

Intersection Control Evaluation Report

STH 23 & Wisconsin American Drive

Project ID 1440-15-01
Fond du Lac County, WI

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Intersection Control Evaluation

Factors to Analyze (Intersection of STH 23 and Wisconsin American Drive)

PROJECT DESCRIPTION

WisDOT is planning a roadway improvement project (I.D. 1440-15-01) for State Trunk Highway (STH) 23 in Fond du Lac County. This project is planned for construction starting in 2015 and includes the intersection of STH 23 and Wisconsin American Drive. The existing intersection of STH 23 and Wisconsin American Drive is located approximately 800 feet east of the northbound USH 151 ramp terminal with STH 23.

Currently, STH 23 is a four-lane divided highway at this intersection with a 130-foot left-turn (westbound) and 130-foot right turn (eastbound) lane onto Wisconsin American Drive. Wisconsin American Drive is a stop-controlled approach from the south which serves as the sole access point for an isolated residential and commercial area. The posted speed limit on STH 23 is 45 mph east of the intersection and 35 mph west of the intersection; Wisconsin American Drive is posted at 25 mph. The proposed project design speed on STH 23 is 50 mph.

This report will analyze and contrast three potential intersection reconfiguration alternatives in accordance with the criteria outlined in FDM chapter 11-25-3 (project development). The intersection alternatives to be analyzed are as follows:

1. No-build, with no change to existing geometry, using maintaining stop control on Wisconsin American Drive.
2. Reconstructed intersection with two travel lanes in each direction on STH 23, using traffic signal control.
3. Reconstructed roundabout-control intersection.

A project location map is included in **Appendix A**.

| | ALTERNATIVE 1 TWO WAY STOP CONTROL | ALTERNATIVE 2 TRAFFIC SIGNAL | ALTERNATIVE 3 ROUNDBOUT |
|------------------------------|--|--|---|
| SAFETY CONSIDERATIONS | <p><u>Existing Crash Patterns</u> A crash report for the project area including this intersection was completed by KL Engineering in 2007. Crash data for this intersection was updated to include crashes that occurred through 2011. Crashes that occurred at this intersection between 2003 and 2011 were evaluated for this report.</p> <p>During this time period, there were twelve non-deer-related crashes reported at this intersection, eight of which occurred in the past six years. This represents an average of approximately 1.3 crashes per year. The resulting crash rate of approximately 0.3 crashes per million entering vehicles (MEV) is below the threshold of concern for a standard intersection (1.5 crashes per MEV).</p> <p>Three of the crashes in the past six years have been angle crashes with a vehicle from Wisconsin American Drive failing to yield the right-of-way to a vehicle on STH 23. Three of the remaining crashes were rear-end crashes. There was one run-off-the-road crash and one crash involving a westbound-to-southbound left-turning vehicle failing to yield the right-of-way to an eastbound vehicle.</p> <p>A collision diagram is included in Appendix B.</p> <p><u>Alternative 1 Analysis</u> This intersection control alternative does not improve upon the existing conditions, so future crash patterns are expected to follow the existing crash pattern. Increased traffic volume will likely result in increased crash frequency.</p> | <p>This intersection control alternative includes reconstruction of the existing condition to a channelized intersection with traffic signal control.</p> <p>The reconstruction of the intersection to current standards under signal control will likely result in a generally safer intersection; however, signalized intersections on high-speed roadways have been known to create an environment for more serious crashes.</p> <p>High speed rural signalized intersections have been shown to experience more serious crashes between drivers having a false sense of security when crossing the intersection obeying a green signal indication, and other drivers deliberately or inattentively disobey signal indications. These crashes result in serious injury given the high rates of speed.</p> <p>Additionally, signalizing intersections can often increase the number of rear-end collisions from vehicles slowing down to a stop compared to a previously free-flowing condition.</p> <p>There are safety features that can be implemented to decrease the potential for high-speed crashes. These features may include advance warning signs, high-speed vehicle detection and careful phasing/timing design for minimizing the chance for crashes to occur.</p> <p>A typical signalized T-intersection has 9 conflict points.</p> | <p>This intersection control alternative includes reconstruction of the existing intersection to a roundabout.</p> <p>It is unlikely that a roundabout would result in a reduction in the number of crashes given the low existing rate. However, roundabout crashes are typically less severe than those occurring at other types of intersections due to lower vehicle operating speeds and smaller impact angles.</p> <p>When compared to a two-way stop-controlled (TWSC) or a signalized intersection, roundabouts reduce the number of conflict points for a T-intersection to 6 (3 diverge and 3 merge, 0 crossing) and reduce the opportunity for high speed and angle crashes.</p> |

Intersection Control Evaluation

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TRAFFIC VOLUMES & OPERATIONAL ANALYSIS

ALTERNATIVE 1 TWO WAY STOP CONTROL

Traffic Volume Background

Hourly traffic counts on STH 23 just east of this intersection show annual average daily traffic (AADT) of 10,800 vehicles per day (vpd) in a 2012. Traffic volumes are projected to reach 13,200 vpd in the construction year (2015), and 17,600 vpd in the design year (2035).

A design year (2035) projection from turning movement count forecasts indicated an AADT on Wisconsin American Drive of 4,550 vpd.

The highest volume of traffic at the intersection occurs during the PM peak hour with the total intersection traffic of approximately 1,865 in the AM and 2,050 in the PM peak hour. The PM peak hour approach volumes projected for the design year (2035) is approximately:

- 1,010 vehicles eastbound STH 23
- 710 vehicles westbound on STH 23
- 330 vehicles northbound on Wisconsin American Drive

In general terms, the vast majority of total traffic using the intersection is through volume on the mainline, with low turning movement volume to or from the side road. STH 23 through volume consists of 76% to 85% of peak hour traffic. Traffic volume on Wisconsin American Drive accounts for 3% to 16% of peak hour traffic. The remaining 8% to 12% is comprised of turning traffic off STH 23.

Truck volume accounts for approximately 12% of total traffic on STH 23 and 2% on Wisconsin American Drive.

Alternative 1 Analysis

A highway capacity analysis using Synchro Software was completed to model this alternative under existing conditions and stop control for the 2015 and 2035 AM and PM peak hour periods.

The Wisconsin American Drive (NB) approach to this intersection would be anticipated to operate at LOS C during the AM peak and LOS F during the PM peak with existing conditions under 2015 projected traffic volumes. The northbound queue on Wisconsin American Drive during the PM peak hour is expected to be approximately 200 feet. The westbound left turn from STH 23 to Wisconsin American Drive is expected to operate at LOS A during both peak hours. See below for a summary of results.

2015 Highway Capacity Results

| Existing Conditions Stop Control | Delay Per Vehicle/LOS (Seconds) | |
|-------------------------------------|---------------------------------|-----------|
| | 2015 AM | 2015 PM |
| NB Approach | 21/C | 79/F |
| EB Approach | Free Flow | Free Flow |
| WB LT | 9/A | 10/A |
| Intersection | 1/A | 12/B |

ALTERNATIVE 2 TRAFFIC SIGNAL

A traffic signal warrant analysis check (70% volume criteria) was completed for the intersection of STH 23 and Wisconsin American Drive using 2012 traffic volumes. Warrant 1A (eight-hour vehicular volume) & 2 (four-hour vehicular volume) were met using 0 percent right-turns. Refer to **Appendix D** for traffic signal warrant analysis results.

Synchro Software was used to model this alternative, the reconstruction of the intersection to current standards with traffic signal control for the design year (2035) peak hour periods. The modeling assumed two through travel lanes in each direction on STH 23, a 350-foot eastbound right-turn lane, a 450-foot left-turn lane, and two approach lanes on Wisconsin American Drive. The signal control assumed protected/permitted (flashing yellow arrow) phasing for the westbound left turns from STH 23.

The USH 151 northbound ramp intersection is located approximately 800-feet west of the Wisconsin American Drive intersection, while the southbound ramp intersection is approximately 500-feet west of the northbound ramp. These intersections are currently signalized and operated together using diamond interchange type traffic signal phasing. The modeling indicated that traffic progression along STH 23 would benefit from operating the signal at Wisconsin American Drive as part of a coordinated network including the interchange ramps. All results shown in this report are from modeling in coordination with the USH 151 interchange.

The tables below summarize the intersection modeling results in 2035. The HCM results from Synchro software indicate that the intersection and all approaches would operate at a LOS C or better during both peak hours in the design year (2035). No queuing issues are anticipated. See below for a summary of results.

2035 Highway Capacity Results

| Traffic Signal | Delay Per Vehicle/LOS (Seconds) HCM | |
|----------------|-------------------------------------|---------|
| | 2035 AM | 2035 PM |
| NB Left | 21/C | 20/B |
| NB Right | 19/B | 14/B |
| EB Approach | 1/A | 8/A |
| WB Thru | 4/A | 9/A |
| WB LT | 3/A | 7/A |
| Intersection | 3/A | 10/A |

2035 Synchro Queues

| Traffic Signal | 95 th % Queue Length (Feet) Synchro | |
|----------------|--|---------|
| | 2035 AM | 2035 PM |
| NB Left | 28 | 124 |
| NB Right | 25 | 25 |
| EB Approach | 32 | 152 |
| WB Thru | 115 | 109 |
| WB LT | 25 | 25 |

This alternative can provide excess capacity to deal with fluctuations in future traffic volumes.

Refer to **Appendix E** for modeling output data for this alternative.

ALTERNATIVE 3 ROUNDBOUT

RODEL roundabout analysis software was used to model this alternative, the reconstruction of the intersection as a dual-lane roundabout for the design year (2035) peak hour periods. The modeling assumed two through travel lanes in each direction on STH 23 and a single approach lane on Wisconsin American Drive.

The results indicate the intersection will maintain acceptable operations for all approaches during both peak hours in the design year (2035). This alternative has higher average overall intersection delay when compared to the signalized alternative. This is due to the roundabout creating an environment where all traffic has to slow to enter the intersection. No queuing issues are anticipated.

Two additional factors regarding the traffic operations under this alternative were considered:

- Interaction with the signalized USH 151 ramp intersections
- Imbalance of movements at the roundabout

The interaction with the signalized USH 151 ramps is expected to create a platoon type arrival pattern at the eastbound approach to the roundabout. The distance between the northbound ramp and Wisconsin American Drive is 800 feet (1,350 feet from the southbound ramp), which is a short distance that won't allow for significant dispersion of traffic.

The imbalance of traffic volume at the roundabout is also a concern. This location has a low percentage of traffic turning left through the intersection. The potential for high entry speeds and failing to yield may result when through traffic becomes accustomed to rarely yielding to certain movements. This issue may be exacerbated by the platoon arrival of traffic from the USH 151 traffic signal.

The tables below summarize the intersection modeling results in 2035. The RODEL results indicate that the intersection and all approaches would operate at a LOS B or better during both peak hours in the design year (2035). No queuing issues were indicated. RODEL results do not account for any additional delay and queuing from the issues noted above. See below for a summary of results.

2035 RODEL Capacity Results

| Roundabout | Delay Per Vehicle/LOS (Seconds) | |
|--------------|---------------------------------|---------|
| | 2035 AM | 2035 PM |
| NB Approach | 13/B | 17/B |
| EB Approach | 16/B | 17/B |
| WB Approach | 17/B | 17/B |
| Intersection | 17/B | 18/B |

2035 RODEL Queues

| Roundabout | Queue Length (Feet) | |
|-------------|---------------------|---------|
| | 2035 AM | 2035 PM |
| NB Approach | 50 | 75 |
| EB Approach | 25 | 75 |
| WB Approach | 75 | 50 |

Intersection Control Evaluation

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| | ALTERNATIVE 1 TWO WAY STOP CONTROL | ALTERNATIVE 2 TRAFFIC SIGNAL | ALTERNATIVE 3 ROUNDBOUT | | | | | | | | | | | | | | | | | | |
|--|---|--|--|--------------|--------------|---------|-------------|-------------|------|-------------|-------------|-----------|-----------|-------|------|------|--------------|---|------|--|--|
| TRAFFIC VOLUMES & OPERATIONAL ANALYSIS (CONTINUED) | 2015 Synchro Queues <table><tr><th>Existing Conditions</th><th colspan="2">95th % Queue Length (Feet)</th></tr><tr><th>Stop Control</th><th>2015 AM</th><th>2015 PM</th></tr><tr><td>NB Approach</td><td>25</td><td>200</td></tr><tr><td>EB Approach</td><td>0</td><td>0</td></tr><tr><td>WB LT</td><td>0</td><td>0</td></tr></table> | Existing Conditions | 95 th % Queue Length (Feet) | | Stop Control | 2015 AM | 2015 PM | NB Approach | 25 | 200 | EB Approach | 0 | 0 | WB LT | 0 | 0 | | This alternative will provide excess capacity to deal with fluctuations in future traffic volumes. Refer to Appendix E for modeling output data for this alternative. | | | |
| | Existing Conditions | 95 th % Queue Length (Feet) | | | | | | | | | | | | | | | | | | | |
| | Stop Control | 2015 AM | 2015 PM | | | | | | | | | | | | | | | | | | |
| | NB Approach | 25 | 200 | | | | | | | | | | | | | | | | | | |
| | EB Approach | 0 | 0 | | | | | | | | | | | | | | | | | | |
| | WB LT | 0 | 0 | | | | | | | | | | | | | | | | | | |
| | 2035 Highway Capacity Results <table><tr><th>No-Build Conditions</th><th colspan="2">Delay Per Vehicle/LOS (Seconds)</th></tr><tr><th>Stop Control</th><th>2035 AM</th><th>2035 PM</th></tr><tr><td>NB Approach</td><td>33/D</td><td>398/F</td></tr><tr><td>EB Approach</td><td>Free Flow</td><td>Free Flow</td></tr><tr><td>WB LT</td><td>10/B</td><td>11/B</td></tr><tr><td>Intersection</td><td>1/A</td><td>63/F</td></tr></table> | No-Build Conditions | Delay Per Vehicle/LOS (Seconds) | | Stop Control | 2035 AM | 2035 PM | NB Approach | 33/D | 398/F | EB Approach | Free Flow | Free Flow | WB LT | 10/B | 11/B | Intersection | 1/A | 63/F | | |
| | No-Build Conditions | Delay Per Vehicle/LOS (Seconds) | | | | | | | | | | | | | | | | | | | |
| | Stop Control | 2035 AM | 2035 PM | | | | | | | | | | | | | | | | | | |
| | NB Approach | 33/D | 398/F | | | | | | | | | | | | | | | | | | |
| EB Approach | Free Flow | Free Flow | | | | | | | | | | | | | | | | | | | |
| WB LT | 10/B | 11/B | | | | | | | | | | | | | | | | | | | |
| Intersection | 1/A | 63/F | | | | | | | | | | | | | | | | | | | |
| 2035 Synchro Queues <table><tr><th>No-Build Conditions</th><th colspan="2">95th % Queue Length (Feet)</th></tr><tr><th>Stop Control</th><th>2035 AM</th><th>2035 PM</th></tr><tr><td>NB Approach</td><td>25</td><td>535</td></tr><tr><td>EB Approach</td><td>0</td><td>0</td></tr><tr><td>WB LT</td><td>0</td><td>0</td></tr></table> | No-Build Conditions | 95 th % Queue Length (Feet) | | Stop Control | 2035 AM | 2035 PM | NB Approach | 25 | 535 | EB Approach | 0 | 0 | WB LT | 0 | 0 | | | | | | |
| No-Build Conditions | 95 th % Queue Length (Feet) | | | | | | | | | | | | | | | | | | | | |
| Stop Control | 2035 AM | 2035 PM | | | | | | | | | | | | | | | | | | | |
| NB Approach | 25 | 535 | | | | | | | | | | | | | | | | | | | |
| EB Approach | 0 | 0 | | | | | | | | | | | | | | | | | | | |
| WB LT | 0 | 0 | | | | | | | | | | | | | | | | | | | |
| In 2035, the modeling indicated that the Wisconsin American Drive approach is expected to operate at LOS D during the AM peak and LOS F during the PM peak hour. Queues over 500 feet would be expected on the northbound approach during the PM hour. This alternative does not maintain an acceptable level of service for Wisconsin American Drive traffic beyond 2015. | | | | | | | | | | | | | | | | | | | | | |
| Refer to Appendix E for modeling output data for this alternative. | | | | | | | | | | | | | | | | | | | | | |
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Intersection Control Evaluation

