6 Rec'd |
| Shoulder: Type: GravelWidth: 2 Ft.Accident Rate: 343Year: 1990 | APR 3 1992 |
| Substandard Alignment: Horizontal: No Vertical: No B. Structure: No structure work is anticipated at this time. Type: Deck Girder - Steel Bridge Number: B-09-0682 Year Constructed: 1942 | D.D. CON. MNT. |
| Clear roadway width: 27.6 Ft. SR: 81.6 RS: 89.4 JUSTIFICATION: Longitudinal cracking and rutting maybe contributed to driving hazard. | ADM. DES. PLN. |
| III. PROPOSED IMPROVEMENT: Mill to shape and overlay with asphaltic pavement This roadway is located close to the Chippewa River and environmental constraints would preclude widening the roadway. Also this is a maintain only roadway. | MAT'L FILE |
| A. Environmental documentation type: Programmatic Type IIIB B. Improvement Type: RDMTN PMSID: 92-060-020-201 C. Cost: \$700,000 Program Year: 1994 Program: 3332 D. Local Participation: No Access Control: No | |
| Project Supervisor: Richard J. Pauser, P.E. Accepted By: Recommend Acceptance: Mark R. Ploederer, P.E. Date: 4-1-92 | |

cc: OEA, CWC, Drith, JW

Concept Definition Report Project 8600-02-31 Page 1 of 2 Date 03/27/92



W

| PLENULE PAV | EMENT STRUCTURE D | ESIUN | |
|-------------|-------------------|---------|-------|
| ED401 M7 | | | |
| Project ID | Federal Project | Highway | Count |

| Project ID | Federal Project | Highway | County | | Data | · · . |
|-------------------------------------|-------------------------------|-------------------------|--------|-------------------------|----------|---|
| 2600-02-31 | | StH 178 | l chi | PPewa | 7- | $\mathcal{J} = \mathcal{I} = \mathcal{I}$ |
| Project Name | | | | | District | |
| CTHY-S | TH 64 | 574178 | | | 6 | |
| TRAFFIC | | | Traffi | ic Analysis Period:_ | 20 | Years |
| Construction Year/ADT | Design Year/ADT | Directional Factor (DF) | Lane (| Distribution Factor (LI | DF) | |
| 1675 | 2275 | 0.5 | | | | |
| Design Lane Traffic (DLT) = (Consti | , Year ADT + Design Year ADT) | X DF X LDF | | | | |
| (| 2 2275) X | 0.5 | × | / | - 6 | 88 |
| | | | | | | |

LOADING (Use charts "18 Kip Loads for Flexible Pavements" or "18 Kip Loads for County Trunk Highways")

| Truck Type | Truck Class. % of ADT | | DLT | No. of T | rucks | | 18K Lõads |
|------------|-----------------------|--------|------------|----------------|------------|------------|-----------|
| 2D | 3.68 | × | | • | (0.3). | • |)/ |
| 3-SU | 1:38 | × | | H | (0.8) | • |)D |
| 28-1, 28-2 | 0.88 | x | 988 | . | (0,5) | u | 4 |
| 35-2 | 2.0% | × | | H | (0.9). | • : | 8 |
| DBL BTM | <u>D</u> | x | | <u>ـــــ</u> د | | • <u> </u> | |
| | | Design | Lane Total | 18× Load | is per Day | <u></u> | 43 |

DESIGN $-\overline{SN}$ (Use Flexible Pavement Design Charts for Pt = 2.5 or 2.0)

| Serviceability Index | Design Group Index | Frost Index | Soil Support Value | ก |
|---------------------------------------|--------------------|------------------|---------------------|------|
| 2.5 | 14 | F-3 | 3.95 | 3.4 |
| ALTERNATE DESIGNS - SN | Exi | Sting | Straight overlo | ر لر |
| · · · · · · · · · · · · · · · · · · · | , | (1) | (+2-) 1 | |
| Bituminous Concrete | | X 0.44 = | 1.2 " × 0.44 = 0.66 | |
| Existing AC . | -4 -2 | x 0==0 =16 | 4/2 " x 0.35 1.6 | |
| Bituminous Base Course (Hot Mi | ×) | X 0.34 = | '' X 0.34 = | |
| Bituminous Stabilized Base | | X* | '' X= | |
| P.C. Stabilized Base | " | × = | " × | |
| Gravel or Crushed Stone Base | | o. /D × 0≩4 = | × 0,+41.1 | _ |
| Granular or Subbase | •'' | X = | " X= | |
| | | ו | " X= | |
| | | sn = <u>3.1</u> | sn = | 6 |

(Show other alternates on attached sheet)

Recommended Alternate

PLEMILLE PRAEMENT STRUCTURE DESIGN ED401 #47

SN.

| Project ID | Federal Project | Highway | County , | Data . |
|--------------|-----------------|---------|-----------|----------|
| 8600-02-31 | | StH 178 | ChiPPe wa | 7-2-42 |
| Project Name | | | | District |
| | | | | |

| TRAFFIC | | Traffic Analysis Period: Years | | | |
|-----------------------------|---------------|-----------------------------------|-------------------------|--------------------------|-------|
| Construction Year/ADT | Design | Year/ADT | Directional Factor (DF) | Lane Distribution Factor | (LDF) |
| Design Lane Trailic (DLT) = | (Constr. Year | ADT + Design Year AC | DT) X OF X LOF | , , | |
| | + | | , | V | _ |
| (| 2 | , , , , , , , , , , , , , , , , , | ` | ~ | - |

LOADING (Use charts "18 Kip Loads for Flexible Pavements" or "18 Kip Loads for County Trunk Highways")

| Truck Type | Truck Class. % of ADT | | DLT | No. of Trucks | 18 ^K Loads |
|------------|-----------------------|----------|-------------|-------------------------------|-------------------------|
| 2D | | _ × | | = | • |
| 3-SU | | _ × | | • | |
| 2S-1, 2S-2 | | _ × | 988 | £ | ······ |
| 3S-2 | | _ × | | a | ···· • · ····· |
| DBL BTM | | _ x | | a | |
| | | Design L | ane Total I | 18 ^k Loads per Day | <u>43x258=11</u> 2.> |

| Design | Lane | 10(a) | 10 | L0803 | per | Day |
|--------|------|-------|----|-------|-----|-----|
| | | | | | | |

DESIGN - SN (Use Flexible Pavement Design Charts for Pt = 2.5 or 2.0) Serviceability Index Design Group Index Frost Index

| Serviceability Index | Design Group Index | Frost Index | Soll Support Value | รัก |
|--------------------------------------|--------------------|----------------------|------------------------|----------------------------------|
| 2.5 | 14 | F-3 | 3.95 | 3.4 |
| ALTERNATE DESIGNS - SN | Surface M | ill + overlag | Compromise Show | ilder design |
| | | | <u>Compromise</u> Shou | |
| Bituminous Concrete | <u> </u> | < 0.44 = <u>0,88</u> | <u>' × 0.44 =</u> | 5 |
| Existing AC . Bighninous Road-Mix | / > | 0.35 1.4 | '' X 0.20 = | |
| Bituminous Base Course (Hot Mi | ×)" > | < 0.34 ■ | '' X 0.34 = | |
| Bituminous Stabilized Base | ·· > | <= | " ×∍ | |
| P.C. Stabilized Base | " > | < = | '' ×= | |
| Gravel or Crushed Stone Base | <u> </u> | 0,10 (0,14 = | X × 0.10 | 15 |
| Granular or Subbase | •" > | = | '' X= | |
| | " × | < * | " X= | |
| | | sn = <u>3.38</u> | SN | 2.65 LOVELS 258 18Kitwheeload |

(Show other alternates on attached sheet)

Recommended Alternate

FACILITIES DEVELOPMENT MANUAL



Date: 05/04/92 From: LARY HYLAND To: Richard Gosnell Subject: Proj. 8600-07-00, STH 178 Reference: Note attached below

HYLANL - HFRC GOSNER - HFRC

The Proj. No. should have been 8600-02-61. Sorry!

----- ATTACHED NOTE -----

Date: 05/01/92 From: LARY HYLAND To: Richard Gosnell Subject: Proj. 8600-07-00, STH 178

HYLANL - HFRC GOSNER - HFRC

I got up there today to look. Here's the way I see it:

1. There are stretches that definitely need milling before paving. (In fact if this weren't a Maintain Only road I'd say protions should be rebuilt). Other portions could be milled as a first choice but we could easily live without. Still other sections don't need milling at all. This is an unusually variable piece of road - I suppose, because of the maintenence-only approach.

2. The need to mill, however, could be rethought if your survey indicates crown problems.



.

Misc.

,

| То | | | Date | Time | |
|---|--|----------|------------------------|---------------------------------------|--|
| From | | | L | Please Call Returning Ca | |
| Phone | | Taken By | | | |
| CommentRoute | For Your Inf.Approve/Sign | | pare Reply e Action | ReturnFile | |
| #1 | 1.46 | Wort | 40 | f y | |
| #2 | 3.29 | | | | |
| #3 | 5.18 | | | | |
| <i>#4</i> | 6.55. | | | | |
| HS | 9.66 | | | | |
| | | | | | |

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| Date Need | Time Need | RoughFinal | Doub Single | | Document |


#2 A/B/S \$ #3 0 2-3 4 9-10 l'surface Mill 3'à "overlay 14 + 17-18 - 22-23 26 · 2'surface mill 4' overlay 28-29 34-35 AC9 - RE-DO 38 40-41 52

existing Structure 5" Asphalt 5" BASE Mż Relay 6" $6'' \times .25 = 1.25$ $5'' \times .10 = 0.70$ 1.75Target X5 3.4 4,2" " 4

MiRelay 4" Mat cost/mile 4000 * 25/00 = 109 100 \$ 15,000 MER 115,000 35 Imise * SBG, RASE 155,000 mile 2 MILLION 11/2" not raise mill out 2" SURFACE MILL 2000 TON/MILE 2 PASS Mat L_AR15,000 \$³¹2" 3500 * 25 = 87,500 102,500 perpare minimum Misa 20% = \$Zerovo 14125,000 I pass (Imillion / 1.4 MILL





C-PNDSS 178-(+9, Y - CORMENT

USE THIS FOR LAVER & BASE INFO ONLY

PDI ? PSI INFO OUTDATED

| | tion ID: 6-09-178-30 P_FLS-CORNELL/JIM_FAL | | | | ength: 1 | | | . Typ)0 P | | | | ĉ | |
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| | sible treatments | 2.0 | | /歌1. | 9 | | | | | | | | |
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| 50% | mana j | 3000 |) | đ. | -prob∕ta∣ | t d | efs | Whic | h?(+ | 5 - F | c,s | (b,p) | 4 5 |
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| <u>10</u> | reconstruct | 100.0 | ţ | | | | | | | | | | |
| | | | t 1 | | | | | | | | | | |
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SEGNENT HISTORY SCREEN SegID:13240 No. 1 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIM_FALLS-STH_64

| Last 12 | yrs surface history | Cross-Section(up to | 10 layers) | |
|---------|---------------------|---------------------------------|-------------|---------------|
| Vr trt | at PSI(s) PDI(s) | Layrt Yr. Type | Thick. | Prev.Lyr.Tat. |
| 89 | | 1 81 SglAgg | 01.5" | |
| 88 | | 2 63 Sglågg | 01.5^{v} | West |
| 87 | 7.4 | 3 50 SqlAqq | 01.5" | sur- |
| 60 | 43 | - <u>11</u> | | |
| 03 | 2.5 | 5 | | |
| 84 | | in Maria Santa | | |
| 83 | 1.0 | 7 | | |
| 82 | | | | |
| 81 | 2.2 | | | |
| 80 | | 10 | | |
| 29 | | Base: 11 [#] crushed g | ravel no si | tab. |
| 28 | | Sub Base: no subb | ase recorde | ed no stab. |
| | 7 | Culle consultate ener | | |

--Widths---LS PVMT RS 2 22 2 +/-= next/prev. segment in this section (this is #1 of 11) Roadway: 28 see the deficiency Section again c= Choose another section Enter your choice (d,+/-,s,c):