Factors to Analyze (Intersection of STH 23 and Wisconsin American Drive)

| | ALTERNATIVE 1 TWO WAY STOP CONTROL | ALTERNATIVE 2 TRAFFIC SIGNAL | ALTERNATIVE 3 ROUNDBOUT |
|-------------------------|--|---|--|
| CONSTRUCTION COSTS | <p><u>General Comments</u> The costs listed for each alternative are specific to the limits of work required for the alternative. The reconstruction areas covered by the estimated costs are measured from the point where the alignment of either alternative deviated from the planned typical section of the STH 23 corridor reconstruction. Refer to the sketch of alternatives in Appendix G for a graphical depiction of the areas represented in the estimates.</p> | <p>The total construction cost for this alternative includes an estimate of items required for grading, pavement, and incidentals to construct an intersection to current standards under signal control.</p> <p>A total construction cost of \$1,750,000 includes a 15% contingency and does not include right-of-way or utility costs. This estimate assumes a full reconstruction within the footprint of the intersection expansion of the STH 23 roadway.</p> <p>Refer to Appendix F for additional estimate detail.</p> | <p>The total construction cost for this alternative includes an estimate of items required for grading, pavement, and incidentals to construct an intersection to current standards under roundabout control.</p> <p>A total construction cost of \$1,250,000 includes a 15% contingency and does not include right-of-way or utility costs. This estimate assumes a full reconstruction within the footprint of the intersection expansion of the STH 23 roadway.</p> <p>Refer to Appendix F for additional estimate detail.</p> |
| RIGHT-OF-WAY IMPACTS | <p><u>General Comments</u> The right-of-way impacts listed for each alternative are specific to the limits of work required for the alternative. The reconstruction areas covered by the estimated impacts are measured from the point where the alignment of either alternative deviated from the planned typical section of the STH 23 corridor reconstruction. Refer to the sketch of alternatives in Appendix G for right-of-way impacts.</p> | <p>An estimate for right-of-way acquisition required for this alternative assumes an additional 12 feet of right-of-way from the parcel on the north side of STH 23 for the length of the westbound left-turn lane. An additional corner of right-of-way is required for the addition of the eastbound right-turn lane. There will be additional right-of-way required for the overall STH 23 corridor expansion. This amount will be determined with higher precision as design progresses. A total of 2.37 Acres of new right-of-way will be required to construct an intersection to current standards under signal control. No relocations are needed with this alternative.</p> | <p>An estimate for right-of-way acquisition required for this alternative includes a larger area of right-of-way from the parcel on the north side of STH 23 to accommodate the offset of the circulatory roadway. There will be additional right-of-way required for the overall STH 23 corridor expansion. This amount will be determined with higher precision as design progresses. A total of 2.71 Acres of new right-of-way will be required to construct an intersection to current standards under roundabout control. No relocations are needed with this alternative.</p> |

Intersection Control Evaluation

Factors to Analyze (Intersection of STH 23 and Wisconsin American Drive)

| | ALTERNATIVE 1 TWO WAY STOP CONTROL | ALTERNATIVE 2 TRAFFIC SIGNAL | ALTERNATIVE 3 ROUNDBOUT |
|---|---------------------------------------|---|--|
| PRACTICAL FEASIBILITY | N/A | <p>This intersection alternative may be considered as feasible for the following reasons:</p> <ul style="list-style-type: none"> The intersections are in proximity to be coordinated with the traffic signals at USH 151 during peak periods, and may run independently during off peak periods. Does not create major impediments for use as an OSOW use. This alternative can be built under traffic without requiring significant cost or impacts to traffic. | <p>This intersection alternative may be considered as feasible for the following reasons:</p> <ul style="list-style-type: none"> Vehicles operate at lower speeds through roundabouts, providing for safer pedestrian and bicycle access. <p>This intersection alternative may be considered as impractical for the following reasons:</p> <ul style="list-style-type: none"> This alternative would require significantly more complex and costly construction staging methods to build under traffic. |
| OPERATIONS & MAINTENANCE COSTS | N/A | <p>In addition to periodic pavement rehabilitation this alternative will require continued operation and maintenance costs incurred for maintenance of the traffic signal and for energy cost. A summary of probable energy usage for the traffic signal is as follows:</p> <p><u>Traffic signal (LED)</u> 11 – 16 kWh LED signal heads 176 kWh/month = 2,112 kWh/year</p> <p>Yearly Cost @ \$0.11/kWh = \$232/year</p> <p><u>Street Lighting</u> 6 – 250 Watt HPS Fixtures: 114 kWh/month/fixture = 684 kWh/month = 8,208 kWh/year</p> <p>Yearly Cost @ \$0.11/kWh= \$903/year</p> <p>Total Energy Cost = \$232 + \$903 = \$1,135/year</p> <p>There would also be an additional cost of maintenance for of a traffic signal and repairing knock-downs and equipment failures. This cost will be variable and difficult to estimate accurately.</p> <p><u>Traffic Signal Timing</u> – Traffic signals will require ongoing periodic evaluation and maintenance to maintain efficient traffic flow and to keep current with updated equipment needs. The cost for this is not easily estimated; however a long term commitment to engineering and maintenance will be required for any new traffic signal.</p> | <p>In addition to periodic pavement rehabilitation this alternative will require unique operation and maintenance costs incurred for maintenance of 16 new street lights and for energy cost. A summary of probable energy usage for the street lighting is as follows:</p> <p>10 – 250 Watt HPS Fixtures: 114 kWh/month/fixture = 1,140 kWh/month = 13,680 kWh/year</p> <p>Yearly Cost @ \$0.11/kWh= \$1505/year</p> <p>There would also be an additional cost of maintenance for the street lighting for repairing knock-downs and equipment failures. This cost will be variable and difficult to estimate accurately. Additional maintenance concerns with this alternative should be considered given the following roadway design features specific to this alternative.</p> <p><u>Drainage</u> – It is reasonable to expect that a considerable amount of curb and gutter will require a storm sewer drainage system. Any drainage system will require period cleaning. A specific cost is not easily attributed without determining the exact design of the roundabout.</p> <p><u>Central Island Landscaping</u> – It is reasonable to expect that a greenscaped central island will require routine maintenance by the local authority. A specific cost is not easily attributed without determining the exact design of the roundabout and landscaping items.</p> <p><u>Pavement Marking</u> – Roundabouts will generally require more pavement marking than traditional intersections. A specific cost is not easily attributed without determining the exact design of the roundabout.</p> |

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| | ALTERNATIVE 1 TWO WAY STOP CONTROL | ALTERNATIVE 2 TRAFFIC SIGNAL | ALTERNATIVE 3 ROUNDBOUT |
|--------------------------------------|--|--|--|
| ENVIRONMENTAL IMPACTS | N/A | There are no environmental impacts identified for this alternative. | There are no environmental impacts identified for this alternative. |
| PEDESTRIAN/BICYCLE ACCOMMODATIONS | <p>Complete Streets (Trans 75) will apply to this project.</p> <p>The corridor expansion project will include a pedestrian and bicycle path along the north side of STH 23.</p> | <p>This alternative will include curb cuts for future cross walks and traversable channelizing islands. The signal could include pedestrian signals if sidewalks are included in the future.</p> <p>This alternative will provide gaps for pedestrians crossing STH 23 and Wisconsin American Drive. Bicycles can use the shoulder or the off-road path.</p> | <p>This alternative will include curb cuts for future cross walks, paved median crossings and off street paths around the roundabout.</p> <p>This alternative will provide gaps for pedestrians crossing STH 23 and Wisconsin American Drive. Bicycles can use the off road path or may travel through the roundabout.</p> |
| OSOW VEHICLES | <p><u>General Information</u></p> <p>STH 23 is a designated long truck route. STH 23 is also considered a primary route for Oversize/Overweight (OSOW) vehicles in the Northeast Region.</p> | <p>This alternative would require removing or raising monotube signal mast arms for loads in excess of 18 feet in height. If turning movements are required, the raised curb may be a barrier for left-turns.</p> | <p>Specific features including mountable curb, increased truck apron size and large offsets to light poles can be designed if it is determined that OSOW vehicles will need to be accommodated.</p> |

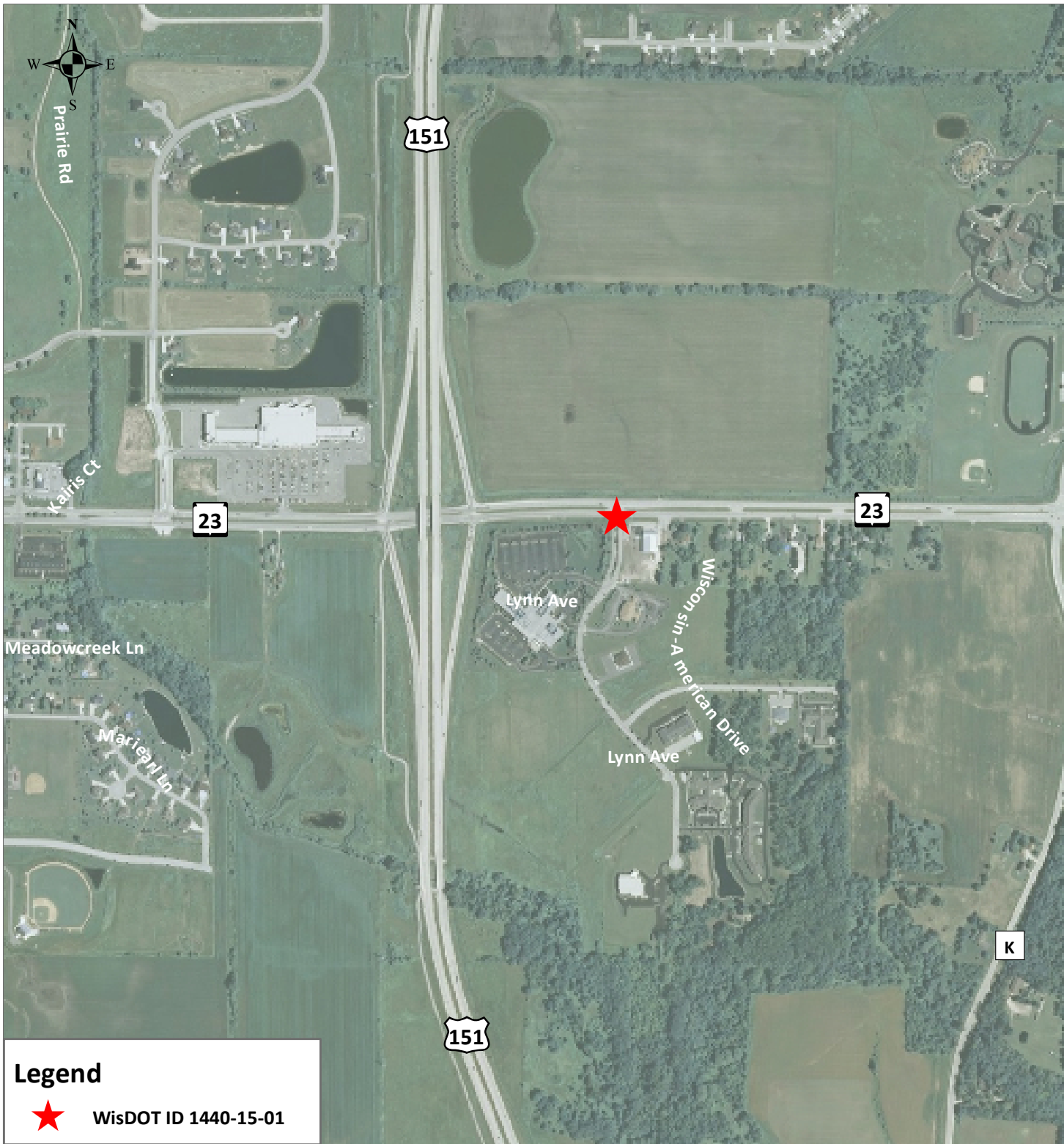
Intersection Control Evaluation

Factors to Analyze (Intersection of STH 23 and Wisconsin American Drive)

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|-----------------------|--|---|--|
| RECOMMENDATION | <p>Alternative 1: The no-build alternative is not recommended because it does not include safety and operational improvements.</p> | <p>Alternative 2: The signalized alternative would include an intersection design which includes desirable geometric features such as long stopping and intersection sight lines and channelized turn lanes.</p> <p>This alternative has the following preferred criteria when compared to the remaining alternatives:</p> <ul style="list-style-type: none"> • Lower delay per vehicle without any major queuing issues. • Practical aspect of constructability while maintaining traffic movements. • Lower amount of right-of-way required • Lower operations and maintenance cost | <p>Alternative 3: This alternative would have the lowest potential for crashes, as well as lower crash severity; in addition to having a lower construction cost than the signalized alternative.</p> <p>The Wisconsin Department of Transportation recommends constructing the intersection as a dual-lane roundabout for the following reasons:</p> <ul style="list-style-type: none"> • Lower cost • A roundabout will fit in with the long range plans for STH 23 and result in continuous travel along STH 23 between USH 151 and Plymouth to the east. |

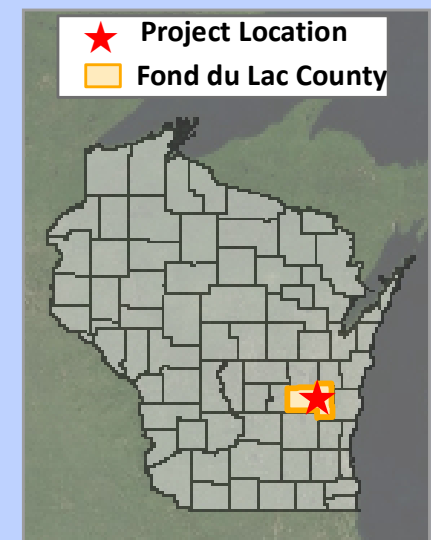
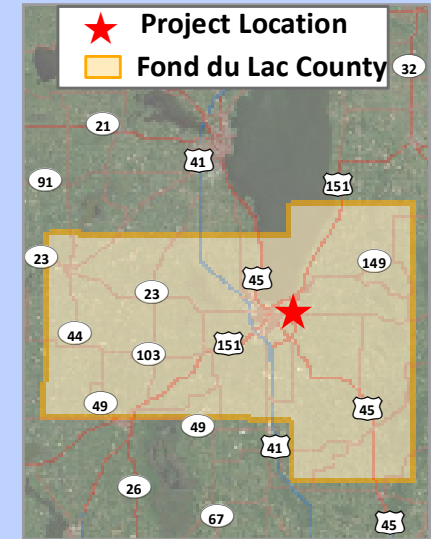
Appendix A

Project Location Map



Project Location Map

WisDOT ID 1440-15-01
USH 151 Interchange - Taft Road
Wisconsin-American Drive Intersection
STH 23
Fond du Lac County

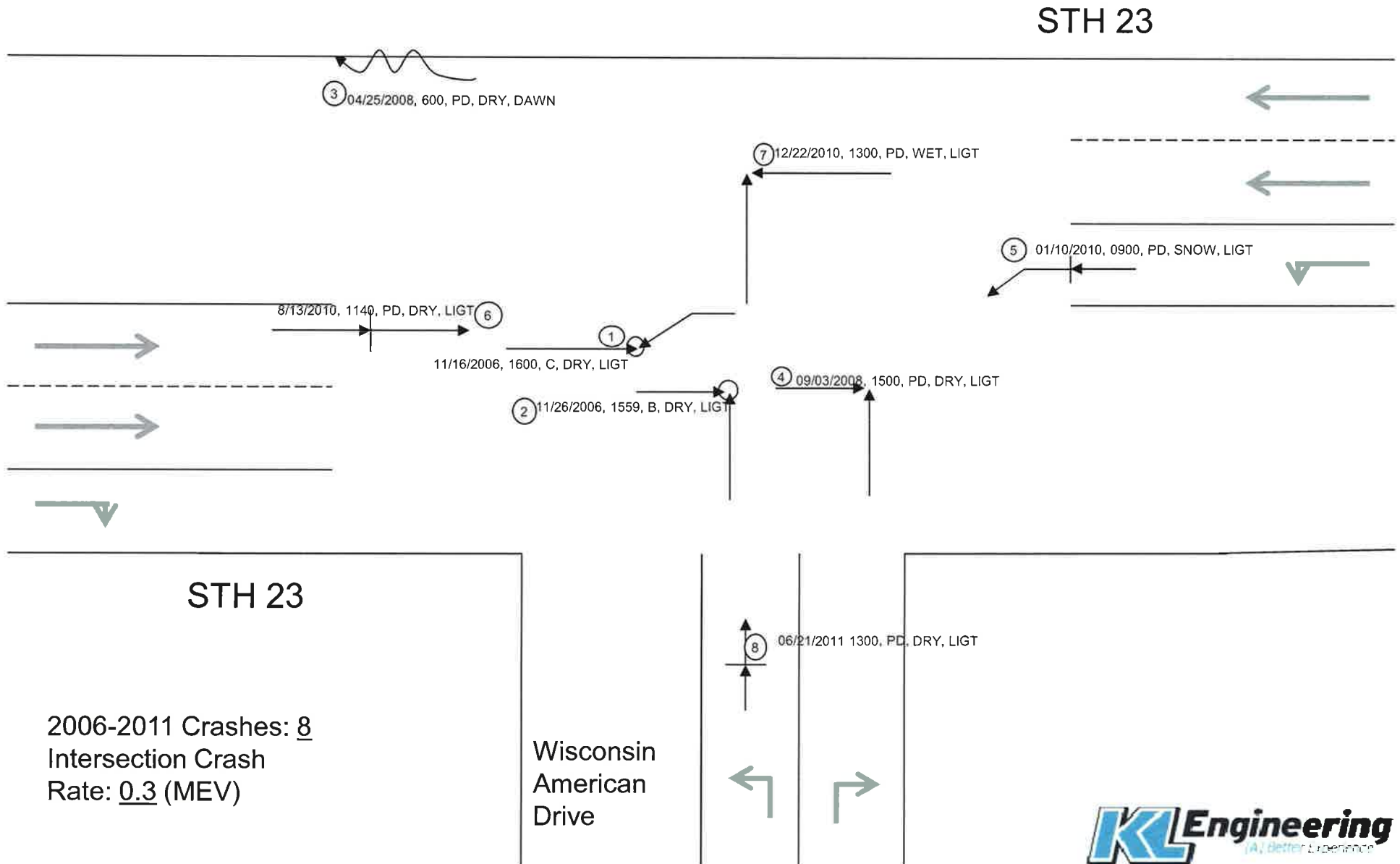


Appendix B

Crash Summary

Project ID: 1440-15-01
County: Fond du Lac
Highway: STH 23

STH 23 @ Wisconsin American Dr. Collision Diagram



Appendix C

Traffic Volume Information

Wisconsin Department of Transportation

Daily Volume from 08/22/2011 through 08/24/2011

Site Names: 200219, 1717, NE
 County: Fond Du Lac
 Funct. Class: U Principal Arterial - Other
 Location: STH 23 EAST OF CTH K FOND DU LAC

Seasonal Factor Type: 2
 Daily Factor Type: 2
 Axle Factor Type: 5
 Growth Factor Type: 1

| | Sun 08/21/2011 | | | Mon 08/22/2011 | | | Tue 08/23/2011 | | | Wed 08/24/2011 | | | Thu 08/25/2011 | | | Fri 08/26/2011 | | | Sat 08/27/2011 | | |
|--------------|----------------|-----|-----|----------------|-------|-------|----------------|-------|-------|----------------|-------|-------|----------------|-----|-----|----------------|-----|-----|----------------|-----|-----|
| | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS |
| 00:00 | | | | | | | 80 | 43 | 37 | 67 | 28 | 39 | | | | | | | | | |
| 01:00 | | | | | | | 39 | 11 | 28 | 66 | 31 | 35 | | | | | | | | | |
| 02:00 | | | | | | | 54 | 27 | 27 | 51 | 37 | 14 | | | | | | | | | |
| 03:00 | | | | | | | 79 | 52 | 27 | 85 | 57 | 28 | | | | | | | | | |
| 04:00 | | | | | | | 157 | 86 | 71 | 154 | 85 | 69 | | | | | | | | | |
| 05:00 | | | | | | | 390 | 226 | 164 | 339 | 212 | 127 | | | | | | | | | |
| 06:00 | | | | | | | 661 | 401 | 260 | 681 | 407 | 274 | | | | | | | | | |
| 07:00 | | | | | | | 893 | 556 | 337 | 911 | 566 | 345 | | | | | | | | | |
| 08:00 | | | | | | | 720 | 430 | 290 | 784 | 473 | 311 | | | | | | | | | |
| 09:00 | | | | | | | 693 | 393 | 300 | 659 | 375 | 284 | | | | | | | | | |
| 10:00 | | | | | | | 789 | 426 | 363 | 736 | 340 | 396 | | | | | | | | | |
| 11:00 | | | | | | | 692 | 356 | 336 | 765 | 424 | 341 | | | | | | | | | |
| 12:00 | | | | | | | 732 | 364 | 368 | 794 | 423 | 371 | | | | | | | | | |
| 13:00 | | | | 813 | 384 | 429 | 798 | 387 | 411 | | | | | | | | | | | | |
| 14:00 | | | | 844 | 422 | 422 | 833 | 447 | 386 | | | | | | | | | | | | |
| 15:00 | | | | 906 | 444 | 462 | 873 | 415 | 458 | | | | | | | | | | | | |
| 16:00 | | | | 1,013 | 427 | 586 | 1,094 | 481 | 613 | | | | | | | | | | | | |
| 17:00 | | | | 992 | 455 | 537 | 1,076 | 483 | 593 | | | | | | | | | | | | |
| 18:00 | | | | 648 | 265 | 383 | 702 | 301 | 401 | | | | | | | | | | | | |
| 19:00 | | | | 507 | 228 | 279 | 530 | 218 | 312 | | | | | | | | | | | | |
| 20:00 | | | | 464 | 195 | 269 | 451 | 188 | 263 | | | | | | | | | | | | |
| 21:00 | | | | 317 | 111 | 206 | 349 | 165 | 184 | | | | | | | | | | | | |
| 22:00 | | | | 206 | 76 | 130 | 197 | 87 | 110 | | | | | | | | | | | | |
| 23:00 | | | | 113 | 53 | 60 | 136 | 67 | 69 | | | | | | | | | | | | |
| Volume | | | | 6,823 | 3,060 | 3,763 | 13,018 | 6,610 | 6,408 | 6,092 | 3,458 | 2,634 | | | | | | | | | |
| AM Peak Vol | | | | | | | 893 | 556 | 363 | 911 | 566 | 396 | | | | | | | | | |
| AM Peak Fct | | | | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | | | | |
| AM Peak Hr | | | | | | | 7:00 | 7:00 | 10:00 | 7:00 | 7:00 | 10:00 | | | | | | | | | |
| PM Peak Vol | | | | | | | 1,094 | 483 | 613 | | | | | | | | | | | | |
| PM Peak Fct | | | | | | | 1.00 | 1.00 | 1.00 | | | | | | | | | | | | |
| PM Peak Hr | | | | | | | 16:00 | 17:00 | 16:00 | | | | | | | | | | | | |
| Seasonal Fct | | | | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | | | | | | | | | |
| Daily Fct | | | | 0.968 | 0.968 | 0.968 | 0.950 | 0.950 | 0.950 | 0.931 | 0.931 | 0.931 | | | | | | | | | |
| Axle Fct | | | | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | | | | | | | | | |
| Pulse Fct | | | | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | | | | | | | | | |

Wisconsin Department of Transportation

Daily Volume from 08/22/2011 through 08/24/2011

Site Names: 201185, 8926, NE
 County: Fond Du Lac
 Funct. Class: U Principal Arterial - Other
 Location: STH 23 BTWN WISCONSIN AMERICAN DR & CTH K FOND DU LAC

Seasonal Factor Type: 2
 Daily Factor Type: 2
 Axle Factor Type: 5
 Growth Factor Type: 1

| | Sun 08/21/2011 | | | Mon 08/22/2011 | | | Tue 08/23/2011 | | | Wed 08/24/2011 | | | Thu 08/25/2011 | | | Fri 08/26/2011 | | | Sat 08/27/2011 | | |
|--------------|----------------|-----|-----|----------------|-------|-------|----------------|-------|-------|----------------|-------|-------|----------------|-----|-----|----------------|-----|-----|----------------|-----|-----|
| | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS | ROAD | NEG | POS |
| 00:00 | | | | | | | 87 | 42 | 45 | 76 | 30 | 46 | | | | | | | | | |
| 01:00 | | | | | | | 39 | 11 | 28 | 66 | 28 | 38 | | | | | | | | | |
| 02:00 | | | | | | | 55 | 29 | 26 | 51 | 37 | 14 | | | | | | | | | |
| 03:00 | | | | | | | 79 | 51 | 28 | 87 | 58 | 29 | | | | | | | | | |
| 04:00 | | | | | | | 157 | 85 | 72 | 155 | 83 | 72 | | | | | | | | | |
| 05:00 | | | | | | | 390 | 223 | 167 | 346 | 215 | 131 | | | | | | | | | |
| 06:00 | | | | | | | 697 | 415 | 282 | 724 | 430 | 294 | | | | | | | | | |
| 07:00 | | | | | | | 980 | 600 | 380 | 961 | 598 | 363 | | | | | | | | | |
| 08:00 | | | | | | | 767 | 475 | 292 | 871 | 520 | 351 | | | | | | | | | |
| 09:00 | | | | | | | 773 | 432 | 341 | 740 | 423 | 317 | | | | | | | | | |
| 10:00 | | | | | | | 850 | 466 | 384 | 811 | 379 | 432 | | | | | | | | | |
| 11:00 | | | | | | | 737 | 380 | 357 | 858 | 469 | 389 | | | | | | | | | |
| 12:00 | | | | | | | 859 | 426 | 433 | 902 | 474 | 428 | | | | | | | | | |
| 13:00 | | | | 885 | 416 | 469 | 912 | 438 | 474 | | | | | | | | | | | | |
| 14:00 | | | | 989 | 488 | 501 | 984 | 499 | 485 | | | | | | | | | | | | |
| 15:00 | | | | 1,055 | 520 | 535 | 1,012 | 476 | 536 | | | | | | | | | | | | |
| 16:00 | | | | 1,154 | 495 | 659 | 1,206 | 548 | 658 | | | | | | | | | | | | |
| 17:00 | | | | 1,148 | 509 | 639 | 1,203 | 545 | 658 | | | | | | | | | | | | |
| 18:00 | | | | 789 | 364 | 425 | 842 | 385 | 457 | | | | | | | | | | | | |
| 19:00 | | | | 608 | 290 | 318 | 612 | 263 | 349 | | | | | | | | | | | | |
| 20:00 | | | | 527 | 218 | 309 | 508 | 207 | 301 | | | | | | | | | | | | |
| 21:00 | | | | 343 | 127 | 216 | 366 | 168 | 198 | | | | | | | | | | | | |
| 22:00 | | | | 217 | 90 | 127 | 231 | 107 | 124 | | | | | | | | | | | | |
| 23:00 | | | | 135 | 64 | 71 | 145 | 75 | 70 | | | | | | | | | | | | |
| Volume | | | | 7,850 | 3,581 | 4,269 | 14,491 | 7,346 | 7,145 | 6,648 | 3,744 | 2,904 | | | | | | | | | |
| AM Peak Vol | | | | | | | 980 | 600 | 384 | 961 | 598 | 432 | | | | | | | | | |
| AM Peak Fct | | | | | | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | | | | | | | | |
| AM Peak Hr | | | | | | | 7:00 | 7:00 | 10:00 | 7:00 | 7:00 | 10:00 | | | | | | | | | |
| PM Peak Vol | | | | | | | 1,206 | 548 | 658 | | | | | | | | | | | | |
| PM Peak Fct | | | | | | | 1.00 | 1.00 | 1.00 | | | | | | | | | | | | |
| PM Peak Hr | | | | | | | 16:00 | 16:00 | 16:00 | | | | | | | | | | | | |
| Seasonal Fct | | | | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | 0.930 | | | | | | | | | |
| Daily Fct | | | | 0.968 | 0.968 | 0.968 | 0.950 | 0.950 | 0.950 | 0.931 | 0.931 | 0.931 | | | | | | | | | |
| Axle Fct | | | | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | 0.435 | | | | | | | | | |
| Pulse Fct | | | | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | 2.000 | | | | | | | | | |

KL Engineering, Inc.