SEGMENT HISTORY SCREEN

SegID:13250 No. 2 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIM_FALLS-STH_64

| Last 12 yrs surface | history | Cross-Section(up to | 10 layers) |
|---------------------|----------------|-----------------------|-------------------------|
| Vr trtat P51(s |) PDI(s) | Layr# Yr. Type | Thick, Prev.Lyr.Tet. |
| 89 | | 1 81 Sglágg | 01.5" - |
| 88 | | 2 63 SqlAgq | Q L C K |
| 87 2.6 | | 3 50 Sglágg | 01. <u>5</u> * ~ |
| 84 | 80 | 1 <u>1</u> | |
| 85 1.9 | | 2. 1 | |
| <u> 2</u> | | 6 | |
| 83 l.6 | | 7 | |
| 82 | | | |
| 81 1.9 | | 7 | |
| 80 | | | |
| 79 | | Base: 11° crushed gr | avel no stab. |
| 78 | | Sub Base: no subba | se recorded no stab. |
| | | Soil: poor draining | |
| Widths | | Struct Num (with soi | 1, w/o PCC)= 6.85 |
| LS PVMT RS | d=change displ | ay mode to decisions | |
| 2 22 2 | +/-= next/prev | . sequent in this sec | tion (this is #2 of 11) |
| Roadway: 28 | s= see the def | iciency Section again | |
| | c= Choose anot | her section | |
| | Enter | your choice (d,+/~,s | |

SEGMENT HISTORY SCREEN

SegID:13260 No. 3 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIM_FALLS-STH_64

| Last 12 yrs | surface | history | Gross | -Sect | ion(up to | 10 layers) | 5 3 S |
|-------------|---------|-----------------|-----------|-----------------------|------------|------------|--|
| Yr trtmt | PS1(s |) PDI(s) | Layr# | Yr. | Type | Thick. | Prev.Lyr.Tat. |
| 89 | | | See 5 | 84 | SglAgg | 01,5" | 500 × |
| 22 | | | 2 | 63 | SglAgg | 01.5" | |
| 87 | 1.5 | | 3 | 50 | SqlAqq | 01.5° | -1400 |
| 28 | | 98 | the state | | | | |
| 85 | 1.6 | | ç | | | | |
| 84 | | | Ĺ | | | | |
| 83 | 2.0 | | 7 | | | | |
| 82 | | | 8 | | | | |
| 01 | 2.2 | | 9 | | | | |
| 80 | | | 10 | | | | |
| 79 | | | | | crushed gr | avel no st | ah. |
| 70 | | | | | na subba | | |
| | | | | | l draining | | and the second sec |
| Widths | | | | | with soi | | 1= 7.15 |
| LS PVMT RS | | d=change displ | | | | | · · · · · · · · · · · · · · · · · · · |
| | | +/-= next/prev | | | | tinn (this | is #3 of (1) |
| | | s= see the def | | | | | (de vet ét les he⊊is ∆raj t |
| | | c= Choose anot | | | | | |
| | | | | | e (d,+/-,s | , e 1 e | |
| | | Sec. 1 Sector 1 | 1.00.003 | પ્રયુપ્ત કે આવે છે. આ | ~ >43.5 84 | 1-22 | |

SEGHENT HISTORY SCREEN

SegI0:13270 No. 4 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIM_FALLS-STH_64

| L a | ist 12 yrs | surface | history | Cross- | Sec | tion(up t | o 10 layers) | 8 S K | |
|------|------------|---------|---|--|--------|-----------|--------------|---------------------------------------|--|
| Yr | | PSI(s) | PBI(s) | Layr# | V in s | Type | Thick. | Frev.Lyr.Tst. | |
| 89 | } | | | 4 1 1 | 84 | Sglågg | | -100 | |
| 86 | | | | 174 | 43 | Sglågg | 01.5" | | |
| 87 | | 2.3 | | | | SglAgg | 01.5° | e e e e e e e e e e e e e e e e e e e | |
| PR 2 | | | a de la companya de l | 1993 - S. 1995 - | | | | | |

60 1.2 62 84 b 83 1.5 7 82 8 81 2.0 9 80 10 79 Base: 11° crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths---Struct Num (with soil, w/o PCC)= 7.15 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. sequent in this section (this is #4 of 11) Roadway: 28 s= see the deficiency Section again c= Choose another section Enter your choice (d,+/-,s,c): SEGNENT HISTORY SCREEN Seq10:13280 No. 5 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIN_FALL5-STH_64 Last 12 yrs surface history... Cross-Section(up to 10 layers)... Yr trtat PSI(s) PDI(s) Layra Yr. Type Thick. Prev.Lyr.Int. 89 1 84 SglAgg 01.5^{*} -2 63 SglAgg 88 01.5" 87 1,4 3 50 SqlAqq 01.5" ËÁ n (j) n 90 85 1.5 5 94 ċ 83 1 1.6 00 82 9 81 1.6 80 10 79 Base: 11" crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths---Struct Num (with soil, w/o PCC)= 7.15 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. segment in this section (this is #5 of 11) Roadway: 28 s= see the deficiency Section again c= Choose another section Enter your choice (d,+/-,s,c): SEGMENT HISTORY SCREEN No. 6 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIN_FALLS-STH_64 SeqID:13290 Last 12 yrs surface history... Cross-Section(up to 10 layers)... Yr trtat PSI(s) PDI(s) Layr# Yr. Type Thick. Prev.Lyr.Int. 89 1 84 SalAqa 01.5"2 63 SqlAgg 20 01.5* 87 4-4 3 50 SqlAgg 01.5° 86 93 2 85 5 1.1 84 6 83 7 1.5 23 87 81 ņ 1.9 80 10 79 Base: 11° crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths----Struct Num (with soil, w/o PCC)= 7.15 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. segment in this section (this is #6 of 11) Roadway: 28 s= see the deficiency Section again c= Choose another section Enter your choice (d,+/-,s,c):

SEGMENT HISTORY SCREEN SeqID:13300 No. 7 of 11 Sect # 60917830: CHIP FLS-CORNELL/JIM FALLS-STK 64 Last 12 yrs surface history... Cross-Section(up to 10 layers)..., Yr trtot PSI(s) PDI(s) Layr# Yr. Type Thick. Frev.Lyr.Tat. 89 1 79 ColdMx 01.5^{*} -195 2 63 SelAge 01.5" 67 2.0 20 01.5* 50 SqlAqq 38 38 4 85 8...57 1,9 84 6 83 1.7 7 82 2 81 2.1 ŋ 30 10 79 Base: 11" crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths----Struct Num (with soil, w/o PCC)= 6.85 LS PVMT RS d=change display mode to decisions +/~= next/prev. segment in this section (this is \$7 of 11) 2 22 2 Roadway: 28 s= see the deficiency Section again c= Choose another section Enter your choice (d,+/-,s,c): SEGMENT HISTORY SCREEN SeqID:13310 No. 8 of 11 Sect # 60917630; CHIP_FLS-CDANELL/JIM FALLS-STH 64 Last 12 yrs surface history... Cross-Section(up to 10 layers)... Yr trimt PSI(s) PDI(s) Lavr‡ Yr. Tyge Thick. Prev.Lyr.Tat. 89 1 80 ColdMx 01.5° 2 75 SalAga 88 01.5× 87 3 50 SqlAqq 1.8 01.5"86 94 n Li 85 с.п $\{ \cdot, \overline{v} \}$ 84 £, 83 1.57 7-11 82 8 81 2.0 Ş 10 79 Base: 11" crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths---Struct Num (with soil, w/o PCC)= 6.85 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. segment in this section (this is #8 of 11) Roadway: 28 s= see the deficiency Section again c= Choose another section Enter your choice (d.+/~.s.c): SEGMENT HISTORY SCREEN Seq18:13320 No. 9 of 11 Sect # 60917830: CHIP FLS-CORNELL/JIN FALLS-STH 64 Last 12 yrs surface history... Cross-Section(up to 10 layers)... Yr trtst PSI(s) PDI(s) Thick. Prev.Lyr.Imt. Layr# Yr. Type 89 1 79 ColdMx 01.5" 500 610 2 63 SolAag 01.5" 87 3 50 SglAgg 1.5 01.5^{8} 86 78 4 85 1.5 10 84 6 83 2.0 1000 82 0 Ēt 2.3 ç 10

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O.

Sub Base: no subbase recorded no stab. 78 Soil: well draining --Widths---Struct Num (with soil, w/o PCC)= 6.85 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. segment in this section (this is #? of 11) s= see the deficiency Section again Roadway: 28 c= Choose another section Enter your choice (d,+/-,s,c): SEGHENT HISTORY SCREEN Seq10:13330 No.10 of 11 Sect # 60917830: CHIP_FLS-CORNELL/JIM_FALLS-STH_64 Last 12 yrs surface bistory... Cross-Section(up to 10 layers)... Layr# Yr. Type Yr triat PSI(s) PDI(s) Thick. Prev.Lyr.Tot. 1 84 SglAgg 01.5* 89 -2 63 SqlAgg 88 01.5" 87 24 3 50 SglAgg 01.5° 85 59 41.54 85 2.0 CD84 6 7 83 8 82 61 1.9 9 80 10 79 Base: 11" crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths----Struct Num (with soil, w/o PCC)= 7.15 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. segment in this section (this is #10 of 11) s= see the deficiency Section again Roadway: 28 c= Choose another section Enter your choice (d,+/-,s,c): SEGMENT HISTORY SCREEN No.11 of 11 Sect # 60917830: CHIP FLS-CORNELL/JIM FALLS-STH 64 Seq10:13340 Last 12 yrs surface history... Cross-Section(up to 10 layers)... Yr trtat PSI(s) PDI(s) Layr# Yr. Type Thick. Prev.Lyr.Imt. 1 84 SglAgg 89 01.5* 88 2 63 Sq1Agg 01.5* 3 50 SglAgg 87 2.1 01.5ª 86 95 200 85 1.1 2.1 84 6 83 1.37 82 B 81 1.7 ę 80 10 79 Base: 11" crushed gravel no stab. 78 Sub Base: no subbase recorded no stab. Soil: well draining --Widths---Struct Num (with soil, w/o FCC)= 7.15 LS PVMT RS d=change display mode to decisions 2 22 2 +/-= next/prev. segment in this section (this is #11 of 11) s= see the deficiency Section again Roadway: 28 c= Choose another section Enter your choice (d,+/~,s,c):

StH 178 CTH y East = 0.00 1.2 - 1.9 0 3.0 - 3.4 3 5.0 - 6.0 (A) 6.4 - 7.2 (E) 9.0 - 10.0 A miles & spots (300-400) file.

178 Jill - Alle bidg to 64

王子子 longitual Crocking \$1 mile 1.50 - 1.8 longitude Cracking J 3.0 -Rutting longital Crocking 3.3 longuture Crocking 4.7 5.0 5.5 Catoban bridge 5.84 blacktop potche blacklog poteks 5.91 longitual Cracking 6.25 3) \$6.50 Songetud Cracken end of forgetund Chaiking Construct Cracking 64.+178 \$1.0 \$.0 - 10.47 64:+178 9.80 longitual Crocking 9.70-9.5 Congetude Cracking 8.30 longelal Crocking along wall Q) longitud Crocking Ungeling 5 8.0 \$ 7.0 Congutial Crocking 6.8. 6.6 longatual Crocking (3) and of Clock stort of longitud Cracks 6.4 5.9 (z)5.77 end of longalow racks 5.5 to 5.9 Congrenal + rulling 5 3.33 longitual Grackary to ()3.0 rutting

1.5 <u>A malante A</u> Care Carl Same State 1 8 ų, È 6 C.

Asphaltic Base Course, Item 90006A

A. <u>Description</u>. This work shall consist of placing the stockpiled milled asphaltic pavement as base course, at the locations shown on the plans or as directed by the engineer. Removal of the material and stockpiling will be paid for under the item of Removing Asphaltic Surface, Milling.

B. <u>Construction Methods</u>. Work shall be performed using methods described in section 304 of the Standard Specifications except that the milled asphaltic pavement shall be processed so that 95% will pass a 50 mm sieve.

C. <u>Method of Measurement.</u> Asphaltic Base Course will be measured as provided in the contract by the megagram. The quantity to be measured for payment shall be amount of material required and incorporated into the work

D. <u>Basis of Payment</u>. Asphaltic Base Course measured as provided above shall be paid for at the contract unit price per megagram which payment shall be in full for hauling, placing, and compacting; for maintaining; for preparing foundation; and for furnishing all labor, tools, and equipment necessary to complete the work.