5950 Seminole Centre Court, Suite 200
Madison, WI 53711

STH 23 & Wisconsin American Dr.
12 Hour turning movement count
January 10, 2006
Fond du Lac, WI

File Name : 23&WIAM
Site Code : 04210112
Start Date : 1/10/2006
Page No : 1

Groups Printed- CARS - TRUCKS

| | From North | | | | | STH 23 From East | | | | | WISCONSIN AMERICAN DR. From South | | | | | STH 23 From West | | | | | |
|------------|------------|------|------|------|------------|---------------------|------|------|------|------------|--------------------------------------|------|------|------|------------|---------------------|------|------|------|------------|------------|
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | |
| 06:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 65 | 0 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 9 | 39 | 0 | 0 | 48 | 113 |
| 06:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 91 | 4 | 0 | 95 | 0 | 0 | 1 | 0 | 1 | 10 | 63 | 0 | 0 | 73 | 169 |
| 06:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 119 | 2 | 0 | 121 | 2 | 0 | 0 | 0 | 2 | 12 | 52 | 0 | 0 | 64 | 187 |
| 06:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 107 | 2 | 0 | 109 | 2 | 0 | 2 | 0 | 4 | 30 | 73 | 0 | 0 | 103 | 216 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 382 | 8 | 0 | 390 | 4 | 0 | 3 | 0 | 7 | 61 | 227 | 0 | 0 | 288 | 685 |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 126 | 5 | 0 | 131 | 1 | 0 | 7 | 0 | 8 | 12 | 74 | 0 | 0 | 86 | 225 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 168 | 3 | 0 | 171 | 0 | 0 | 7 | 0 | 7 | 22 | 78 | 0 | 0 | 100 | 278 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 180 | 4 | 0 | 184 | 0 | 0 | 1 | 0 | 1 | 13 | 87 | 1 | 0 | 101 | 286 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 171 | 4 | 0 | 175 | 1 | 0 | 7 | 0 | 8 | 49 | 134 | 0 | 0 | 183 | 366 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 645 | 16 | 0 | 661 | 2 | 0 | 22 | 0 | 24 | 96 | 373 | 1 | 0 | 470 | 1155 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 103 | 4 | 0 | 107 | 2 | 0 | 8 | 0 | 10 | 30 | 85 | 0 | 0 | 115 | 232 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 95 | 7 | 0 | 102 | 1 | 0 | 9 | 0 | 10 | 43 | 61 | 0 | 0 | 104 | 216 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 90 | 1 | 0 | 91 | 4 | 0 | 15 | 0 | 19 | 24 | 55 | 0 | 0 | 79 | 189 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 86 | 4 | 0 | 90 | 3 | 0 | 15 | 0 | 18 | 45 | 56 | 0 | 0 | 101 | 209 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 374 | 16 | 0 | 390 | 10 | 0 | 47 | 0 | 57 | 142 | 257 | 0 | 0 | 399 | 846 |
| 09:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 3 | 0 | 71 | 1 | 0 | 8 | 0 | 9 | 33 | 55 | 0 | 0 | 88 | 168 |
| 09:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 73 | 6 | 0 | 79 | 3 | 0 | 18 | 0 | 21 | 31 | 49 | 0 | 0 | 80 | 180 |
| 09:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 7 | 0 | 82 | 5 | 0 | 21 | 0 | 26 | 33 | 65 | 0 | 0 | 98 | 206 |
| 09:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 79 | 3 | 0 | 82 | 3 | 0 | 27 | 0 | 30 | 28 | 66 | 0 | 0 | 94 | 206 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 295 | 19 | 0 | 314 | 12 | 0 | 74 | 0 | 86 | 125 | 235 | 0 | 0 | 360 | 760 |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 2 | 0 | 78 | 1 | 0 | 29 | 0 | 30 | 17 | 50 | 0 | 0 | 67 | 175 |
| 10:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 4 | 0 | 72 | 4 | 0 | 30 | 0 | 34 | 48 | 56 | 0 | 0 | 104 | 210 |
| 10:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 60 | 5 | 0 | 65 | 3 | 0 | 37 | 0 | 40 | 23 | 56 | 0 | 0 | 79 | 184 |
| 10:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 69 | 3 | 0 | 72 | 2 | 0 | 33 | 0 | 35 | 36 | 56 | 0 | 0 | 92 | 199 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 273 | 14 | 0 | 287 | 10 | 0 | 129 | 0 | 139 | 124 | 218 | 0 | 0 | 342 | 768 |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 4 | 0 | 80 | 4 | 0 | 31 | 0 | 35 | 38 | 74 | 0 | 0 | 112 | 227 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 78 | 2 | 0 | 80 | 4 | 0 | 32 | 0 | 36 | 20 | 66 | 0 | 0 | 86 | 202 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 63 | 3 | 0 | 66 | 7 | 0 | 41 | 0 | 48 | 26 | 78 | 0 | 0 | 104 | 218 |
| 11:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 80 | 4 | 0 | 84 | 3 | 0 | 38 | 0 | 41 | 17 | 59 | 0 | 0 | 76 | 201 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 297 | 13 | 0 | 310 | 18 | 0 | 142 | 0 | 160 | 101 | 277 | 0 | 0 | 378 | 848 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 3 | 0 | 78 | 5 | 0 | 36 | 0 | 41 | 23 | 77 | 0 | 0 | 100 | 219 |
| 12:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 83 | 2 | 0 | 85 | 2 | 0 | 14 | 0 | 16 | 21 | 79 | 0 | 0 | 100 | 201 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 2 | 0 | 78 | 6 | 0 | 30 | 0 | 36 | 38 | 71 | 0 | 0 | 109 | 223 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 96 | 2 | 0 | 98 | 6 | 0 | 22 | 0 | 28 | 38 | 80 | 0 | 0 | 118 | 244 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 330 | 9 | 0 | 339 | 19 | 0 | 102 | 0 | 121 | 120 | 307 | 0 | 0 | 427 | 887 |
| 01:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 3 | 0 | 79 | 3 | 0 | 23 | 0 | 26 | 31 | 82 | 0 | 0 | 113 | 218 |
| 01:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 80 | 4 | 0 | 84 | 7 | 0 | 27 | 0 | 34 | 34 | 92 | 0 | 0 | 126 | 244 |
| 01:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 77 | 2 | 0 | 79 | 5 | 0 | 35 | 0 | 40 | 35 | 89 | 0 | 0 | 124 | 243 |
| 01:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 84 | 6 | 0 | 90 | 3 | 0 | 17 | 0 | 20 | 30 | 94 | 0 | 0 | 124 | 234 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 317 | 15 | 0 | 332 | 18 | 0 | 102 | 0 | 120 | 130 | 357 | 0 | 0 | 487 | 939 |
| 02:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 71 | 1 | 0 | 72 | 4 | 0 | 23 | 0 | 27 | 29 | 66 | 0 | 0 | 95 | 194 |
| 02:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 97 | 6 | 0 | 103 | 1 | 0 | 27 | 0 | 28 | 29 | 61 | 0 | 0 | 90 | 221 |
| 02:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 4 | 0 | 89 | 4 | 0 | 41 | 0 | 45 | 23 | 88 | 0 | 0 | 111 | 245 |
| 02:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 4 | 0 | 103 | 4 | 0 | 33 | 0 | 37 | 23 | 93 | 0 | 0 | 116 | 256 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 352 | 15 | 0 | 367 | 13 | 0 | 124 | 0 | 137 | 104 | 308 | 0 | 0 | 412 | 916 |
| 03:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 131 | 1 | 0 | 132 | 4 | 0 | 27 | 0 | 31 | 25 | 101 | 0 | 0 | 126 | 289 |
| 03:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 126 | 3 | 0 | 129 | 6 | 0 | 27 | 0 | 33 | 30 | 115 | 0 | 0 | 145 | 307 |
| 03:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 107 | 2 | 0 | 109 | 5 | 0 | 43 | 0 | 48 | 18 | 137 | 0 | 0 | 155 | 312 |

KL Engineering, Inc.

5950 Seminole Centre Court, Suite 200
Madison, WI 53711

File Name : 23&WIAM

Site Code : 04210112

Start Date : 1/10/2006

Page No : 2

Groups Printed- CARS - TRUCKS

| | From North | | | | | STH 23 From East | | | | | WISCONSIN AMERICAN DR. From South | | | | | STH 23 From West | | | | | |
|-------------|------------|------|------|------|------------|---------------------|------|------|------|------------|--------------------------------------|------|------|------|------------|---------------------|------|------|------|------------|------------|
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | |
| 03:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 3 | 0 | 102 | 5 | 0 | 35 | 0 | 40 | 30 | 124 | 3 | 0 | 157 | 299 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 463 | 9 | 0 | 472 | 20 | 0 | 132 | 0 | 152 | 103 | 477 | 3 | 0 | 583 | 1207 |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 118 | 4 | 0 | 122 | 7 | 0 | 45 | 0 | 52 | 28 | 115 | 0 | 0 | 143 | 317 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 114 | 8 | 0 | 122 | 9 | 0 | 43 | 0 | 52 | 10 | 144 | 0 | 0 | 154 | 328 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 104 | 3 | 0 | 107 | 8 | 0 | 49 | 0 | 57 | 20 | 141 | 0 | 0 | 161 | 325 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 105 | 2 | 0 | 107 | 2 | 0 | 36 | 0 | 38 | 18 | 125 | 0 | 0 | 143 | 288 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 441 | 17 | 0 | 458 | 26 | 0 | 173 | 0 | 199 | 76 | 525 | 0 | 0 | 601 | 1258 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 5 | 0 | 104 | 13 | 0 | 57 | 0 | 70 | 10 | 143 | 0 | 0 | 153 | 327 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 81 | 4 | 0 | 85 | 8 | 0 | 20 | 0 | 28 | 11 | 117 | 0 | 0 | 128 | 241 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 0 | 0 | 85 | 6 | 0 | 29 | 0 | 35 | 4 | 134 | 0 | 0 | 138 | 258 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 104 | 0 | 0 | 104 | 1 | 0 | 9 | 0 | 10 | 2 | 117 | 0 | 0 | 119 | 233 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 369 | 9 | 0 | 378 | 28 | 0 | 115 | 0 | 143 | 27 | 511 | 0 | 0 | 538 | 1059 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 4538 | 160 | 0 | 4698 | 180 | 0 | 1165 | 0 | 1345 | 1209 | 4072 | 4 | 0 | 5285 | 11328 |
| Apprch % | 0 | 0 | 0 | 0 | | 0 | 96.6 | 3.4 | 0 | | 13.4 | 0 | 86.6 | 0 | | 22.9 | 77 | 0.1 | 0 | | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 40.1 | 1.4 | 0 | 41.5 | 1.6 | 0 | 10.3 | 0 | 11.9 | 10.7 | 35.9 | 0 | 0 | 46.7 | |
| CARS | 0 | 0 | 0 | 0 | 0 | 0 | 4100 | 157 | 0 | 4257 | 175 | 0 | 1150 | 0 | 1325 | 1191 | 3628 | 4 | 0 | 4823 | 10405 |
| % CARS | 0 | 0 | 0 | 0 | 0 | 0 | 90.3 | 98.1 | 0 | 90.6 | 97.2 | 0 | 98.7 | 0 | 98.5 | 98.5 | 89.1 | 100 | 0 | 91.3 | 91.9 |
| TRUCKS | 0 | 0 | 0 | 0 | 0 | 0 | 438 | 3 | 0 | 441 | 5 | 0 | 15 | 0 | 20 | 18 | 444 | 0 | 0 | 462 | 923 |
| % TRUCKS | 0 | 0 | 0 | 0 | 0 | 0 | 9.7 | 1.9 | 0 | 9.4 | 2.8 | 0 | 1.3 | 0 | 1.5 | 1.5 | 10.9 | 0 | 0 | 8.7 | 8.1 |

KL Engineering, Inc.

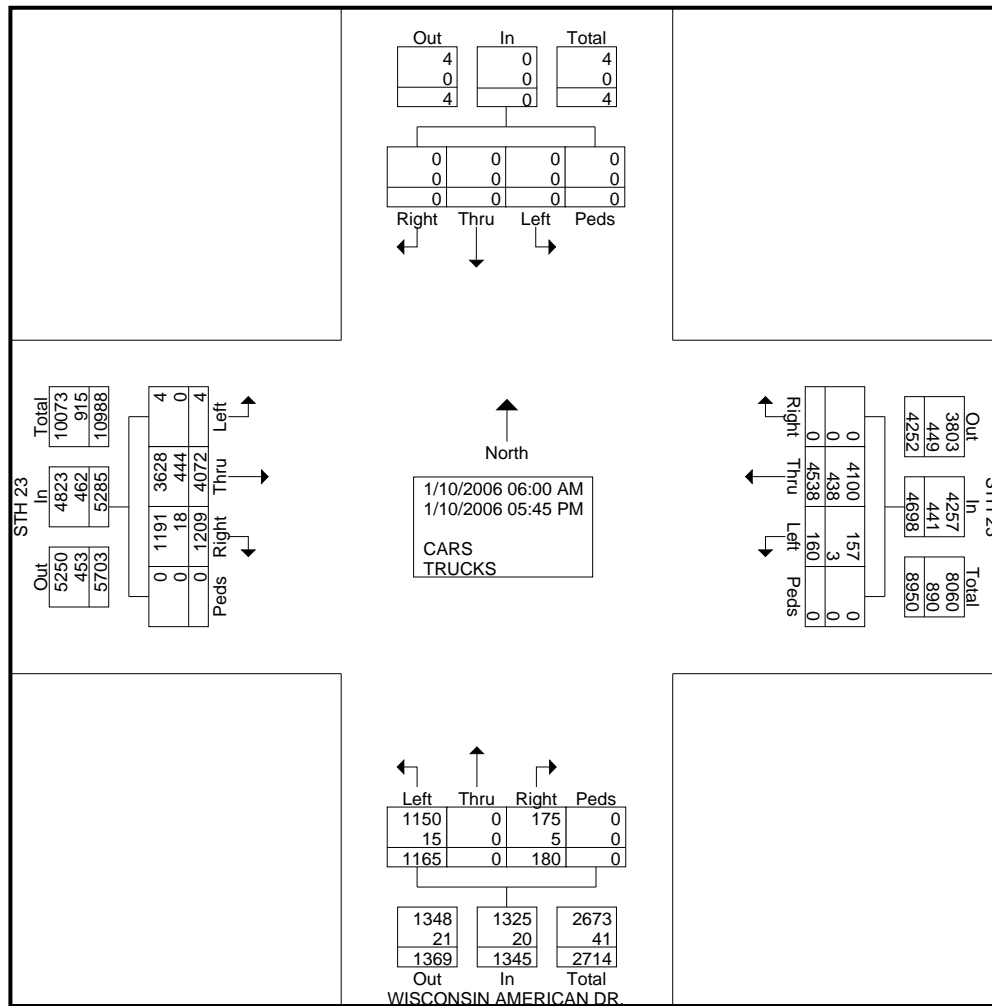
5950 Seminole Centre Court, Suite 200
Madison, WI 53711

File Name : 23&WIAM

Site Code : 04210112

Start Date : 1/10/2006

Page No : 3



KL Engineering, Inc.