20. Crushed Aggregate Base Course, Trench, Item 90006B

A. <u>Description</u>. This work shall consist of placing crushed aggregate base course over the trenches for the pipe culvert installations.

B. <u>Construction Methods</u>. Work shall be performed using methods described in section 304 of the Standard Specifications and the Detail Drawings shown in the plans.

C. <u>Method of Measurement.</u> Crushed Aggregate Base Course, Trench will be measured as provided in the contract by the megagram. The quantity to be measured vor payment shall be the amount of material required and incorporated into the work.

D. <u>Basis of Payment.</u> Crushed Aggregate Base Course, Trench measured as provided above shall be paid of at the contract unit price per megagram which payment shall be in full for hauling, placing and compacting; for maintaining: for preparing foundation and for furnishing all labor, tools ,and equipment necessary to complete the work.

21. Shoulder Coring, Item 90012A

A. Description. This work shall consist of stripping the sod from the existing shoulder and/or removing the existing turf shoulder to an average depth of 150 mm unless otherwise directed by the engineer. The excavated material shall be placed on the existing unstripped inslopes to shape them to the desired slope as shown in the special details of the plan or established by the engineer. The remaining existing crushed aggregate base course shall remain in place.

8580-01-70

11 of 26

B. Construction Methods. The construction methods for shoulder coring shall comply with Section 205.3 of the 1996 Standard Specifications for Highway and Structure Construction. Shoulder Coring shall be done prior to the milling and relaying existing asphaltic pavement.

C. Method of Measurement. All excavation and grading, actually performed and accepted as herein provided and within the specified limits, will be measured in station units of 40 meters along the roadway centerline for each side of the roadway where the work of Shoulder Coring occurs.

D. Basis of Payment. Shoulder Coring, measured as provided above, will be paid for at the contract unit price per 40M. That price shall be payment in full for excavating, placing as fill, and compacting to the specified limits and elevations as shown in the plan. Additional fill required to complete the slopes will be paid for under the item of Borrow Excavation, Common Excavation or Ditching. (090189)

22. Ditching, Item 90012B

A. Description. This work shall consist of the grading new ditches or shaping existing ditches at the locations as shown on the plans. All ditches shall drain in the same direction as the existing ditches unless otherwise directed by the engineer.

B. Construction Methods. The construction methods for ditching shall comply with Section 205.3 of the 1996 Standard Specifications for Highway and Structure Construction.

C. Method of Measurement. All excavation performed and accepted as herein provided and within the specified limits will be measured in station units of 40 meters along the roadway centerline for each side of the roadway where the work of Ditching occurs.

D. Basis of Payment. Ditching, measured as provided above, will be paid for at the contract unit price per 40M. This price shall be payment in full for excavating, hauling, placing as fill and compacting to the specified limits and elevations as shown in the plan, and for disposing of surplus and unsuitable material. Additional fill required to complete the grading will be paid for under the item of Borrow Excavation. Backslope grading in excess of 2 M in height measured from the bottom of the ditch shall be paid for as Common Excavation. Finishing items will be paid for separately.

23. Mill and Relay Asphaltic Pavement, Item 90358

. .

A. <u>Description</u>. This work shall consist of constructing base course utilizing inplace milling and relaying of the existing asphaltic surface over the roadbed as shown on the plans and as hereinafter provided.

B. <u>Construction Methods.</u> The existing asphaltic surface shall be milled to the depth shown on the plans and to a maximum size of 37.5 mm. The milling machine shall be equipped with electronic devices which will provide accurate depth, grade and slope control.

8580-01-70

12 of 26



ILE NAME: D6 85800101:8580TYP.DGN

| | EXISTING D | EPTH (mm) |
|--|---|--|
| LOCATION | ASPHALT | ROAD MIX |
| 23+200 23+690 24+815 26+590 28+035 29+000 29+320 30+930 32+060 32+220 331+85 33+665 | 150 175 175 150 150 125 175 150 175 200 200 | 150 200 175 175 150 300 125 200 150 225 200 300 |

178 Field Review 7-14 - South 223 miles could still be a PiR - North 4 combinations possible - existing SHR 2-5' wide - it still appears that there is other options - 3 curves around 35 mph speed





B.G. wide. }\ 150,000 / mile \$81200 ASPHALT SAME B151000 MILLING SAME \$19,000 BASE 'Z100 # 9 JAL $10_{1} m$ SHOULDER CVT 125 200 MISC DRAINAGE ITEMS ETC. 25,000 \$ 150,000 SYZ SOME CUTS-SAND _ DEF OLD ROAD LORE BORROW-SAND COMPLETELY 12" BAJE BORROW-SAIND 5″ 1\

Resurfacing # 125,000/mile v) MILL OFF2" e 22' wide REPAVE 3'2" 2": (<u>23)(2")(110)(5280</u>), 484 Say 1500 TON/MILE MILLING ASPHALT 3 2": (28')(3.5")(112)(5280) _ 3220 TONSYMILE 18000 MAT'L AC 3220 \$,058 = 187 TONS/MILE 25*6 * 5280 * 2.25 = 660 TONSMILE BASE 3"? 27 COSTMILE =#15,000 1500 TON & 10/TON 1500 TON & 10/TUN MATL 3220 TUNS * 16.50 \$53130 MATL 3270 TUNS * 15.0 = 28,050 MILLING AC 187 TONS \$ 150 ASPHALT : 5940 660 TUNS * B 9,00 # 10 Z 120/MILE BASE 23,000 Mise .

| | | S | TH 1: | | | DZ-01 FALLS-CTI | HR | |
|----------------------|---|-------------------------|---|---|---------------------|--|--|--|
| | | ESTIMA | TED | GRID L | LCA LF. | RE | IELD REVIEW ZQUIRED TO FINAL XATIONS | ZE) |
| PLACE | | 868t00 to 300750 ta | | | 1250 250 | LT È RT FINISHED SHR. PT To FINISHED SHR PT. | PDR DETAIL #3 FIPE REDLACEMEN | ^μ ζζζ |
| under base Course | | 941+50 to 1032+00 to | | | 300 2850 | FINGHED SHR. PT. to FINISHED SHR PT LT | PIPE REPLACEMEN PROFILE ADJUSTMEL PDR DETAIL #4- | π <u>?</u> ??? π <u>?</u> ?? |
| | | 1080+50 t | | a na sa | <i>1550</i> 1950 | LTS ET LTSRT | PDR DETAIL # PDR DETAIL # | |
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Luedtke, Randy

| From: | Perkins, Mike |
|----------|---|
| Sent: | Wednesday, October 11, 2000 1:30 PM |
| То: | Kopacz, Karl |
| Cc: | Luedtke, Randy |
| Subject: | RE: STH 178 - id 8600-02-01, 71 Jim Falls - CTH R -CHIPPEWA CO. Soil Boring Information |

I could not find any soils report in the soils/pavement folders. I offer the following for your DSR:

The project soils were formed along outwash plains and stream terraces. Based on Soil Conservation Service mapping, the predominant soils are Menahga and Friendship. These sandy soils comprise over half the project length. Additional soil associations of some note are Chetek, Caryville and Scott Lake which slant more to the sandy loam and loam soils. Soil borings indicate peat, sand, silty sand, sandy silt, and silt along the project route. Noted in the July 16, 1998 Pavement Design Report, the high water table and the silty soils present could present difficulties during construction (especially in areas of realignment/reconstruction). Portions of the project will include marsh and excavation below subgrade.

Karl,

Let me know if you need more than this for the DSR

| lessage |
|-----------------------------------|
| Kopacz, Karl |
| Tuesday, October 10, 2000 3:51 PM |
| Perkins, Mike |
| STH 178 Soil Boring Information |
| |

Mike:

I am in the process of drafting the DSR for STH 178 (Project I.D. 8600-02-01, CTH Y to CTH R, Chippewa County) and am looking for soil information. Previously this project was scoped as a reconstruct (currently is a recondition) and according to notes in the file there were soil borings completed along this section of STH 178. Unfortunately, I cannot find the actual soil and boring information in the file. I was hoping that you would be able to help me out; do you have the original data, copies, etc. of soil information for this project? Or can you direct me to where I might be able to find it? I would appreciate your help. Thanks......Karl Kopacz, 833-5566

as per Suils Investigation Report Jan 3/2002 shift of 5' BR grid Braken

EBS prior to Grid & Rusher Run

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Correspondence

DISTRICT #6

Department of Transportation

Date: December 29, 1999

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: **PAVEMENT DESIGN DOCUMENTATION-REVISED** Approval Letter

> Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

Upon review of the attached pavement design documentation, the pavement type selection recommendations are approved for the above mentioned project segments. The Project Engineer should forward a copy of this document to the appropriate C.O. representative at this time or attach it as documentation to the revised Design Study Report(DSR).

NOTE: The Exact stationing of the following typicals will be defined with a final field review to completed in 2000-2001.

Reviewed:

Richard J. Shermo, PE Date District #6 Area Supv.-Project Development Section

Approved:

Michael S. Ostrowski, P.E.

District #6 Manager-Project Development Section

COMMENTS

COMMENTS

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last

DISTRICT #6

Department of Transportation

Date: December 29, 1999

To: File

- *From:* Randy W. Luedtke, P.E. District #6 Pavement Design Engineer
- Subject: PAVEMENT DESIGN DOCUMENTATION-REVISED Approval Letter

Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

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29/99

Richard J. Shermo, PE Date District #6 Area Supv.-Project Development Section

Approved:

Michael S. Östrowski, P.E.

District #6 Manager-Project Development Section

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Richard J. Shermo, PE Date District #6 Area Supv.-Project Development Section

Approved:

Michael S. Ostrowski, P.E.

District #6 Manager-Project Development Section

COMMENTS

COMMENTS

RJS MSC MMH RWL FILE

Luedtke, Randy

| From: | | Hayek, Mohamad |
|----------|---|---|
| Sent: | | Tuesday, September 14, 1999 11:24 AM |
| То: | | Anderson, Paul; Effinger, Robert; Bisonette, Dale; Drake, Raymond; Helgeson, Greg; Kern, Jeffrey; Shermo, Richard; Hyland, Lary; Ostrowski, Mike; Luedtke, Randy; Pawelski, Timothy; Hayek, Mohamad |
| Subject: | , | Agenda For STH 178 Design Review Meeting on THurs. Sep. 16,1999 |

1. Design Constraints / Criteria / Commitments

-Typical -Clear zone -Design Speed -Exception to Standards

2. Review of Horizontal & Vertical Alignments

-DNR Concerns -Critical locations -Intersections -By - Pass left turn lanes -Vision Triangles -Misc. Items (Cobban Bridge , etc.)

3. Construction Staging

-Filing over old ditch lines (for slight alignment shifts) -Special slopes (rip rap). -Misc. items.

4. Structures

-Retaining Walls -Culverts

- 5. Drainage
 - -Curb & Gutter Locations -Culverts

6. R / W

-Reduce Access / Driveways -6F (Wayside) -Misc. items

7. Misc.

-Schedule -Cost Estimate -DNR coordination / concerns -Archeology -Environmental concern / update



4/11/00 STH 178 /of 3 Mill \$ Overlay: 789+51 to 859+00 (Beamgard 811+00 to 814+00 Right) Align Correction: 859+00 to 868+00 Mill & Overlay: 868+00 to 906+50 Profile Correction: 906 + 50 + 910 + 75Mill \$ Overlay: 910+75 to 922+75 Profile Correction: 922+75 to 935+25 (Beamguard 929+00 to 932+00 Right) Mill & Overlay: 935+25 to 938+50 Profile Correction : 438+50, to 946+00 (Beamouand 940+50 to 944+00 Right ELett)

4/11/00

2 of 3

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Align Correction 970+00 to 980+25 (Beamguad 970+00 to 978+00 Right) ?

Profile Correction 980+25 to 297+50

Mill & Overlay 997+50 to 999+85

Profile Correction 999+85 to 1004+50

Mill # Overlay 1004+50 to 1008+50

Align Correction 1008+50 to 1029+00 (Beamguard 1012+50 to 1016 Right)

Mill & Overlay 1029+00 to 1063+00 (Bunguard 1030+00 to 1063+00 Right)

Profile Correction 1063+00 to 1074+00 (Beamqued 1863+0) to 1076+00)

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Mill & Overlay 1141+00 to 1164 + 21 (Beingmand 1141+00 to 1144+50, 1147+00 to 1149+00 Right)

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DISTRICT #6

Date: December 29, 1999

To: File

- *From:* Randy W. Luedtke, P.E. District #6 Pavement Design Engineer
- Subject: PAVEMENT DESIGN DOCUMENTATION-REVISED Approval Letter

Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

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Reviewed:

COMMENTS

Richard J. Shermo, PE Date District #6 Area Supv.-Project Development Section

Approved:

COMMENTS

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

| RJS | |
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DISTRICT#6

Date: December 29, 1999

To: File

From: Randy W. Luedtke, P.E. District Pavement Design Engineer

Subject: Pavement Documentation -*REVISED* Project ID 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

On this project, the Pavement Design Report for reconstruction was approved in October of 1998 as a 5" asphalt over 11" of Base over 11" of sand lift. In the fall of 1999, the project was re-visited to redefine the scope of the project. Since the roadway is classified as a collector and not an arterial highway, it was concluded that the District's 33 program could not handle a full reconstruct option. In-house and field review has led to the following alternatives being chosen as the best solution to fit under the initial cost constraints. The LCCA was not re-done because all of the additional alternatives drawn below have less initial cost than the reconstruct typical.

State of Wisconsin

Department of Transportation



A provision should be included that the lower lift asphalt paving operation shall start within 10 calendar days of any area that has been surface milled. Shoulder shall be shaped prior to paving to allow for a 1 ¹/₂" lower layer and 2" surface layer



TYPICALS -CONT.



*1-3' if beam guard area

In areas where the grid is only needed on ½ of the roadway, there will need to be some staging specified on the plan. An example is as follows: 1. Notch shoulder at existing edge to a depth of 10" and push outward to widen shoulder. 2. Mill out and/or remove existing ½ roadway core to a depth of 10" and stockpile material(if no local traffic -stockpile on adjacent lane). 3. Place grid 4. Relay/Spread salvaged road core material over grid and widened shoulder area. 5. Add additional base course to provide a minimum of 8" lift material over the grid area. 6. Place 1 ½" Asphalt to match adjacent surface milled profile. *This example will/may need to be modified to match final plan conditions*.

There should also be a provision that no trucking or other heavy construction traffic be allowed in grid area until at lest the lower levels of asphalt(3") are placed.



TYPICALS -CONT.



Transition details will be required when switching from typical to typical. Length of transition will be dependent upon location.

The Lane line should be placed at 11' on all typical sections and is very important that it be placed there for stability and support in the typical sections 1-4.

Lane and shoulder widths may be modified to match appropriate 3R standards.

Randy W. Luedtke, PE

CORRESPONDENCE/MEMORANDUM DISTRICT #6

Date: December 29, 1999

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: PAVEMENT DESIGN DOCUMENTATION-<u>REVISED</u> Approval Letter

> Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

Upon review of the attached pavement design documentation, the pavement type selection recommendations are approved for the above mentioned project segments. The Project Engineer should forward a copy of this document to the appropriate C.O. representative at this time or attach it as documentation to the revised Design Study Report(DSR).

NOTE: The Exact stationing of the following typicals will be defined with a final field review to completed in 2000-2001.

Reviewed:

COMMENTS

Richard J. Shermo, PE Date District #6 Area Supv.-Project Development Section

Approved:

COMMENTS

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

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| RWL | |
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DISTRICT#6

Date: December 29, 1999

To: File

From: Randy W. Luedtke, P.E. District Pavement Design Engineer

Subject: Pavement Documentation -REVISED Project ID 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

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A provision should be included that the lower lift asphalt paving operation shall start within 10 calendar days of any area that has been surface milled. Shoulder shall be shaped prior to paving to allow for a 1 ¹/₂" lower layer and 2" surface layer



TYPICALS-CONT.



*1-3' if beam guard area

In areas where the grid is only needed on ½ of the roadway, there will need to be some staging specified on the plan. An example is as follows: 1. Notch shoulder at existing edge to a depth of 10" and push outward to widen shoulder. 2. Mill out and/or remove existing ½ roadway core to a depth of 10" and stockpile material(if no local traffic -stockpile on adjacent lane). 3. Place grid 4. Relay/Spread salvaged road core material over grid and widened shoulder area. 5. Add additional base course to provide a minimum of 8" lift material over the grid area. 6. Place 1 ½" Asphalt to match adjacent surface milled profile. *This example will/may need to be modified to match final plan conditions.*

There should also be a provision that no trucking or other heavy construction traffic be allowed in grid area until at lest the lower levels of asphalt(3") are placed.



Sand lift material should be specified as Grade #2

TYPICALS -CONT.



Transition details will be required when switching from typical to typical. Length of transition will be dependent upon location.

The Lane line should be placed at 11' on all typical sections and is very important that it be placed there for stability and support in the typical sections 1-4.

Lane and shoulder widths may be modified to match appropriate 3R standards.

Randy W. Luedtke, PE

CONCEPT DEFINITION REPORT

To: Michael A. Cass (P.E.)

From: District 6

- Related ID(s): 8600-02-71(Const) I. Design ID: 8600-02-01 Highway No. or Local Road Name: STH 178 8600-02-21 (R/W) Title: CHIPPEWA FALLS - CORNELL ROAD Length: 7.4 Miles 11.9 km County: CHIPPEWA Functional Class: Major Collector Current ADT: 1650 (1993) LOCATION: CTH Y - CTH R Roadway Conditions: II. A. Width: 22 Pavement: Type: AC Year: 1981 PSI: 2.69 (1993) PDI: 30 (1994) Shoulder: Type: Gravel Accident Rate: 480 Width: 2 Year: 1995 Substandard Alignment: Horizontal: Yes Vertical: Yes
 - B. Structure: (may be continued on back side) Type: DECK GIRDER Length: 86.5 ft, 26.4 m Bridge Number: B-09-0682 Year Constructed: 1942 Clear Roadway Width: 27.6 SR: 80.5 RS: 89.4

JUSTIFICATION: Accident rate is 480 vs State ave of 222 because of narrow shoulders, sharp horiz curvature and short vertical and horiz sight distance. There are many power poles and trees in clear zone.

III. PROPOSED IMPROVEMENT: Grade, Base, Asphaltic Surface to C3 standards with a 24 ft surface on a 36 ft roadway with a 30 ft clear zone.

A. Environmental documentation type: III ER

- B. Improvement Type: RECST PMSID: 98060020201
- C. Cost: \$ 3,850,000 Program Year: 2002 Program: 3334
- D. Local Participation: \$ No Access Control: No

DISTRICT 6 APPROVAL Project Supervisor

Planning Supervisor

Date: 07/17/96

Concept Definition Report Project: 8600-02-01

CC: Gerry Feiler - Rm 951, Len Stanek - Rm 651, Bureau of Environment - Rm 451 Gene Hoelker - FHWA

District 6 Geographic Information System

Page: 1 of 2 Date: 07/17/96

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Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: **PAVEMENT DESIGN REPORT** Approval Letter

> Project I.D. 8600-02-01 Chippewa Falls - Cornell Road Jim Falls - CTH R STH 178 Chippewa County

Upon review of the attached pavement design documentation, the pavement type selection recommendations are approved for the above mentioned project segments.

Reviewed:

7/14/98

Richard J. Shermo, P.E. Date District #6 Area Supv.-Project Development Section

Approved:

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

COMMENTS Have some concern about the slight horizontal alignment "shifts" which puts New & over the old Rendy, can you set up sch line meeting so the 4 of us can Weakot RJS 7/16 dir20352 3~ MSO 2 MMH 7/23 at >RWL

COMMENTS

CORRESPONDENCE/MEMORANDUM DISTRICT #6

Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: **PAVEMENT DESIGN REPORT** Approval Letter

> Project I.D. 8600-02-01 Chippewa Falls - Cornell Road Jim Falls - CTH R STH 178 Chippewa County

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Reviewed:

COMMENTS

Richard J. Shermo, P.E. Date District #6 Area Supv.-Project Development Section

Approved:

COMMENTS

Michael S. Ostrowski, P.E. Date District #6 Manager-Project Development Section

State of Wisconsin Transportation District #6

CORRESPONDENCE/<u>MEMORANDUM</u>

Date: July 16, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: Pavement Design Report Project 8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa County

EXECUTIVE SUMMARY

This report makes the following recommendations for the proposed reconstruction project.

| LOCATION | PAVEMENT STRUCTURE | THICKNESS |
|---------------------------------|---------------------------------|---|
| STH 178-mainline & bypass lanes | Asphalt/ Base Course/ Sand Lift | 125mm/275mm/275mm (5") /(11") /(11") |
| Side Roads >500 ADT | Asphalt/ Base Course | 100mm/300mm (4") /(12") |
| Side Roads <500 ADT | Asphalt/Base Course | 75mm /225mm (3") /(9") |

Type MV Asphaltic Concrete Pavement mix with PG grade 58-28 should be used for this project. It is anticipated that by the time this plan is let to bid, a different PG graded oil could be the standard. The designer should coordinate the special provisions to reflect the correct AC type.

The 125mm(5") asphalt pavement should be constructed with two lower layers totaling $85mm(3 \frac{1}{2})$ and a upper layer of $40mm(1 \frac{1}{2})$. The 100mm(4") asphalt pavement should be constructed with a 50mm(2") lower layer and a 50mm(2") upper layer. The 75mm(3") asphalt pavement should be constructed with two layers.

The sand lift should be specified to meet Grade #1 requirements as specified in the Standard Specifications Section 209.2.2 for granular backfill.

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EXISTING CONDITIONS

This 11.9km(7.4 mile) project involves the portion of STH 178 from the intersection of CTH Y at Jim Falls northerly along the Chippewa River to the intersection of CTH R. Due to a high accident rate, as stated in the CDR, the roadway will be reconstructed to C3 standards. This roadway is not being reconstructed due to excessive pavement failures or deficiencies. It appears that the roadway was last resurfaced in 1981 with a maintenance type overlay. The 1996 PDI ranged from 28-75 for this section. The 1997 IRI ranged from 1.4-3.6.

In 1993, the roadway core was investigated for a resurfacing type project. Since that time, the concept was revised to a reconstruct type improvement. The 1993 borings are located in the technical services project records.





TRAFFIC PROJECTIONS

The construction year-0 year ADT is 2000 and the 20 year ADT is projected to be 2400.

Truck percentages are as follows:

| TRUCK TYPE | | <u>%</u> |
|---|-------|---------------------------------|
| 2D 3AX 2SI,2S2 3-S2 DBL.BTM | | 3.6 1.3 0.8 2.3 0.0 |
| | TOTAL | 8.0 |

PROPOSED IMPROVEMENT

This project is currently scheduled for a reconstruct(RECST) type improvement. The existing roadway will be reconstructed to C3 standards which will include adjustments to the horizontal and vertical alignments.

SOIL ENGINEERING FACTORS

Over the length of this project, many different soil series are located under the roadway. The roadway core itself, as revealed in the 1993 roadway borings, has various amounts of silt and topsoil present along with some granular material in some of the fill locations. With the existing roadway material varying from moist to wet, construction could be a problem. With the existing silty materials in mind, it was agreed to with the Soils Engineer- Lary Hyland that a sand lift would be the best choice in this situation. For further discussion see the "alternative evaluated section". The DGI recommended for this roadway is 14 with a soil support value of 4.0. At the time of this report, due to the uncertainty of the horizontal and vertical alignment only a preliminary soils analysis has been completed.

FRICTION CHARACTERISTICS

The aggregate is expected to be igneous with 0% dolomite and a 20% L.A. wear resulting in a friction number of 44 and 51 for the PCC. Friction is not expected to be a problem.

ALTERNATIVES EVALUATED and RECOMMENDATIONS

Alternative Discussion

Initially, this segment of roadway was scheduled for a maintenance type overlay in 1998. That project was scrapped and the roadway segment is now being evaluated as a reconstruct to C3(100KM/60MPH) standards. In January 1997, the project was explained to me as a typical shoulder widening project on the south end with some short segments of relocation from the middle of the project northward to CTH R. Since that time, evaluation by the development staff has led to a concept of a total reconstruction.