5950 Seminole Centre Court, Suite 200
Madison, WI 53711

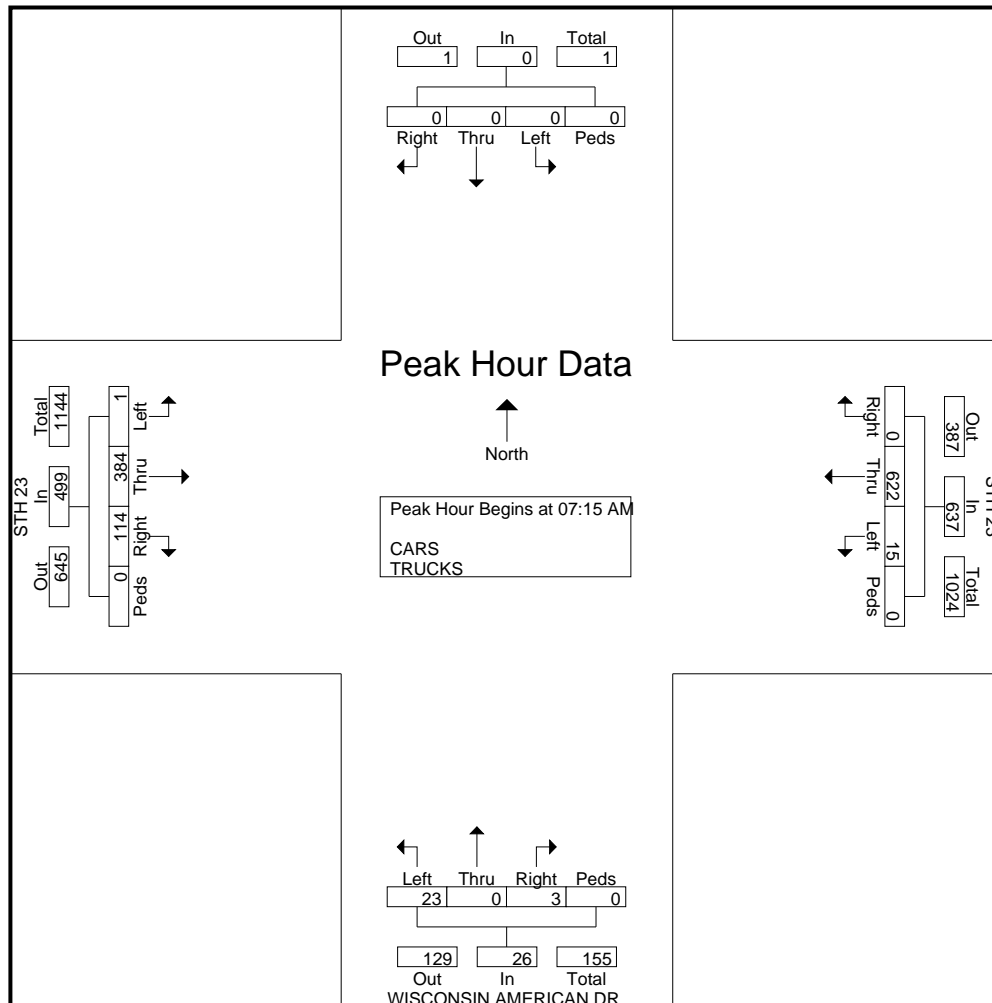
File Name : 23&WIAM

Site Code : 04210112

Start Date : 1/10/2006

Page No : 4

| | From North | | | | | STH 23 From East | | | | | WISCONSIN AMERICAN DR. From South | | | | | STH 23 From West | | | | | |
|--|------------|----------|----------|----------|------------|---------------------|------------|----------|----------|------------|--------------------------------------|----------|----------|----------|------------|---------------------|------------|----------|----------|------------|------------|
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 06:00 AM to 09:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:15 AM | | | | | | | | | | | | | | | | | | | | | |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 168 | 3 | 0 | 171 | 0 | 0 | 7 | 0 | 7 | 22 | 78 | 0 | 0 | 100 | 278 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 180 | 4 | 0 | 184 | 0 | 0 | 1 | 0 | 1 | 13 | 87 | 1 | 0 | 115 | 232 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 171 | 4 | 0 | 175 | 1 | 0 | 7 | 0 | 8 | 49 | 134 | 0 | 0 | 183 | 366 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 103 | 4 | 0 | 107 | 2 | 0 | 8 | 0 | 10 | 30 | 85 | 0 | 0 | 115 | 232 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 622 | 15 | 0 | 637 | 3 | 0 | 23 | 0 | 26 | 114 | 384 | 1 | 0 | 499 | 1162 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 97.6 | 2.4 | 0 | 100.0 | 11.5 | 0 | 88.5 | 0 | 100.0 | 22.8 | 77 | 0.2 | 0 | 100.0 | 100.0 |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .864 | .938 | .000 | .865 | .375 | .000 | .719 | .000 | .650 | .582 | .716 | .250 | .000 | .682 | .794 |



KL Engineering, Inc.

5950 Seminole Centre Court, Suite 200
Madison, WI 53711

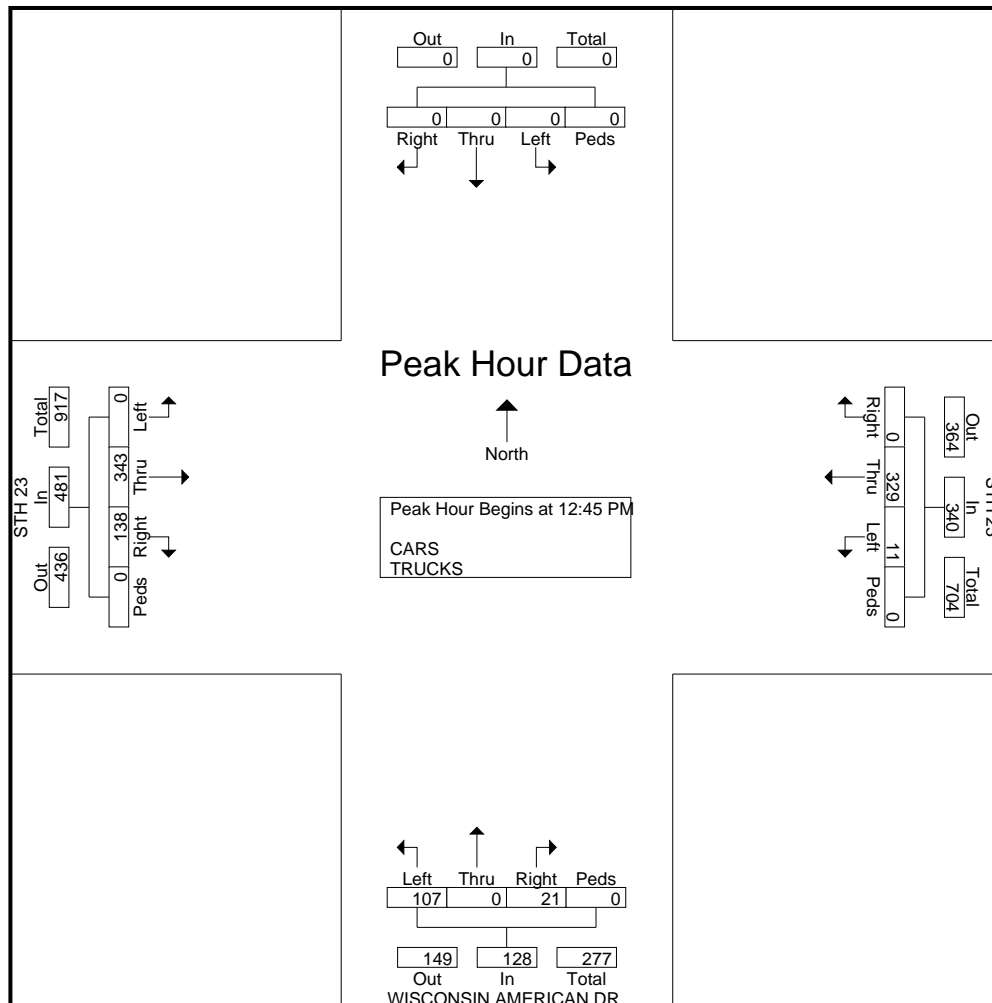
File Name : 23&WIAM

Site Code : 04210112

Start Date : 1/10/2006

Page No : 5

| | From North | | | | | STH 23 From East | | | | | WISCONSIN AMERICAN DR. From South | | | | | STH 23 From West | | | | | |
|--|------------|------|------|------|------------|---------------------|-----------|----------|------|------------|--------------------------------------|------|-----------|------|------------|---------------------|-----------|------|------|------------|------------|
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 10:00 AM to 01:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 12:45 PM | | | | | | | | | | | | | | | | | | | | | |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 96 | 3 | 0 | 98 | 6 | 0 | 22 | 0 | 28 | 38 | 82 | 0 | 0 | 113 | 244 |
| 01:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 3 | 0 | 79 | 3 | 0 | 23 | 0 | 26 | 31 | 92 | 0 | 0 | 126 | 218 |
| 01:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 80 | 4 | 0 | 84 | 7 | 0 | 23 | 0 | 26 | 31 | 92 | 0 | 0 | 126 | 244 |
| 01:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 77 | 2 | 0 | 79 | 5 | 0 | 35 | 0 | 40 | 35 | 89 | 0 | 0 | 124 | 243 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 329 | 11 | 0 | 340 | 21 | 0 | 107 | 0 | 128 | 138 | 343 | 0 | 0 | 481 | 949 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 96.8 | 3.2 | 0 | 100 | 16.4 | 0 | 83.6 | 0 | 100 | 28.7 | 71.3 | 0 | 0 | 100 | 100 |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .857 | .688 | .000 | .867 | .750 | .000 | .764 | .000 | .800 | .908 | .932 | .000 | .000 | .954 | .972 |



KL Engineering, Inc.

5950 Seminole Centre Court, Suite 200
Madison, WI 53711

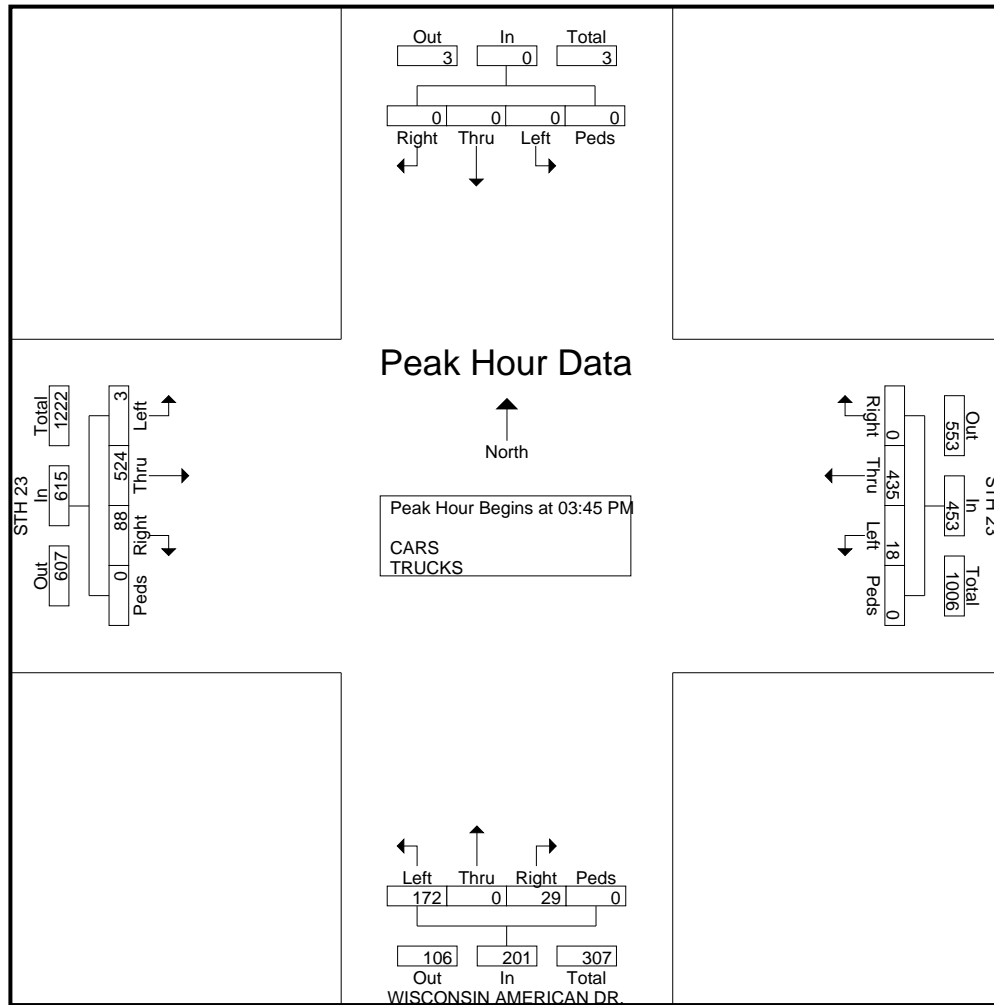
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Site Code : 04210112

Start Date : 1/10/2006

Page No : 6

| | From North | | | | | STH 23 From East | | | | | WISCONSIN AMERICAN DR. From South | | | | | STH 23 From West | | | | | |
|--|------------|----------|----------|----------|------------|---------------------|------------|----------|----------|------------|--------------------------------------|----------|-----------|----------|------------|---------------------|------------|----------|------|------------|------------|
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 02:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 03:45 PM | | | | | | | | | | | | | | | | | | | | | |
| 03:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 3 | 0 | 102 | 5 | 0 | 35 | 0 | 40 | 30 | | 3 | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 118 | 4 | 0 | 122 | 7 | 0 | 45 | 0 | 52 | 28 | 115 | 0 | 0 | 143 | 317 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 114 | 8 | | | 9 | | | | | | 144 | 0 | 0 | 154 | 328 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 104 | 3 | 0 | 107 | 8 | 0 | 49 | 0 | 57 | 20 | 141 | 0 | 0 | 161 | 325 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 435 | 18 | 0 | 453 | 29 | 0 | 172 | 0 | 201 | 88 | 524 | 3 | 0 | 615 | 1269 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 96 | 4 | 0 | | 14.4 | 0 | 85.6 | 0 | | 14.3 | 85.2 | 0.5 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .922 | .563 | .000 | .928 | .806 | .000 | .878 | .000 | .882 | .733 | .910 | .250 | .000 | .955 | .967 |