I have numerous concerns that need to be addressed. The horizontal alignment, provided at the time of this report, continually drifts on and off the centerline of the existing road core in a range of 0-8 feet(0-2.5m). We have had past mid lane failures in minor grading areas when part of the old core supports the new lane and new material is added adjacent to support the remaining lane. Besides the obvious heave potential of the different materials, differential settlement occurs in the new material due to different compaction levels of the new material versus the old road core. As shown on the plan sheets and preliminary sections, in many cases, the subgrade point is being moved out over wet silty marshy material in the old ditches. Also in many locations, water is within 2-3 feet of the pavement surface. At this point in the design process, I can only assume that the designer will follow through with his/her responsibility to provide information to and coordinate with the district Soils Engineer to identify and treat these problem areas once the final horizontal and vertical alignment is chosen. In past situations of widening over old ditches, these areas have either been excavated and back-filled or a grid/back-fill combination was used. The high water table is a separate issue, as obviously it is hard to construct a stable subgrade within 1-2 feet of the existing water elevation. There is a reasonable chance that the asphalt/base/sand lift pavement will not perform in this situation . The designer should remember that a sand lift or breaker run platform will typically push the subgrade to 2 feet or greater below the finished profile.

Alternative Discussion-cont.

On other projects/roadways of this type, past experience had led to a district sequence of operations where the horizontal alignment is left in place and the shoulders are widened and raised to the existing profile. If a sag vertical deficiency exists in this area we will typically gravel lift up to a foot to improve the profile. Crest and sag verticals are routinely excepted to standards of 40 mph if there is no accident history at that location. After the widening or lifting is completed the traveled way surface is addressed with some type of overlay or mill/pulverize & relay and overlay combination, always taking care to remain in the middle of the old roadway core. We typically do experience some shoulder distortion but it is not critical to the performance of the pavement. Besides achieving pavement performance, this operation also has the benefit of providing adequate local access because, typically 2 lane traffic can be provided in the off hours and on weekends during the life of the project.

With reconstruction of the existing STH 178 roadway the project option chosen versus the above mentioned scenario, local access and staging of construction activities will both play major roles in the plan development. Since local access will need to be provided, I am assuming a grading operation will need to be completed one half at a time with excavation, EBS, back-fill, borrow, sand lift and base course progressing down the roadway as access permits. The relocation areas are typically completed separately with the old road in these relocated areas being obliterated at the end. For the sand lift to perform in the pavement structure, the sand cannot be placed on a rutted un-rolled subgrade. This typically requires the contractor to exercise care in the placing of the lift material. Some type of drain will be required at the low points in the sand lift profile. A breaker run was not chosen due the availability of local materials.

With this type of work, it is beneficial to work during the dry part of the summer. Even with these precautions, there is a reasonable chance that stage construction grading might not be completed in one year. Soft spots in the base could be common place under the reconstruct option. If the base course and the two lower layers were placed in year one, the surface layer could be placed the following year. This approach would allow some repair of the broken up areas prior to the final surface being placed.

SUMMARY OF COSTS-----LCCA

A twenty year service life was used.

The first alternative is : 175mm(7") PCC over 150mm(6") base over sand lift: \$219008 per KM for initial construction cost \$ 11463 per KM for Equivalent Uniform Annual Cost The second alternative is : 125mm(5") AC over 275mm(11") base course over 275mm(11") sand lift: \$155257 per KM for initial construction cost

\$ 9759 per KM for Equivalent Uniform Annual Cost
 The third alternative is : 140mm(5 ½")AC over 300(12") base course *
 \$ \$157763 per KM for initial construction cost
 \$ 9921 per KM for Equivalent Uniform Annual Cost

* Not recommended due to sand lift requirement. For information purposes only

RECOMMENDATIONS

| LOCATION | PAVEMENT STRUCTURE | THICKNESS |
|---------------------------------|---------------------------------|---|
| STH 178-mainline & bypass lanes | Asphalt/ Base Course/ Sand Lift | 125mm/275mm/275mm (5") /(11") /(11") |
| Side Roads >500 ADT | Asphalt/ Base Course | 100mm/300mm (4") /(12") |
| Side Roads <500 ADT | Asphalt/Base Course | 75mm /225mm (3") /(9") |

Type MV Asphaltic Concrete Pavement mix with PG grade 58-28 should be used for this project. It is anticipated that by the time this plan is let to bid, a different PG graded oil could be the standard. The designer should coordinate the special provisions to reflect the correct AC type.

The $125 \text{mm}(5^{"})$ asphalt pavement should be constructed with two lower layers totaling $85 \text{mm}(3 \frac{1}{2}^{"})$ and a upper layer of $40 \text{mm}(1 \frac{1}{2}^{"})$. The $100 \text{mm}(4^{"})$ asphalt pavement should be constructed with a $50 \text{mm}(2^{"})$ lower layer and a $50 \text{mm}(2^{"})$ upper layer. The $75 \text{mm}(3^{"})$ asphalt pavement should be constructed with two layers.

The sand lift should be specified to meet Grade #1 requirements as specified in the Standard Specifications Section 209.2.2 for granular backfill.

The designer should use asphaltic surface items for incidental asphalt work such as driveways, safety islands, etc. as allowed under the 1997 Supplemental Specs.

Randy W. Luedtke, P.E.



RIGID PAVEMENT DESIGN WORKSHEET

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT DESIGN YEAR DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|------------------|
| 2,000 |
| 2022 |
| 2,400 |
| <u>0</u> .50 |
| 1.00 |
| 20.0 |
| 1,100 |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL'S |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 1.2 | 17 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.6 | 5 |
| 3S-2 | 2.3 | 1,100 | 25 | 1.6 | 40 |
| DBL BTM | 0.0 | 1,100 | 0 | 2.1 | 0 |
| DESIGN LANE DAILY ESAL's | 8.0 | | | | 74 |
| DESIGN LANE TOTAL LIFE ESAL'S | | | | Γ | 540,200 |

SOILS:

MODULUS OF SUBGRADE REACTION (K)

30

THICKNESSES:

CALCULATED PAVEMENT THICKNESS PAVEMENT THICKNESS TO BE USED



FLEXIBLE PAVEMENT DESIGN WORKSHEET

Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls – CTH R STH 178 Chippewa

TRAFFIC:

CONSTRUCTION YEAR CONSTRUCTION YEAR ADT DESIGN YEAR DESIGN YEAR ADT DIRECTIONAL FACTOR (DF) LANE DISTRIBUTION FACTOR (LDF) TRAFFIC ANALYSIS PERIOD DESIGN LANE TRAFFIC (DLT)

| 2002 |
|-----------|
| 2,000 |
| 2022 |
| 2,400 |
| 0.50 |
| 1.00 |
| 20.0 |
| 1,100 |

LOADING:

| | | | | ESAL LOAD | |
|-------------------------------|----------|-------|----------|-----------|---------|
| TRUCK TYPE | % OF ADT | DLT | # TRUCKS | FACTOR | ESAL's |
| 2D | 3.6 | 1,100 | 40 | 0.3 | 12 |
| 3–SU | 1.3 | 1,100 | 14 | 0.8 | 11 |
| 2S-1,2S-2 | 0.8 | 1,100 | 9 | 0.5 | 4 |
| 3S-2 | 2.3 | 1,100 | 25 | 0.9 | 23 |
| DBL BTM | 0.0 | 1,100 | . 0 | 2.0 | 0 |
| DESIGN LANE DAILY ESAL'S | 8.0 | | | | 50 |
| DESIGN LANE TOTAL LIFE ESAL'S | | | | | 365,000 |

SOILS:

> DESIGN GROUP INDEX SOIL SUPPORT VALUE FROST INDEX

| | 14 |
|-----|-----|
| | 4.0 |
| F-3 | |

DESIGN - SN VALUE & MIX TYPE:

3.0

3.49

SERVICEABILITY INDEX **REQUIRED SN VALUE**

ASPHALT MIX TYPE: MV

ALTERNATE DESIGN:

| | Asphalt/base/s | sand | Asphalt/base | | | |
|----------------------------|------------------|------|--------------|---------|------|--|
| LAYER | THICKNESS COEFF. | SN | THICKNESS | COEFF. | SN | |
| SURFACE: | SURFACE | | | SURFACE | | |
| ASPHALTIC CONCRETE | 125 0.0173 | 2.16 | 140 | 0.0173 | 2.42 | |
| EXISTING ASPHALT | 0.0100 | 0.00 | | | 0.00 | |
| BASE COURSE: | BASE | | | BASE | | |
| CRUSHED AGG, BASE COURSE | 275 0.0039 | 1.07 | 300 | 0.0039 | 1.17 | |
| OPEN GRADED BASE COURSE #1 | | 0.00 | | | 0.00 | |
| OPEN GRADED BASE COURSE #2 | | 0.00 | | | 0.00 | |
| EXISTING BASE | 0.0039 | 0.00 | | 0.0039 | 0.00 | |
| EXISTING AC | | 0.00 | | | 0.00 | |
| PULVERIZED AC | | 0.00 | | | 0.00 | |
| EXISTING PCC | | 0.00 | | | 0.00 | |
| RUBBLIZED PCC | | 0.00 | | | 0.00 | |
| CRACK (BREAK) & SEAT PCC | | 0.00 | | | 0.00 | |
| SUBBASE COURSE: | SUBBASE | | | SUBBASE | | |
| CRUSHED AGG. BASE COURSE | | 0.00 | | | 0.00 | |
| BREAKER RUN | | 0.00 | | | 0.00 | |
| GRANULAR SUBBASE | 275 0.0012 | 0.33 | | | 0.00 | |
| EXISTING SAND LIFT | 0.0025 | 0.00 | | 0.0025 | 0.00 | |
| TOTAL SN VALUE | | 3.57 | | | 3.59 | |

FLEXIBLE PAVEMENT DESIGN

ALTERNATE DESIGN:

| | | Existing Structu | re | | | |
|----------------------------|----------------|------------------|------|-----------|---------|----------|
| LAYER | THICKNESS | COEFF. | SN | THICKNESS | COEFF. | SN |
| SURFACE: | | SURFACE | | | SURFACE | <u> </u> |
| ASPHALTIC CONCRETE | 125 | 0.0173 | 2.16 | | 0.0173 | 0.00 |
| EXISTING ASPHALT | | | 0.00 | | | 0.00 |
| BASE COURSE: | | BASE | | | BASE | |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | 0.0039 | 0.00 |
| OPEN GRADED BASE COURSE #1 | | | 0.00 | | | 0.00 |
| OPEN GRADED BASE COURSE #2 | | | 0.00 | | | 0.00 |
| EXISTING BASE | 125 | 0.0039 | 0.49 | | | 0.00 |
| EXISTING AC | | | 0.00 | | | 0.00 |
| PULVERIZED AC | | | 0.00 | • | | 0.00 |
| EXISTING PCC | | | 0.00 | | | 0.00 |
| RUBBLIZED PCC | | | 0.00 | | | 0.00 |
| CRACK (BREAK) & SEAT PCC | | | 0.00 | | | 0.00 |
| SUBBASE COURSE: | | SUBBASE | | | SUBBASE | 0.00 |
| CRUSHED AGG. BASE COURSE | | | 0.00 | | | 0.00 |
| BREAKER RUN | | | 0.00 | | | 0.00 |
| GRANULAR SUBBASE | | | 0.00 | | 0.0012 | 0.00 |
| EXISTING SAND LIFT | | 0.0025 | 0.00 | | | 0.00 |
| TOTAL SN VALUE | | | 2.65 | | | 0.00 |
| | SN is Less Tha | n SNrog'd | | | | 0.00 |

SN is Less Than SNreq'd

PAVEMENT SURFACE FRICTION DESIGN

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PCC MIX AGGREGATES

0

20

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Chippewa

TRAFFIC:

| CONSTRUCTION YEAR ADT | 2,000 | | |
|--|--------|------------------|-------|
| DESIGN YEAR ADT | 2,400 | EXP. GROWTH RATE | 0.92% |
| DIRECTIONAL FACTOR (DF) | 0.50 | | |
| LANE DISTRIBUTION FACTOR (LDF) | 1.00 | | |
| % HEAVY VEHICLES (HV) | 8.0 | | |
| AC PAVEMENT AGE OR SERVICE LIFE (YR) | 15.0 | AC "AGE" ADT | 2,293 |
| AC LAVP AT SPECIFIED AGE (IN MILLIONS) | 5.876 | | |
| PC PAVEMENT AGE OR SERVICE LIFE (YR) | 25.0 | PC "AGE" ADT | 2,512 |
| PC LAVP AT SPECIFIED AGE (IN MILLIONS) | 10.293 | | |

AGGREGATE PROPERTIES:

AC MIX AGGREGATES

0

20

| % DOLOMITE | |
|------------|--|
| %1A WFAR | |

AC AGGREGATE SOURCE: PCC AGGREGATE SOURCE:

DESIGN

ASPHALTIC SURFACE FORMULA

FN40 = 41.4 - 1.45 ln(LAVP) + 0.245(LAWEAR) - 0.00075(DOLOMITE) ^2

| FN40 AT SPECIFIED PAVEMENT AGE | 43.7 |
|---|--------|
| % PROBABILITY THAT CALCULATED VALUE IS < 35 | 7.9 |
| | |
| AGE (YR) WHEN FN40=35 | AGE>50 |

CONCRETE SURFACE FORMULA

 $\ln(FN40) = 3.99 - 0.0419\ln(LAVP) - 0.00129(DOLOMITE) + 0.00474(HV)$

| FN40 AT SPECIFIED PAVEMENT AGE | 50.9 |
|---|--------|
| % PROBABILITY THAT CALCULATED VALUE IS < 35 | <0.05% |
| | |
| AGE (YR) WHEN FN40=35 | AGE>50 |
| | |

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| | BID ITEM | | UNIT |
|--|--------------|-------|----------|
| BID ITEM | # | UNITS | COST |
| ASPHALTIC MATERIAL FOR TACK COAT | 40204 | L | \$1.00 |
| ASPHALTIC MATERIAL FOR PLANT MIXES | 40501 | Mg | \$155.00 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE HV | 40712 | Mg | \$22.00 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE MV | 40713 | Mg | \$16.50 |
| ASPHALTIC CONCRETE PAVEMENT, TYPE LV | 40714 | Mg | \$16.50 |
| RECYCLED ASPHALTIC SURFACE, TYPE HV | 90381 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE MV | 90382 | Mg | |
| RECYCLED ASPHALTIC SURFACE, TYPE LV | 90383 | Mg | |
| CONCRETE PAVEMENT, 150 mm | 41506 | sm | \$13.50 |
| CONCRETE PAVEMENT, 175 mm | 41507 | sm | \$18.00 |
| CONCRETE PAVEMENT, 200 mm | 41508 | sm | \$18.00 |
| CONCRETE PAVEMENT, 225 mm | 41509 | sm | \$20.25 |
| CONCRETE PAVEMENT, 250 mm | 41510 | sm | |
| CONCRETE PAVEMENT, 275 mm | 41511 | sm | |
| CONCRETE PAVEMENT, 300 mm | 41512 | sm | |
| CONCRETE WIDENING | 41530 | sm | |
| CONTINUOUS CONCRETE PAV'T REINFORCEMENT | 41551 | sm | |
| PAVEMENT TIES | 41571 | EACH | \$5.00 |
| DOWEL BARS | 41572 | EACH | \$5.00 |
| CRUSHED AGGREGATE BASE COURSE | 30404 | Mg | \$7.75 |
| OPEN GRADED BASE COURSE #1 | 30418 | Mg | \$9.00 |
| OPEN GRADED BASE COURSE #2 | 30420 | Mg | \$9.00 |
| ASPHALTIC BASE COURSE | 30601 | Mg | |
| ASPHALTIC BASE COURSE WIDENING | 30606 | Mg | |
| CONCRETE BASE COURSE | 30706-9 | sm | |
| CONCRETE BASE COURSE WIDENING | 30751 | sm | |
| BREAKER RUN | 30426 | Mg | \$7.00 |
| GRANULAR SUBBASE COURSE | 21201 | cm | \$3.30 |
| MILL AND RELAY ASPHALTIC CONCRETE PAVEMENT | | sm | \$0.86 |
| SALVAGED ASPHALTIC PAVEMENT | 41010 | Mg | |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | 41020 | Mg | \$7.72 |
| ASPHALTIC SURFACE, PATCHING | 41102 | Mg | |
| PULVERIZING ASPHALTIC CONCRETE PAVEMENT | NT-51/7/ 51/ | sm | \$0.70 |
| BASE PATCHING, ASPHALTIC | 30810 | sm | |
| BASE PATCHING, CONCRETE | 30820 | sm | \$40.95 |
| CRACKING AND SEATING CONCRETE PAVEMENT | 41040 | sm | |
| BREAKING AND SEATING CONCRETE PAVEMENT | | sm | |
| CONCRETE PAVEMENT REPAIR | 41574 | cm | \$183.00 |
| CONTINUOUS DIAMOND GRINDING | 41576 | sm | \$2.69 |
| RUBBLIZING CONCRETE PAVEMENT | | sm | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE A | 60123 | m | |
| CONCRETE CURB & GUTTER, 750 mm, TYPE D | 60133 | m | |
| GEOTEXTILE FABRIC, TYPE DF | 64503 | sm | \$1.20 |
| PIPE UNDERDRAIN, 150 mm | 61201 | m | \$4.43 |
| PIPE UNDERDRAIN, UNPERFORATED, 150 mm | 61211 | m | \$22.15 |
| R.C. APRON ENDWALLS FOR UNDERDRAIN | 61254 | EACH | \$125.00 |
| REMOVING PAVEMENT | 20401 | sm | |
| GEO-GRID | '90xxx | sm | \$1.75 |
| | | | |

ALTERNATE DESCRIPTION WORKSHEET

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| PARAMETER | UNITS | ALT 1 VALUE | ALT 2 VALUE | ALT 3 VALUE | ALT 4 VALUE | ALT 5 VALUE | ALT 6 VALUE |
|--|------------------|----------------|----------------|-----------------|---|------------------|----------------|
| RURAL OR URBAN PROJECT | R/U | 1 | 1 | 1 | | | |
| ROADWAY WIDTH | m | 10.80 | 10.80 | 10.80 | | | |
| PAVEMENT STRUCTURE WIDTH | m | 7.20 | 7.20 | 7.20 | | | |
| TOTAL PAVED SHOULDER WIDTH | m | 1.80 | 1.80 | 1.80 | | | |
| CONCRETE RDWY PAVEMENT THICKNESS | mm | 175 | | | | | |
| CONCRETE SHOULDER THICKNESS | mm | 175 | | | | | |
| AC RDWY PAVEMENT MIX TYPE | HV/MV/LV | | MV | MV | | | |
| TOTAL AC RDWY PAVEMENT THICKNESS | mm | | 125 | 140 | 125 | | |
| VIRGIN AC RDWY PAVEMENT THICKNESS | mm | | 125 | 140 | | | |
| % OF ASPHALT CEMENT USED | % | | 6.0 | 6.0 | | | |
| RECYCLED AC RDWY PAVEMENT THICKNESS | mm | | | | | | |
| % OF ASPHALT CEMENT USED | | | | | | | |
| % RAP | | | | | | | |
| AC SHOULDER PAVEMENT MIX TYPE | HV/MV/LV | | MV | mv | | | |
| TOTAL AC SHOULDER PAVEMENT THICKNESS | mm | L | 125 | 140 | | | |
| VIRGIN AC SHOULDER THICKNESS | mm | | 125 | 140 | | | |
| RECYCLED AC SHOULDER THICKNESS | | | | | | | |
| % OF ASPHALT CEMENT USED | | | 6.0 | 6.0 | | | |
| ASPHALTIC CONCRETE PAVEMENT WT. TACK COAT COVERAGE | kg/sm/mm | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 | 2.3 |
| WHICH LAYER IS THE DRAINAGE LAYER? | L/sm | 0.113 | 0.113 | 0.113 | 0.113 | 0.113 | 0.113 |
| CRUSHED AGG. BASE COURSE THICKNESS | 0-4 | 0 | 0 | | 0 | 0 | |
| UNIT WT OF CABC | mm | 150.00 | 275.00 | 300.00 | 0 | | |
| OPEN GRADED BASE COURSE #1 THICKNESS | Mg/cm | 2.4 | 2.4 0 | 2.4 | | | |
| UNIT WT OF OGBC #1 | mm Mg/cm | | | 0 | 0 | | |
| OPEN GRADED BASE COURSE #2 THICKNESS | mm | | | 0 | 0 | | |
| UNIT WT OF OGBC #2 | | | | 0 | 0 | | |
| BREAKER RUN THICKNESS | mm | | 0 | . 0 | 0 | | |
| UNIT WT OF BREAKER RUN | Mg/cm | | ····· | 0 | | | |
| ASPHALTIC STABILIZED B.C. THICKNESS | mm | | | | | | |
| % OF ASPHALTIC CEMENT USED | % | | | | | | |
| UNIT WT OF AC STABILIZED BASE COURSE | Mg/cm | | | | | | |
| P.C. STABILIZED BASE COURSE THICKNESS | mm | | | | | | |
| UNIT WT OF PCC STABILIZED BASE COURSE | Mg/cm | | | | | ******** | |
| GRANULAR SUBBASE COURSE THICKNESS | mm | 275 | 275 | 0 | 0 | | |
| OTHER #1 (STRUCTURE WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| OTHER #2 (ROADWAY WIDTH) | mm | | | | | | |
| | Mg/cm | | | | | | |
| EXISTING PAVEMENT WIDTH | m | | 6.70 | 6.70 | | | |
| EXISTING PAVEMENT THICKNESS | mm | | | | | | |
| % OF PROJECT LENGTH FOR CURB & GUTTER | % | | | | | | |
| TYPE OF CURB & GUTTER | A/D | | | | | | |
| 6 OF PROJECT LENGTH FOR GEOTEXTILE FABRIC | % | | | | | | |
| 6 OF PROJECT LENGTH FOR UNDERDRAINS | % | | | | | | |
| 6 OF PROJECT LENGTH FOR TACK COATING | % | | 66 | 66 | | | |
| TOTAL m2 OF CRCP STEEL REINFORCEMENT | sm | | | | | | |
| 60F PROJECT LENGTH FOR MILL & RELAY AC PAV'T 60F PROJECT PAV'T AREA FOR AC SURF PATCHING | % | | | | | | |
| 60F PROJECT LENGTH FOR PULVERIZING AC PAV'T | % | | | | | | |
| AILLING DEPTH | % | | | | | | |
| 60F PROJECT LENGTH FOR SALV AC PAV'T MILLING | mm % | | | | | | |
| 60F PROJECT LENGTH FOR SALV AC PAV'T MILLING | % | | | | | | |
| 60F PROJECT LENGTH FOR DIAMOND GRINDING | % | | | ····· | | | |
| 60F PROJECT LENGTH FOR PCC PAV'T REPAIR | % | | | | | | |
| OF PAV'T TIES PER METER OF LONGIT. LENGTH | EACH | | | | | | |
| DOWELS PER PATCH JOINT | EACH | | | | | | |
| VG. LENGTH OF PCC PATCH | m | | | | | | |
| 60F PROJECT LENGTH FOR CRACK & SEAT | % | | | | | | |
| 60F PROJECT LENGTH FOR BREAK & SEAT | % | | | | | | |
| OF PROJECT LENGTH FOR RUBBLIZING | % | | | | | | |
| OTAL AREA FOR ASPHALTIC BASE PATCHING | sm | | | | | | |
| OTAL AREA FOR CONCRETE BASE PATCHING | sm | | | | | | |
| OTAL AREA FOR CONCRETE WIDENING | sm | | | | | | |
| OTAL AREA FOR AC BASE COURSE WIDENING | sm | | | | | | |
| OTAL AREA FOR PCC BASE COURSE WIDENING | sm | | | | | | |
| OF PROJECT LENGTH FOR PAVEMENT REMOVAL | % | | | | | | |
| ···= [| | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| ASE LAYER: (FOR QUANTITY CALCULATIONS) - NONE E - AC STABILIZED | Г | ALT 1 | ALT 2 | ALT 3 | ALT 4 | ALT 5 | ALT 6 |
| – NONE E – AC STABILIZED – CABC F – PC STABILIZED | AYER 1 | ALT 1 | | | | | ****** |
| - NONE E - AC STABILIZED - CABC F - PC STABILIZED - OGBC #1 G - GRANULAR | AYER 2 | a z | 1 2 | . x | × * | x | |
| - NONE E - AC STABILIZED - CABC F - PC STABILIZED - OGBC #1 G - GRANULAR - OGBC #2 H - OTHER #1 | AYER 2 AYER 3 | a z | a a 2 × × | i x x (X | ××××××××××××××××××××××××××××××××××××××× | × × × × | |