WisDot Bureau of State Highway Programs
 Traffic Forecasting Section
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 Phone: (608) 266-3976
 Email: william.gavinski@dot.state.wi.us

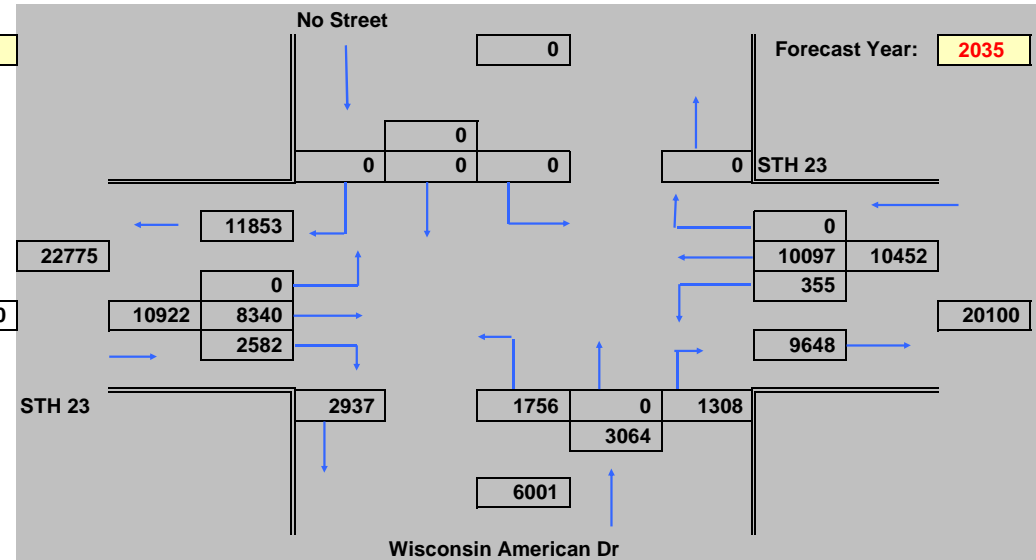
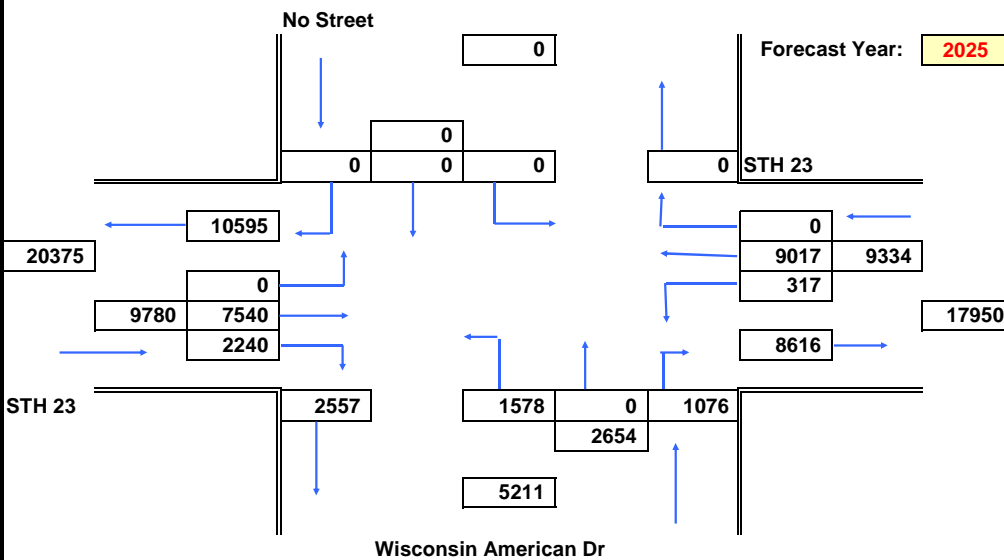
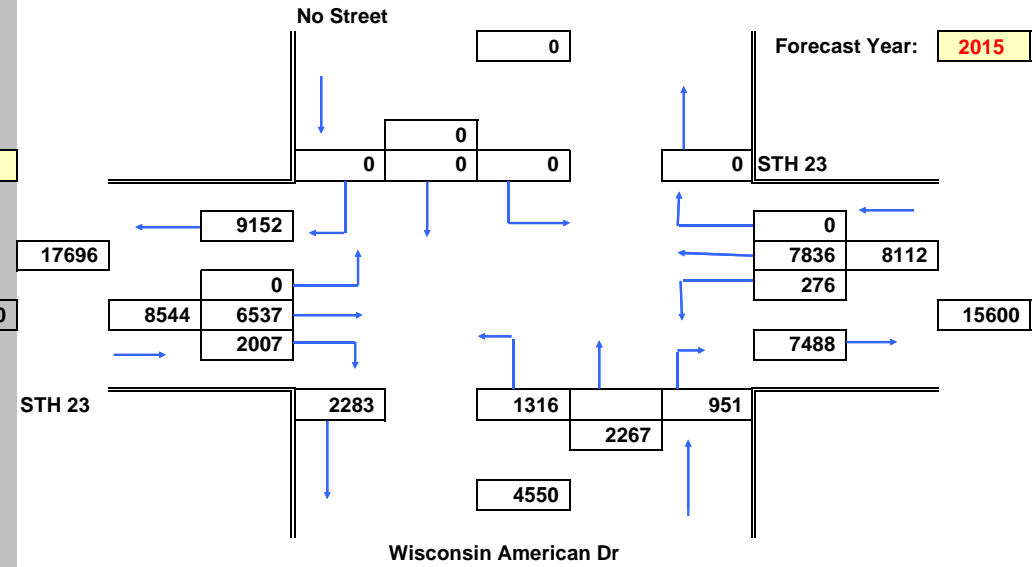
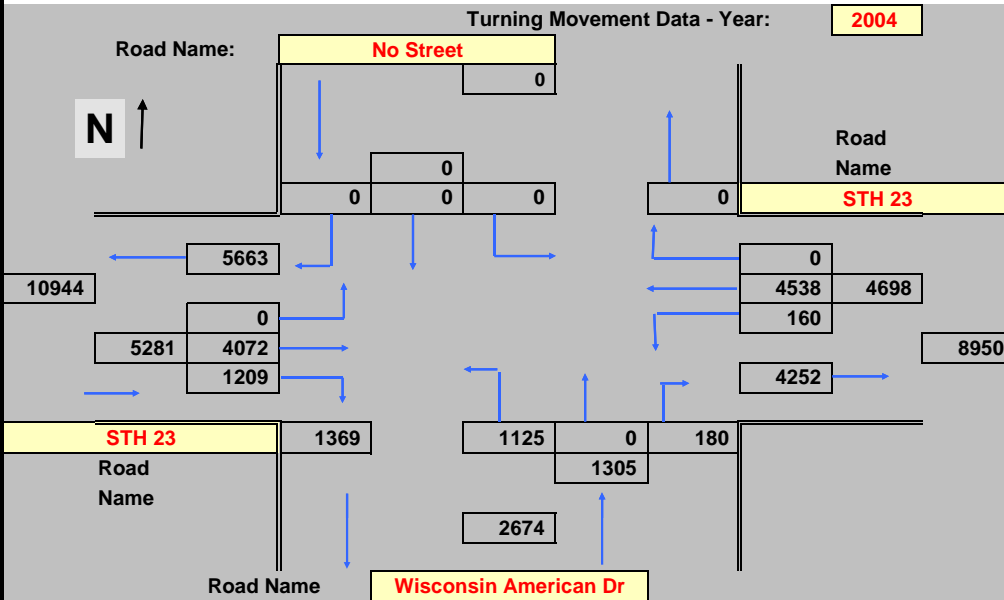
Projected AADT Traffic Volumes

Project Description

Project ID: 1440-13-00
 Location: USH 151 to CTH "UU"

Route: STH 23
 County: Fond du Lac

Forecast Completed: **02-20-06**



WisDot Bureau of State Highway Programs
Traffic Forecasting Section
Developed by Bill Gavinski
Phone: (608) 266-3976
Email: william.gavinski@dot.state.wi.us

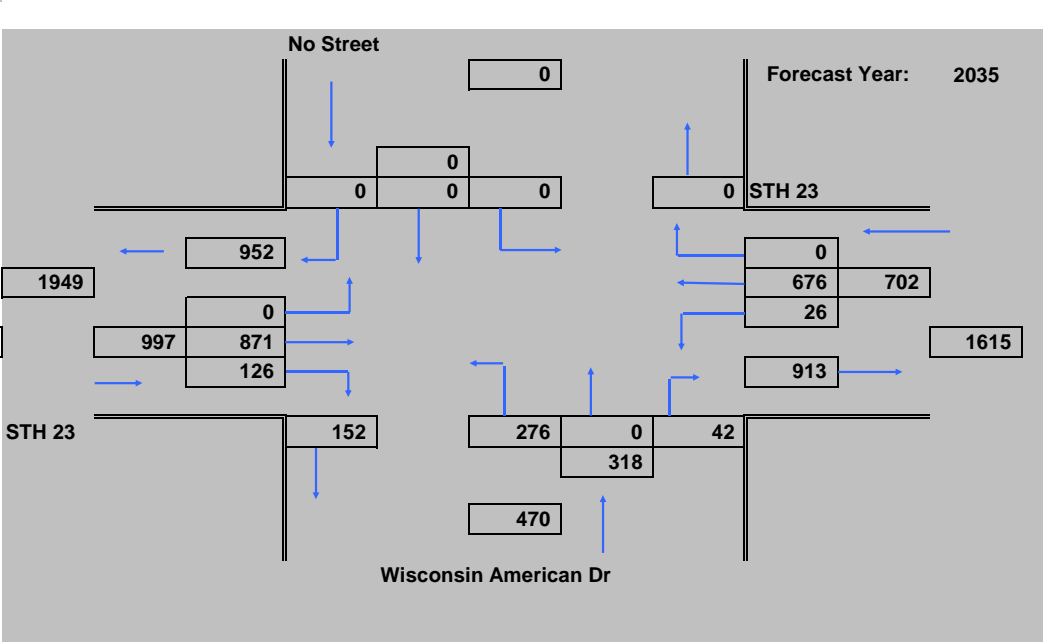
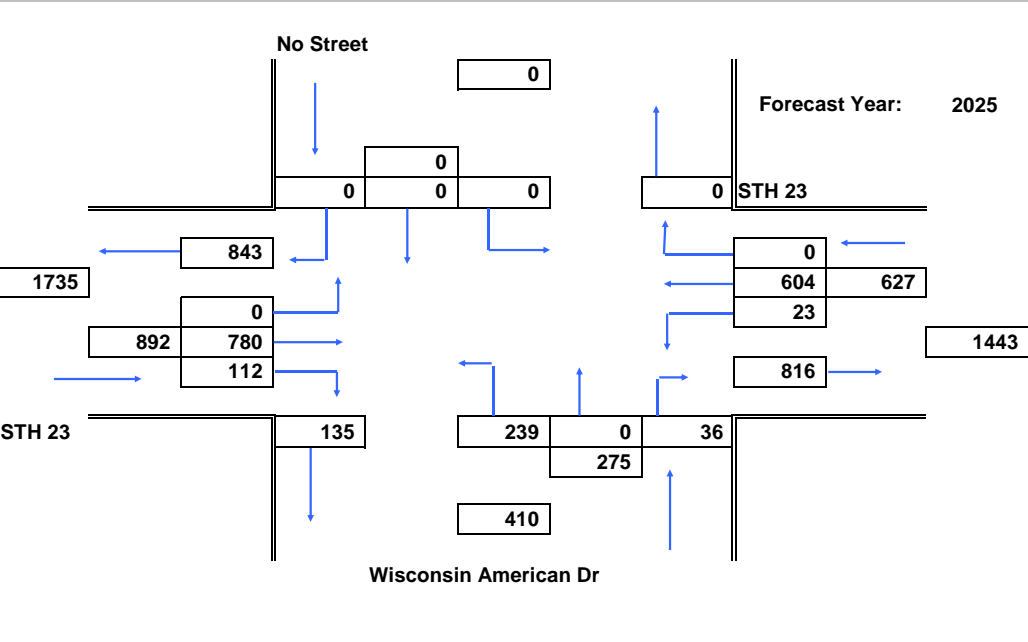
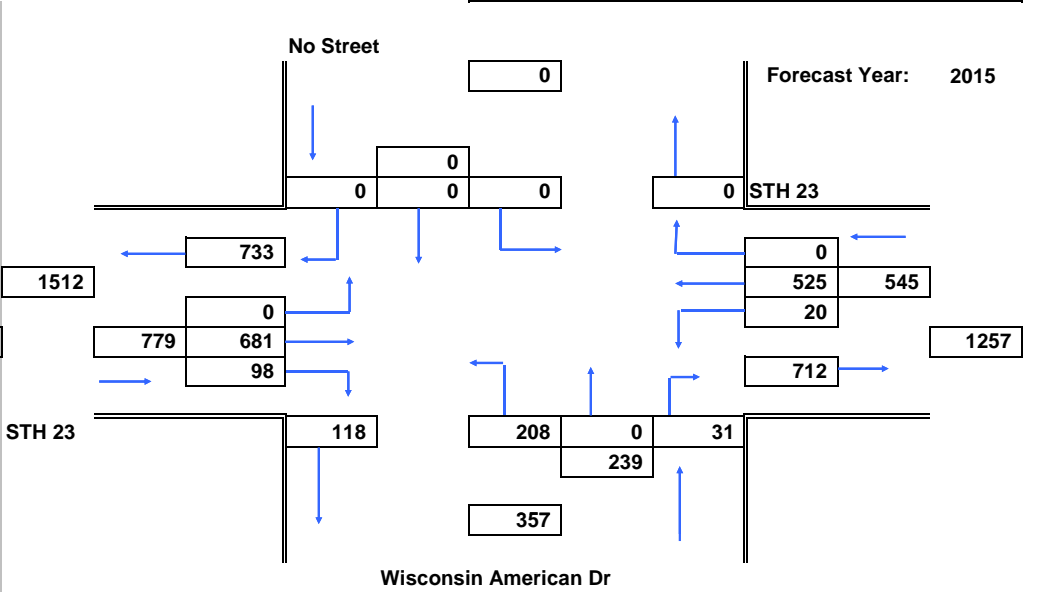
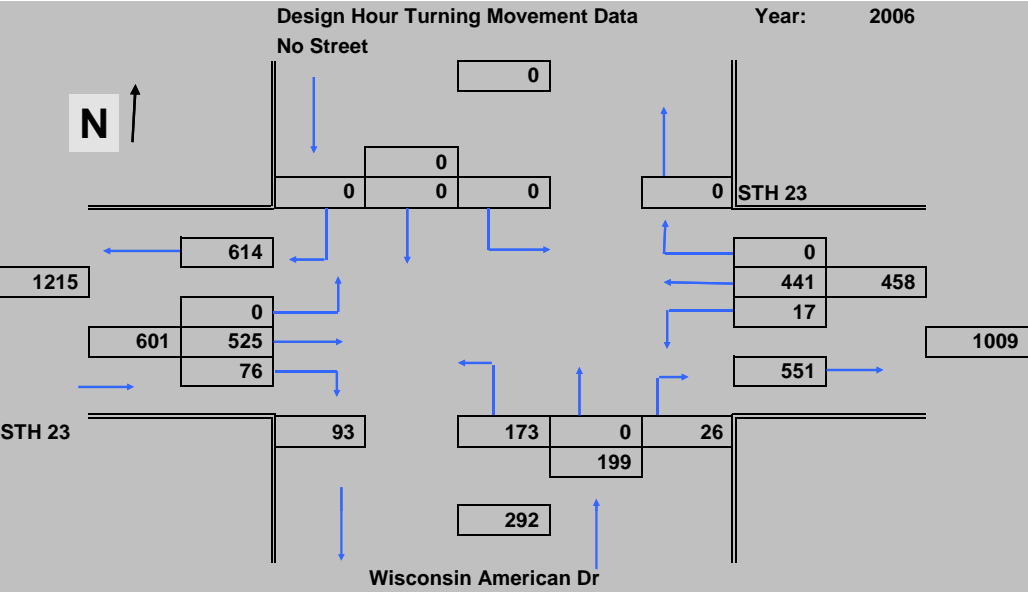
Projected PM Design Hour Traffic Volumes

Design Hour: 4 - 5 p.m.