ALTERNATE QUANTITIES AND COSTS

Version 3.3

07/13/98

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| | | ALTERNATI | VE #1 | ALTERNA Asphalt/base/sand | ſE #2 | ALTERNATE #3 Asphalt/base | | |
|--------------------------------------|-----------|-----------|--------------|------------------------------|--------------|------------------------------|--------------|--|
| PARAMETER | UNITS | QUANTITY | COST | QUANTITY | COST | QUANTITY | COST | |
| CONCRETE PAVEMENT (RDWY) | sm | 7,200.0 | \$129,600.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 1,800.0 | \$32,400.00 | 0.0 | \$0.00 | 0.0 | \$0. \$0. | |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 2,115.0 | \$34,897.50 | 2,368.8 | \$39,085. | |
| VIRGIN AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 528.8 | \$8,724.38 | 592.2 | | |
| RECYCLED AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$9,771. | |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| ASPHALT CEMENT | Mg | 0.0 | \$0.00 | 158.6 | \$24,586.88 | 177.7 | \$0. | |
| CRUSHED AGG. BASE COURSE | Mg | 5,658.0 | \$43,849.50 | 9,204.0 | \$71,331.00 | | \$27,537. | |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 10,239.4 | \$79,355. | |
| DPEN GRADED BASE COURSE #2 | Mg | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0. | |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| GRANULAR SUBBASE COURSE | cm | 3.987.5 | \$13,158.75 | | \$0.00 | 0.0 | \$0. | |
| CURB & GUTTER | m | 0.0 | \$0.00 | 4,152.5 | \$13,703.25 | 0.0 | \$0. | |
| YPE DF GEOTEXTILE FABRIC | sm | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| 50 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| 50mm PIPE UNDERDRAINS, UNPERFORATED | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| PRON ENDWALLS FOR UNDERDRAINS | EACH | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| ACK COATING | | 0.0 | \$0.00 | 0 | \$0.00 | 0 | \$0. | |
| AILL & RELAY AC PAVEMENT | <u>_</u> | | \$0.00 | 2,013.7 | \$2,013.66 | 2,013.7 | \$2,013. | |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | Ma | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| SPHALTIC SURFACE PATCHING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| ULVERIZING AC PAVEMENT | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| CONTINUOUS DIAMOND GRINDING | <u>sm</u> | 0.0 | \$0.00 | `0.0 | \$0.00 | 0.0 | \$0. | |
| CONCRETE PAVEMENT REPAIR | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| CRCP REINFORCEMENT | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| PAVEMENT TIES | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| OWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0. | |
| | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0. | |
| BREAK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| SPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. \$0. | |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | | |
| ONCRETE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| SPHALTIC BASE COURSE WIDENING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0. | |
| ONCRETE BASE COURSE WIDENING | <u>sm</u> | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| EMOVING PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0. | |
| ost Adjustmentsee comps | | | +3:00 | | | 0.0 | \$0.0 | |
| THER BASE #1 | Mg | 0.0 | | 0.0 | | | | |
| OTHER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | | |
| TERNATIVE TOTAL | | | \$219,008.25 | | \$155,256.66 | | \$157,762. | |

| | | ALTERNAT Existing Structure | E#4 | ALTERNAT 0 | E#5 | ALTERNATE #6 0 | | |
|--------------------------------------|-------|--------------------------------|--------|---------------|--|---|------------------|--|
| PARAMETER | UNITS | QUANTITY | COST | QUANTITY | COST | QUANTITY | COST | |
| CONCRETE PAVEMENT (RDWY) | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| CONCRETE PAVEMENT (SHOULDERS) | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| VIRGIN AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| VIRGIN AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| RECYCLED AC PAVEMENT (RDWY) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.0 | |
| RECYCLED AC PAVEMENT (SHOULDERS) | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | | |
| ASPHALT CEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CRUSHED AGG. BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| OPEN GRADED BASE COURSE #1 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | the second se | \$0.00 | |
| OPEN GRADED BASE COURSE #2 | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| BREAKER RUN | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| ASPHALTIC BASE COURSE | Mg | 0.0 | \$0.00 | 0.0 | | 0.0 | \$0.00 | |
| CONCRETE BASE COURSE | sm | 0.0 | \$0.00 | | \$0.00 | 0.0 | \$0.00 | |
| GRANULAR SUBBASE COURSE | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CURB & GUTTER | m | 0.0 | | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| 150 mm PIPE UNDERDRAINS | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| 150mm PIPE UNDERDRAINS, UNPERFORATED | m | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| APRON ENDWALLS FOR UNDERDRAINS | EACH | | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| TACK COATING | | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 | |
| MILL & RELAY AC PAVEMENT | | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| SALVAGED ASPHALTIC PAVEMENT, MILLING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| SALVAGED ASPHALTIC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| ASPHALTIC SURFACE PATCHING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| PULVERIZING AC PAVEMENT | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONTINUOUS DIAMOND GRINDING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE PAVEMENT REPAIR | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CRCP REINFORCEMENT | cm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| PAVEMENT TIES | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 | |
| DOWEL BARS | EACH | 0 | \$0.00 | 0 | \$0.00 | 0 | \$0.00 | |
| CRACK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| BREAK & SEATING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 \$0.00 | |
| RUBBLIZING CONCRETE PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | | |
| ASPHALTIC BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE BASE PATCHING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | | \$0.00 | |
| CONCRETEWIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| ASPHALTIC BASE COURSE WIDENING | Mg | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| CONCRETE BASE COURSE WIDENING | sm | 0.0 | \$0.00 | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| REMOVING PAVEMENT | sm | 0.0 | \$0.00 | 0.0 | and the second | 0.0 | \$0.00 | |
| Cost Adjustment-see comps | | | | 0.0 | \$0.00 | 0.0 | \$0.00 | |
| OTHER BASE #1 | Mg | 0.0 | | 0.0 | | | | |
| OTHER BASE #2 | Mg | 0.0 | | 0.0 | | 0.0 | | |
| LTERNATIVE TOTAL | | | \$0.00 | | \$0.00 | | \$0.00 | |

ALTERNATE MAINTENANCE Version 3.3

8600–02–01 Chippewa Falls – Comell Jim Falls – CTH R STH 178 Chippewa

MAINTENANCE COSTS: (CURRENT YEAR)

| | INCREMENT 1 | | INCREMENT 2 | | | | INCREME | NT 3 | INCREMEN | | NODENE | |
|-----------------------------------|-----------------------|------------|--------------|------------|------------------|------------|----------------------|------------|------------------|------------|--------|--|
| ALTERNATE TITLE | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM | TO YEAR | FROM YEAR | TO YEAR | | |
| YEARLY COST Asphalt/base/sand | 12 \$2,400.00 2 | 13 | \$4,970.00 | 18 | 24 \$4,970 00 | 25 | 27 \$4,970.00 | 28 | 33 \$1,250.00 | 34 | | |
| YEARLY COST Asphalt/base | \$1,250.00 | 3 | \$1,550.00 | 10 | 16 \$1.250.00 | 17 | 22 \$1,550.00 | 23 | 28 \$1,250.00 | 29 | | |
| YEARLY COST Existing Structure | \$1,250.00 | | \$1,550.00 | 10 | 16 \$1,250.00 | | <u>22</u> \$1,350.00 | 23 | 26 \$1,250.00 | 29 | | |
| YEARLY COST | | | | | | | | | | | | |
| YEARLY COST | | | | | | | | | | | | |
| YEARLY COST | | | | | | | | | | | | |

07/13/98

| | INCREME | | INCREMEN | NT 7 | INCREME | INCREMENT 8 | | MENT 9 | | |
|----------------------------------|------------------|------------|------------------|------------|------------------|-------------|------|------------|------|------|
| ALTERNATE TITLE | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM YEAR | TO YEAR | FROM | TO YEAR | FROM | то |
| YEARLY COST | 47 \$1,550.00 | 38 | 43 | 44 | 47 | 48 | | | YEAR | YEAR |
| YEARLY COST | 34 \$1,550.00 | 35 | 40 \$1,250 00 | 41 | 47 \$1 550 00 | 45 | | | | |
| YEARLY COST | 94 \$1,550.00 | 35 | 40 \$1,250.00 | 41 | 47 \$1,650.00 | 48 | | | | |
| xisting Structure YEARLY COST | | | | | | | | | | |
| 0 YEARLY COST | | | | | | | | | | |
| 0 () YEARLY COST | | | | | | | | | | |

MAINTENANCE COSTS: (CURRENT YEAR)

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ALTERNATE REHABILITATION Version 3.3

07/13/98

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

ASPHALT PAVEMENT REHABILITATION SCHEMES:

| AC1 AC2 | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders | MILLING DEPTH (mm) 25 | % OF PROJECT for SURF. PATCHING 0:0 0:0 | OVERLAY THICKNESS (mm) | MIX TYPE (HV,MV,LV) | % AC n OVERLAY MIX 8:3 | OTHER COSTS | OTHER COST DESCRIPTION |
|--------------------------|---|-----------------------------|---|---------------------------|------------------------|------------------------------|----------------|------------------------|
| AC3 AC4 AC5 AC6 | | | | 190 | | 0.8 | | |
| AC7 AC8 AC9 | RECONSTRUCT: USIN | G ORIGINAL AC LAY | ERTHICKNESSES | | | | | |

CONCRETE PAVEMENT REHABILITATION SCHEMES:

| Repair - Grind | | | | % OF PROJECT | | | |
|----------------|--------------|------------------|-------|-------------------|--------------------|-------|------------------------|
| SCHEMES | % PCC REPAIR | AVG PATCH LENGTH | | for | | OTHER | |
| PC1 | % PCC HEPAIH | in m | JOINT | PCC Base Patching | | | OTHER COST DESCRIPTION |
| PC2 | L-U | 1.6 | 32 | 0.0 | & Continuous Grind | | |
| | | 1.8 | \$2 | t D | & Continuous Grind | | |
| | | | | | & Continuous Grind | | |

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| Repair – Overlay SCHEMES % PCC REPAIR PC4 | AVG PATCH LENGTH | # DOWELS PER JOINT | % OF PROJECT for PCC Base Patching | % OF PROJECT for AC Base Patching | OVERLAY THICKNESS (mm) | MIX TYPE (HV,MV,LV) | % AC in OVERLAY MIX | OVERLAY LIMITS 1: RDWY ONLY 2: RDWY & Shoulders | OTHER COSTS | OTHER COST DESCRIPTION |
|---|------------------|-----------------------|--|---|---------------------------|------------------------|---------------------------|---|----------------|------------------------|
| PC4 0.0 PC5 130 PC6 | 1.8 1.8 | 12 12 | 50 50 | 0.0 1.0 | 0 75 | (HV,MV,LV) | OVERLAY MIX 6.0 8.0 | 2: RDWY & Shoulders | COSTS | OTHER COST DESCRIPTION |

| Mill – Repair – Overlay SCHEMES PC7 PC8 PC9 | Mill / Overlay Limits 1: RDWY ONLY 2:RDWY & Shoulders Z | | AVG PATCH LENGTH in m 1.8 | | % OF PROJECT for PCC Base Patching 2:0 | % OF PROJECT for AC Base Patching 0.0 | OVERLAY THICKNESS (mm) 75 | MIX TYPE (HV,MV,LV) | % AC in OVERLAY MIX 6:0 | OTHER COSTS |
|---|--|----------------------------------|---------------------------------|-----------------|---|--|---------------------------------|------------------------|-------------------------------|----------------|
| | | | | | | | | | | |
| SCHEME PCI0 PC11 | CONTINUOUS DIAMOND GRIND RECONSTRUCT: USING ORIGIN | ONLY AL PCC LAYER THICKNESSES | OTHER COSTS | OTHER COST DESC | | | | |] | |