Forecast Completed: 02-15-06

Project Description

Project ID: 1440-13-00
Location: USH 151 to CTH "UU"
Route: STH 23
County: Fond du Lac



2035 Projected AM Design Hour Traffic Volumes

Mary Greuel
KL Engineering

Design Hour: 7:15 - 8:15 AM

Project Description

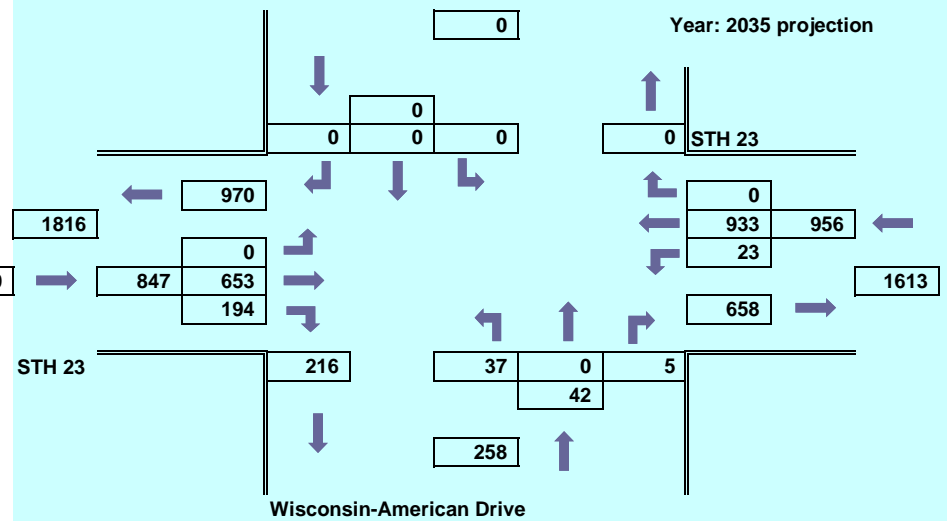
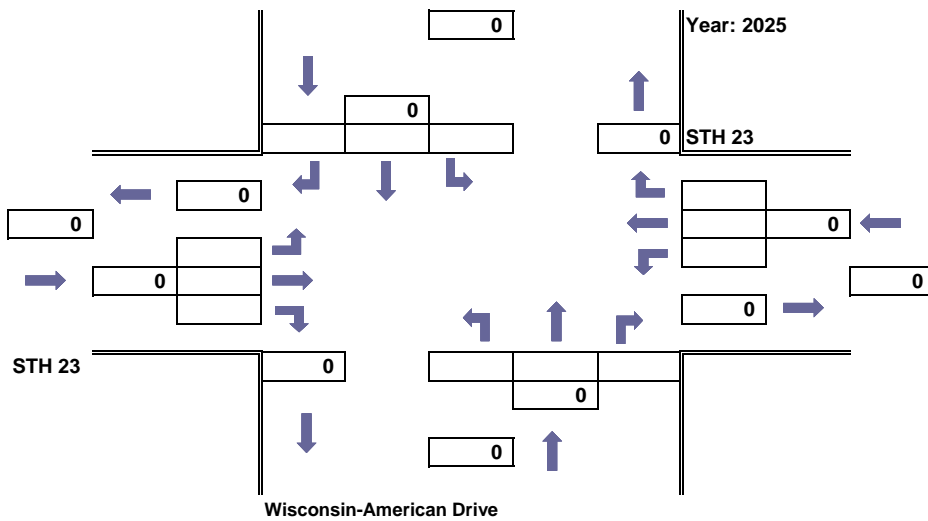
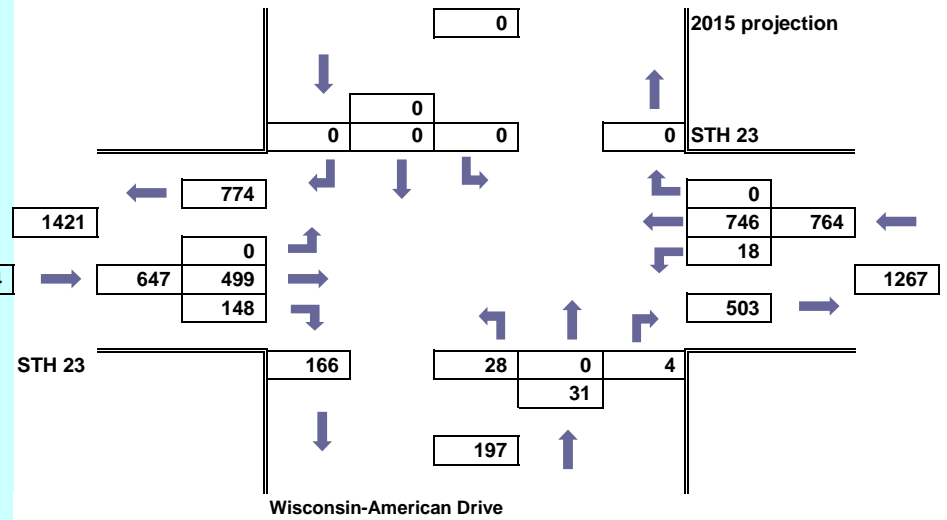
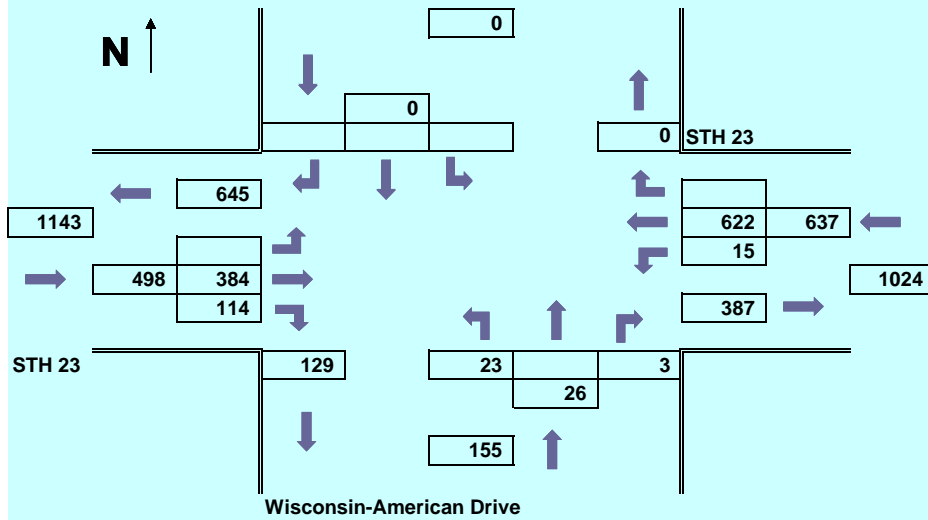
STH 23 and Wisconsin-American Drive

Location: Fond du Lac

Fond du Lac County, WI

Design Hour Turning Movement Data

Year: 2006 Count



Appendix D

Traffic Signal Warrants

Instructions for Completing Warrant Analysis Worksheets

These worksheets contain several fields. It is important to keep in mind the following when entering information in these fields so as to obtain an easy to read final product.

When entering hours relating to which hour meets warrants or describing which hours are used to compare against the warrants, you should not enter the time as 1-2 pm. Rather, the time should be entered as military time (13:00). The assumption is that the one-hour interval begins at 13:00. The reason for this discussion is that there is limited size in the fields that are needed to put the form together. If you input data into the field and extend it outside the limits of the table cell some of the data will be cut off.

Some portions of the worksheet are set up so that values are filled in automatically. If a field does not update properly when a change is made to the source information, you may need to manually enter the information in that particular field. In addition, the worksheet has been set up to automatically update all fields before printing, so if there are fields that you see not updating, please print the document and it will automatically update all of the fields within the worksheet. You will notice that the Warrant Evaluation Summary on the page immediately following this instruction page appears blank to the right of each warrant. There are imbedded fields located here that will only be visible during a print preview or on a hard copy (printed document). These fields are tied to dropdowns located within the document for each signal warrant.

Adding Hours and Volumes to the 8 Highest Hours Table

When entering data into this table it is critical that it is **NOT** entered chronologically, but rather with the **highest volume hour in the first column, the second highest volume hour in the second column** and so forth across the table. This is because the information entered into the first four columns is then used for the Four Hour Warrant table and the Peak Hour Warrant uses the first column of data.

Plotting data for Four Hour, Peak Hour Volume Pedestrian Volume and Intersection Near Grade Crossing Warrants

Plot the points manually after printing out the Worksheets. Following this process eliminates the need to play with the form protections.

Wisconsin Department of Transportation Traffic Signal Warrant Summary Worksheet

70% RURAL

The Worksheet(s) attached are provided as an attachment to the Engineering Investigation Study for:

Intersection: STH 23 and Wisconsin American Drive

Date: 02-23-2012

County: Fond du Lac

Town

Village

City: Fond du Lac

Major Street: STH 23

Critical Approach Speed 45

Lanes 2

Minor Street: General American Drive

Critical Approach Speed 25

Lanes 1

Note: The warrants for rural areas (70% of urban warrant) are used when the 85% speed on the major street exceeds 40 m.p.h. or when the intersection lies within the built-up area of an isolated community having a population of less than 10,000.

THE ANALYSIS IS BASED ON COUNTS CONDUCTED ON 2012 & , 20 , FROM 6:00 A M TO 6:00 P M
DATES DAYS

% Right Turns Included

Warrant Evaluation Summary

YES/NO/NOT EVALUATED

Warrant 1 Eight-Hour Vehicular Volume Yes

Condition A Minimum Vehicular Volume Yes

Condition B Interruption of Continuous Traffic No

Condition C Combination: 80% of A and B N/A

Warrant 2 Four-Hour Volume Yes

Warrant 3 Peak Hour Volume N/A

Warrant 4 Pedestrian Volume N/A

Criterion A Four-Hour N/A

Criterion B Peak Hour N/A

Warrant 5 School Crossing N/A

Warrant 6 Coordinated Signal System N/A

Warrant 7 Crash Experience N/A

Warrant 8 Roadway Network N/A

Warrant 9 Intersection Near A Grade Crossing N/A

This analysis was conducted by:

Mary Greuel

(Name)

KL Engineering

(Agency)

02-23-2012

(Date)

TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

Sheet 1

| | | |
|---|----------------------------|------------------|
| Intersection: STH 23 and Wisconsin American Drive | | Date: 02-23-2012 |
| County: Fond du Lac | | |
| Town Village City Fond du Lac | | |
| Major Street STH 23 | Critical Approach Speed 45 | Lanes 2 |
| Minor Street General American Drive | Critical Approach Speed 25 | Lanes 1 |

Volume Level

1. Critical speed of major road traffic > 40 mph : Yes ☒ No ☐
2. In built-up area of isolated community of < 10,000 pop.: Yes ☐ No ☒
- If Question 1 or 2 above is answered "Yes" then use "70%" volume level: 70% ☒ 100% ☐

WARRANT 1 – Eight-Hour Vehicular Volume

Warrant is satisfied if Condition A or B is "100 % satisfied." Warrant also satisfied if Condition C (80% of A and B) is satisfied.

| 8 Highest Hours | | | | | | | | |
|-----------------------------|-------|-------|------|-------|-------|-------|-------|-------|
| Hour | 16:00 | 15:00 | 1035 | 13:00 | 14:00 | 12:00 | 11:00 | 10:00 |
| Major Road Both App. vph | 1142 | 1101 | 1035 | 800 | 781 | 748 | 680 | 584 |
| Minor Road High App. vph | 195 | 149 | 130 | 115 | 140 | 115 | 160 | 146 |

Record hours where condition is met and the corresponding volumes in boxes provided. Condition is 100% satisfied if the minimum volumes are met for eight hours.