ALTERNATE REHABILITATION SCENARIOS:

| | REHABILITATION COSTS | ALT. #1: | PCC | | ALT #0 | | | | | | | energia energia este esta porta (esta) | Received and relieve wheel |
|---------|-------------------------------|----------|-------|-----------------|----------|-------------------|-----------------|----------|--------------|--|----------|--|----------------------------|
| (C | OSTS ARE CURRENT YEAR) | SPACING | TYPE | | ALT. #2: | Asphalt/base/sand | | ALT. #3: | Asphalt/base | | ALT. #4: | F (1) F (1) | |
| | HABILITATION | | | CURRENT YR COST | | TYPE | CURRENT YR COST | SPACING | | CURRENT YR COST | | Existing Structure | |
| | REHABILITATION | £ | u rc4 | \$14,742.00 | | 4 AC2 | \$57,402,45 | | AC2 | | SPACING | TYPE | CURRENT YR COST |
| | HABILITATION | J | U PC5 | \$60,212.25 | | 2 AC3 | \$66,438.90 | | | | | | \$0.00 |
| | REHABILITATION | E | 0 PC7 | \$61,101,90 | | 2 4 10 | | | ACS | \$66,438.90 | | | \$0.00 |
| | | | | \$0.00 | | * 173 MB | \$70,222.41 | | AC9 | \$78,407.46 | | | \$0.00 |
| | HABILITATION | | | \$0.00 | | | \$0.00 | | | \$0.00 | | 4 | |
| EXPECTE | D LIFE OF LAST REHABILITATION | 1 | 0 | | | | \$0.00 | | | \$0.00 | | | \$0.00 |
| | TOTAL LIFE | | | | | <u>*</u> | | 14 | 2 | | | | \$0.00 |
| | | J | | | 5 | 2 | | 50 | | le l | | Se 1997 - | |
| | | | | | | | | | | Ľ | | | |

LIFE CYCLE COST ANALYSIS

Version 3.3

8600-02-01 Chippewa Falls - Cornell Jim Falls - CTH R STH 178 Chippewa

| CURRENT YEAR CONSTRUCTION YEAR DESIGN YEAR ANALYSIS PERIOD | 1998 2002 2022 50.0 | PROJECT L | T RATE (%) ENGTH (Km) BASIS (P/M) | 5.0 1.00 M | | |
|---|------------------------------|-----------|---|------------------|-------|--------|
| TERMINAL SALVAGE VALUE | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |

| PRESENT WORTH COSTS: |
|----------------------|
| |

(CURRENT YEAR)

ALT. 1 ALT. 2 ALT. 3 ALT. 4 ALT.5 ALT. 6 PCC Asphalt/base/sand Existing Structure Asphalt/base 0 0 INITIAL CONSTRUCTION COSTS \$180,178.63 \$127,730.04 \$129,791.60 \$0.00 \$0.00 \$0.00 **REHABILITATION COSTS** \$23,173.16 \$48,271.80 \$49,326.35 \$0.00 \$0.00 \$0.00 MAINTENANCE COSTS \$5,916.56 \$3,441.68 \$3,441.68 \$0.00 \$0.00 \$0.00 TERMINAL SALVAGE VALE \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 REHABILITATION SALVAGE VALUE \$0.00 (\$1,292.49)(\$1,443.14) \$0.00 \$0.00 \$0.00 TOTAL FACILITY COSTS \$209,268.35 \$178,151.02 \$181,116.49 \$0.00 \$0.00 \$0.00

EQUIVALENT UNIFORM ANNUAL COSTS:

(OVER ANALYSIS PERIOD)

| | ALT. 1 | ALT. 2 | ALT. 3 | ALT. 4 | ALT.5 | ALT. 6 |
|------------------------------|-------------|-------------------|--------------|--------------------|--------|--------|
| | | Asphalt/base/sand | Asphalt/base | Existing Structure | 0 | |
| INITIAL CONSTRUCTION COSTS | \$9,869.60 | \$6,996.63 | | | \$0.00 | \$0.0 |
| REHABILITATION COSTS | \$1,269.35 | \$2,644.17 | \$2,701.94 | | | |
| MAINTENANCE COSTS | \$324.09 | \$188.52 | \$188.52 | | \$0.00 | \$0.00 |
| TERMINAL SALVAGE VALE | \$0.00 | \$0.00 | | +0.00 | | \$0.00 |
| REHABILITATION SALVAGE VALUE | \$0.00 | (\$70.80) | \$0.00 | +0.00 | \$0.00 | \$0.00 |
| | | (\$10.00) | (\$79.03) | \$0.00 | \$0.00 | \$0.00 |
| | | | | | | |
| TOTAL FACILITY COSTS | \$11,463.04 | \$9,758.53 | \$9,920.97 | \$0.00 | \$0.00 | \$0.00 |

07/13/98

| 7/14/98WISCONSIN DEPARTMENT06:26:33PAVEMENT INDEXBROWSE OF CURRENT | FILE SYSTEM |
|--|---|
| District 6 County Name CHIPPEWA | County Number 9 Highway 178N |
| 011G + 0.000 CTH. Y 012K + 0.000 182ND. ST. 014G + 0.000 CTH Y INT | a*Current* *PDI**IRI*ToSurfaceSurveyRP + DistanceYrTyYrNo.012K +0.000851962897014G +0.0008519649971.40015 +0.0008119657972.38015 +0.9808119676973.08017 +0.0008719634972.75018 +0.6808819631972.46020 +0.0008419650972.86022 +0.0008819641972.97023 +0.0008329675973.58 |
| Surf Type 1=ACPM/FB,2=BRM, 3=ACPM/RB, 4=3 | |

SELECT DATA TO VIEW, OR PRESS ENTER FOR MORE ENTER TO CONTINUEPF3 OR PF15 TO BROWSE MENUPA2 TO CANCEPF2 OR PF14 TO PRIMARY MENUPF12 OR PF24 TO LOGOFF CICSPA2 TO CANCE

| | ENT OF TRANSPORTATION IPFMBC |
|---------------------------------------|---|
| | DEX FILE SYSTEM |
| BROWSE OF CURRE | NT PDI & PSI VALUES |
| District 6 County Name CHIPPEWA | County Number 9 Highway 178N |
| Enter S in Opt Field to View Section | Data *Current* *PDI* *IRI* |
| From | To Surface Survey Survey |
| pt RP + Distance From Feature | RP + Distance Yr Ty Yr No. Yr mm/m |
| 022 + 0.000 190TH AVE. | 023 + 0.000 83 2 96 75 97 3.58 |
| 023 + 0.000 CTH R INT | 024 + 0.000 87 1 96 38 97 2.60 |
| 024 + 0.000 CTH ZZ INT | 024 + 1.250 81 1 96 24 97 2.45 |
| 024 + 1.250 SECTION 25 & 24 | 027 + 0.000 84 1 96 66 97 2.57 |
| 027 + 0.000 STH 64E | 499E + 0.000 |
| + | + |
| + | + |
| + | + |
| + . | + |
| + | + |
| Surf Type 1=ACPM/FB,2=BRM, 3=ACPM/RB, | 4=JRCP, 5=JPCP w/o d, 6=CRCP, 8=JPCP /d |
| | |
| NO MORE SECTIONS FOR COUNTY & HIGHWAY | |
| ENTER TO CONTINUE PF3 O | R PF15 TO BROWSE MENU PA2 TO CANCE |

Date: July 13, 1998

To: File

From: Randy W. Luedtke, P.E. District #6 Pavement Design Engineer

Subject: Traffic Forecast projection revisions Project 8600-02-01

This project has been in and out of the six year program for the last 5-10 years. There has been no recent specific traffic forecast done for this segment. For structural design purposes, I chose to use a construction year ADT of 2000 and a 20 year ADT of 2400. The truck percentage was rounded to 8%. The following two forecasts done in 1992 and 1995 give volumes for the roadway but are outdated.

TRAFFIC FORECAST

PROJECT ID:8600-02-71COUNTY:ChippewaROUTE:STH 178LOCATION:Int. w/ CTH X to the second second

| 1 : | Int. | w/ | СЦН | Y | to | Int. | w/ | STH 6 | 4 |
|------------|------|----|-----|---|----|------|----|-------|---|
|------------|------|----|-----|---|----|------|----|-------|---|



veloped by Keith Wendt, Traffic Forecasting and Analysis Section 14-Sep-92

| PROJECT ID: 8191-01-01 COUNTY: Chippewa ROUTE: STH 64 LOCATION: STH 64: CTH R to STH27 DISTRICT: 6 | KEY *000* 1993 AD1 -000- 1999 AD1 (000) 2009 AD1 000 2019 AD1 | $ \begin{array}{llllllllllllllllllllllllllllllllllll$ |
|---|---|--|
| N $64 -\frac{-700-}{(775)} 178$ $64 -\frac{-200-}{(225)} 178$ 250 | 64 | See Detail *450* -900- (1000) 1100 |
| Detail *990* -1150- (1350) 1550 (64) R | ZZ -400- (450) 475 | 178 -2450- (2900) 3350 *1700* -1950- |
| *580* -600- (650) 700 | -200- (200) 225 *1500* -1750- (2100) 2500 | (2350) 2750 (27) |
| DESIGN VALUESTRUCK CLASSNotes on the Forecast:K10011.5TRUCK1. Historic and projected traffic wK5012.3TYPE $%$ ADTAdjusted AADT. Pre – 1990 wK3012.92D3.6indicated Axle – Adjustment HP(PHV)16.73AX1.42. This forecast assumes that no sT(DHV)6.22S1+2S20.7generators will be developed inT(PHV)3.53-S22.0the forecast period.D60/40Dbl-Btm0.03. STH 64 has an axle – adjustmK8(ADT)NATOTAL7.7in Factor Group 4, indicating nT(A8HV)NATOTAL7.7fluctuation. | volumes represent Axle – counts are factored using Factors (A – AF). signficant new traffic the project area during ent factor of .93 and is | REFERENCES 1. "Wisconsin Highway Traffic", available coverage counts, 1975 – 1993. 2. "Official Poulation Estimates, Demographic Services Center, DOA. |

CONCEPT DEFINITION REPORT

Date: 07/17/96

To: Michael A. Cass (P.E.) From: District 6

- Design ID: 8600-02-01 I. Related ID(s): 8600-02-71(Const) Highway No. or Local Road Name: STH 178 8600-02-21 (R/W) Title: CHIPPEWA FALLS - CORNELL ROAD County: CHIPPEWA Length: 7.4 Miles 11.9 km Functional Class: Major Collector Current ADT: 1650 (1993) LOCATION: CTH Y - CTH R
- II. A. Roadway Conditions: Pavement: Type: AC Width: 22 Year: 1981 PSI: 2.69 (1993) PDI: 30 (1994) Shoulder: Type: Gravel Width: 2 Accident Rate: 480 Year: 1995 Substandard Alignment: Horizontal: Yes Vertical: Yes
 - B. Structure: (may be continued on back side) Type: DECK GIRDER Lengtn: 00.5 10, ____ Year Constructed: 1942 Length: 86.5 ft, 26.4 m Bridge Number: B-09-0682 SR: 80.5 Clear Roadway Width: 27.6 RS: 89.4

JUSTIFICATION: Accident rate is 480 vs State ave of 222 because of narrow shoulders, sharp horiz curvature and short vertical and horiz sight distance. There are many power poles and trees in clear zone.

- III. PROPOSED IMPROVEMENT: Grade, Base, Asphaltic Surface to C3 standards with a 24 ft surface on a 36 ft roadway with a 30 ft clear zone.
 - A. Environmental documentation type: III ER
 - B. Improvement Type: RECST PMSID: 98060020201
 - C. Cost: \$ 3,850,000 Program Year: 2002 Program: 3334

D. Local Participation: \$ No Access Control: No

DISTRICT 6 APPROVAL Project Supervisor

Planning Supervisor

Concept Definition Report Project: 8600-02-01

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Page: 1 of 2 Date: 07/17/96 CC: Gerry Feiler - Rm 951, Len Stanek - Rm 651, Bureau of Environment - Rm 451

Gene Hoelker-FHWA District 6 Geographic Information System