Condition A – Minimum Vehicular Volume

| (volumes in veh/h) | Minimum Requirements (80% Shown in Brackets) | | | |
|-----------------------------|---|-------|--------------|-------|
| Approach Lanes: | 1 | | 2 or more | |
| Volume Level: | 100% | Hours | 100% | Hours |
| Major Road-Both Approaches | 350 | | 420 | 8 |
| | (280) | | (336) | 8 |
| Minor Road-Highest Approach | 105 | 8 | 140 | |
| | (84) | 8 | (112) | |

100% Satisfied: Yes

80 % Satisfied: Yes

Condition B – Interruption of Continuous Traffic

| (volumes in veh/h) | Minimum Requirements (80% Shown in Brackets) | | | |
|-----------------------------|---|-------|--------------|-------|
| Approach Lanes: | 1 | | 2 or more | |
| Volume Level: | 100% | Hours | 100% | Hours |
| Major Road-Both Approaches | 525 | | 630 | 7 |
| | (420) | | (504) | 8 |
| Minor Road-Highest Approach | 53 | 8 | 70 | |
| | (42) | 8 | (56) | |

100% Satisfied: No

80 % Satisfied: Yes

Condition C – Combination of Condition A and B: Condition A and B Both 80% Satisfied?:

Warrant Satisfied?: Yes

% Right Turns Included: 0%

TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

Sheet 2

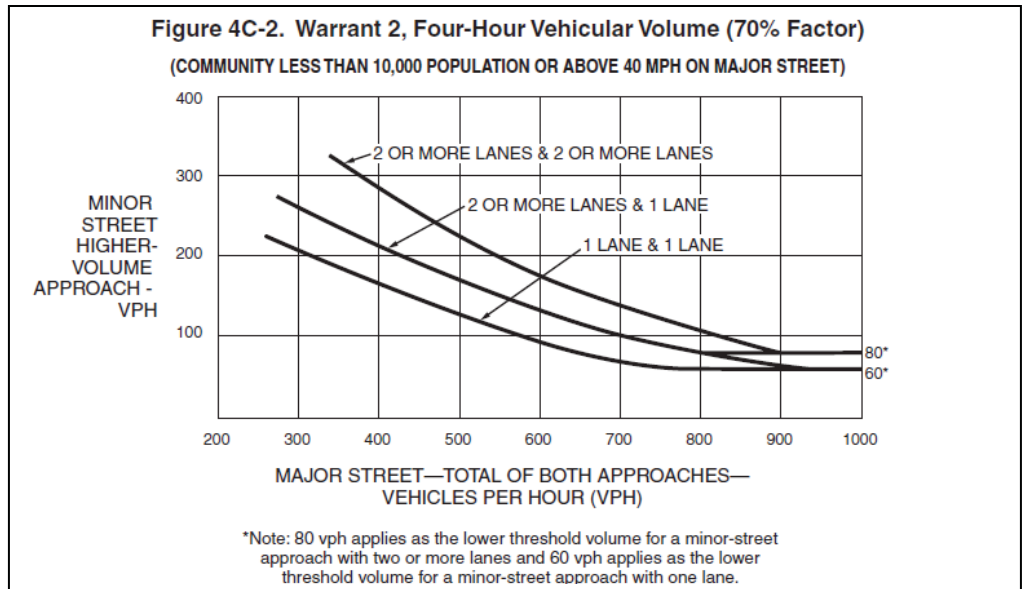
Warrant 2 – Four-Hour Vehicular Volume

Plot four volume combinations on the applicable figure below. If four points lie above the appropriate line, then the warrant is satisfied.

Figure A. Criteria for “70%” volume level.

| Hour | 16:00 | 15:00 | 1035 | 13:00 |
|------------|-------|-------|------|-------|
| Major Vol. | 1142 | 1101 | 1035 | 800 |
| Minor Vol. | 195 | 149 | 130 | 115 |

Satisfied?: Yes



Warrant 3 – Peak Hour

Unusual condition justifying use of warrant: _____

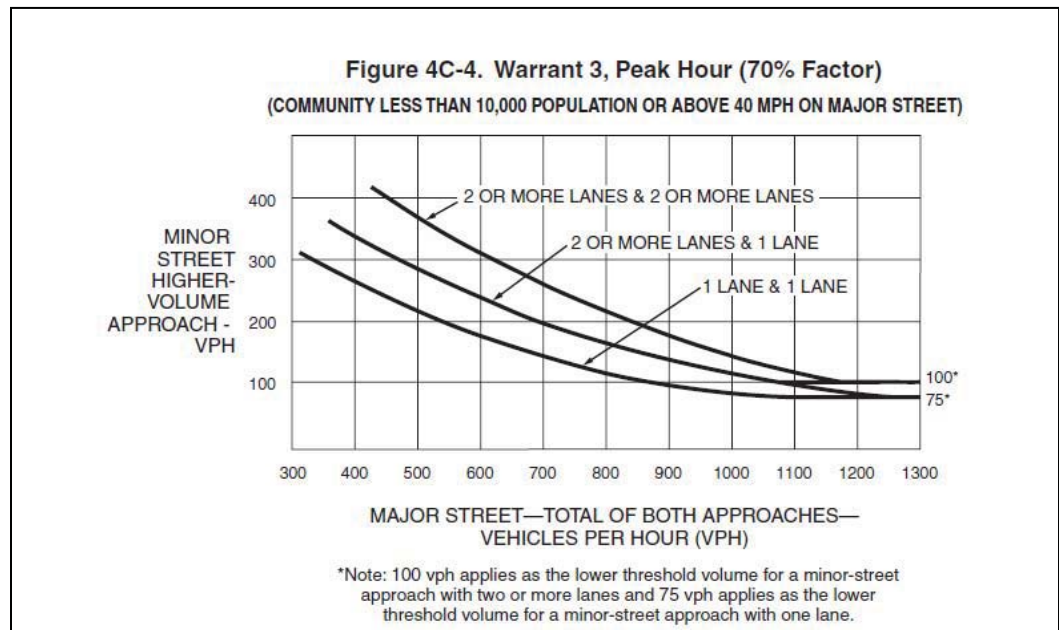
Record hour where criteria are fulfilled and the corresponding delay or volume in boxes provided. Plot the peak hour volume combination on the applicable figure below. If all three criteria are fulfilled or the plotted point lies above the appropriate line, then the warrant is satisfied.

| Criteria | Approach Lanes | | No. of Approaches | | Hour | Fulfilled? | |
|-------------------------------------|----------------|-----|-------------------|-----|------|--------------------------|--------------------------|
| | 1 | 2 | 3 | 4 | | Yes | No |
| 1. Delay on Minor Approach (veh/h) | 4 | 5 | | | | <input type="checkbox"/> | <input type="checkbox"/> |
| 2. Volume on Minor Approach (veh/h) | 100 | 150 | | | | <input type="checkbox"/> | <input type="checkbox"/> |
| 3. Total Entering Volume (veh/h) | | | 650 | 800 | | <input type="checkbox"/> | <input type="checkbox"/> |

Figure A. Criteria for “70%” volume level.

| | |
|------------|-------|
| Hour | 16:00 |
| Major Vol. | 1142 |
| Minor Vol. | 195 |

Satisfied?: N/A



TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

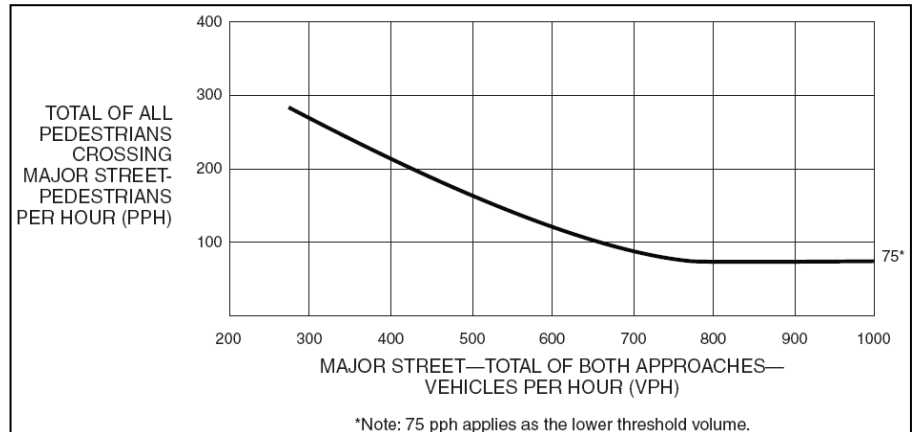
Sheet 3

Warrant 4 – Pedestrian Volume

Plot four volume combinations on the applicable figure below.

Criterion A

| | | | | |
|-----------------|--|--|--|--|
| Hour | | | | |
| Major Vol. | | | | |
| Pedestrian Vol. | | | | |

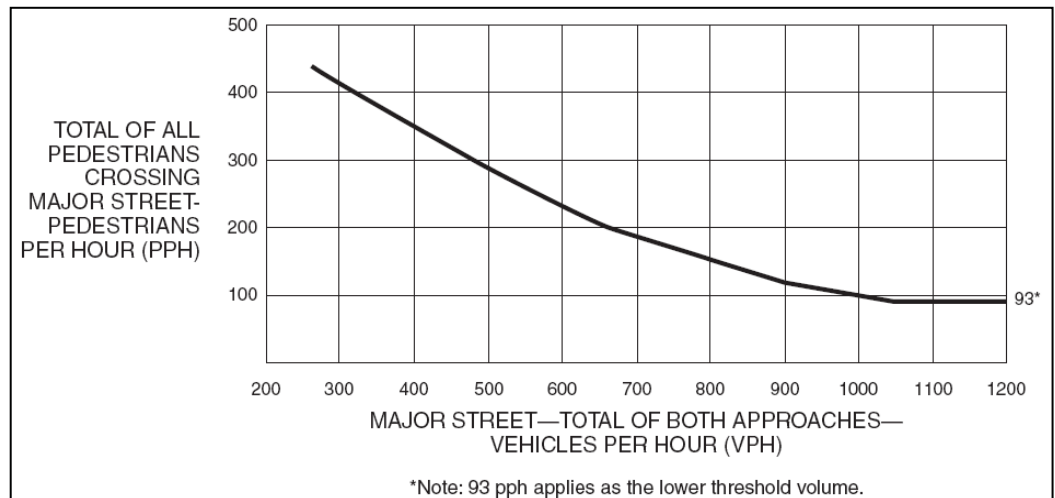


Criterion A Satisfied?: N/A

Criterion B

Plot the peak hour volume combination on the applicable figure below.

| | |
|-----------------|--|
| Hour | |
| Major Vol. | |
| Pedestrian Vol. | |



Criterion B Satisfied?:

N/A

Warrant Satisfied?:

N/A

Warrant 5 – School Crossing

Record hours where criteria are fulfilled and the corresponding volume or gap frequency in the boxes provided.
The warrant is satisfied if all three of the criteria are fulfilled.

| Criteria | Fulfilled? | |
|---|--------------------------|--------------------------|
| | Yes | No |
| 1. There are a minimum of 20 school children during the highest crossing hour. | <input type="checkbox"/> | <input type="checkbox"/> |
| 2. There are fewer adequate gaps in the major road traffic stream during the period when the school children are using the crossing than the number of minutes in the same period. | <input type="checkbox"/> | <input type="checkbox"/> |
| 3. The nearest traffic signal along the major road is located more than 300 ft away. Or, the nearest traffic signal is within 300 ft but the proposed traffic signal will not restrict the progressive movement of traffic. | <input type="checkbox"/> | <input type="checkbox"/> |

Satisfied?: N/A

TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

Sheet 4

Warrant 6 – Coordinated Signal System

Indicate if the criteria are fulfilled in the boxes provided. The warrant is satisfied if either criterion is fulfilled. This warrant should not be applied when the resulting signal spacing would be less than 1000 ft.

| Criteria | Fulfilled? | |
|--|--------------------------|--------------------------|
| | Yes | No |
| 1. On a one-way road or a road that has traffic predominantly in one direction, the adjacent signals are so far apart that they do not provide the necessary degree of vehicle platooning. | <input type="checkbox"/> | <input type="checkbox"/> |
| 2. On a two-way road, adjacent signals do not provide the necessary degree of platooning and the proposed and adjacent signals will collectively provide a progressive operation. | <input type="checkbox"/> | <input type="checkbox"/> |

Satisfied?: N/A

Warrant 7 – Crash Experience

The warrant is satisfied if all three of the criteria are fulfilled.

| Criteria (Must use 80% - Urban - Condition Warrant Volume Levels) | | Met? | | Fulfilled? | |
|--|---|--------------------------|--------------------------|--------------------------|--------------------------|
| | | Yes | No | Yes | No |
| A. Adequate trial of other remedial measures has failed to reduce crash frequency. | Measures tried: | | | <input type="checkbox"/> | <input type="checkbox"/> |
| B. Five or more reported crashes, of types susceptible to correction by signal, have occurred within a 12-mo period. | Number of crashes per 12 months: | | | <input type="checkbox"/> | <input type="checkbox"/> |
| C. One of the warrants to the right is met. | Warrant 1, Condition A (80% satisfied from Table 1 above) | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| | Warrant 1, Condition B (80% satisfied from Table 1 above) | <input type="checkbox"/> | <input type="checkbox"/> | | |
| | Warrant 4, Criterion A (80% satisfied above) | <input type="checkbox"/> | <input type="checkbox"/> | | |
| | Warrant 4, Criterion B (80% satisfied above) | <input type="checkbox"/> | <input type="checkbox"/> | | |

Table 1: 80% Volume Comparison Criteria for Warrant 1

| (Volumes in veh/h) | | Minimum Requirements | | | |
|-----------------------------|----|----------------------|-------|------------------|-------|
| Approach Lanes: | | 1 | | 2 or more | |
| Volume Level: | | 80% | Hours | 80% | Hours |
| Major Road Both App. vph | 1A | 280 | | 336 | |
| | 1B | 420 | | 504 | |
| Minor Road High App. vph | 1A | 84 | | 112 | |
| | 1B | 42 | | 56 | |

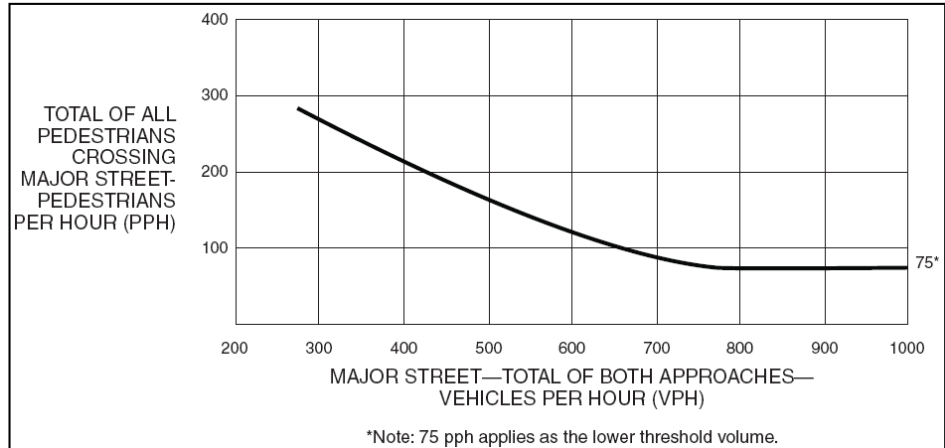
TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

Sheet 5

Criterion 4A

Plot four volume combinations on the applicable figure below. Draw vertical line for each of the four major road volumes. Where this line meets the graphed line, draw horizontal line to determine the minimum pedestrian volume to meet the warrant for this major road volume. Enter that value as the "Graph Ped. Volume." Multiply the "Graph Ped. Volume" by 0.8. Enter this new value as the "80% of Graphed Ped. Volume." If your actual "Pedestrian Volume" value exceeds the "80% of Graphed Ped. Volume" for each of the four hours, the 80% warrant is met.

| | | | | |
|--------------------------|--|--|--|--|
| Hour | | | | |
| Major Vol. | | | | |
| Ped. Vol. | | | | |
| Graphed Ped. Vol. | | | | |
| 80% of Graphed Ped. Vol. | | | | |



Criterion A Satisfied?:

N/A

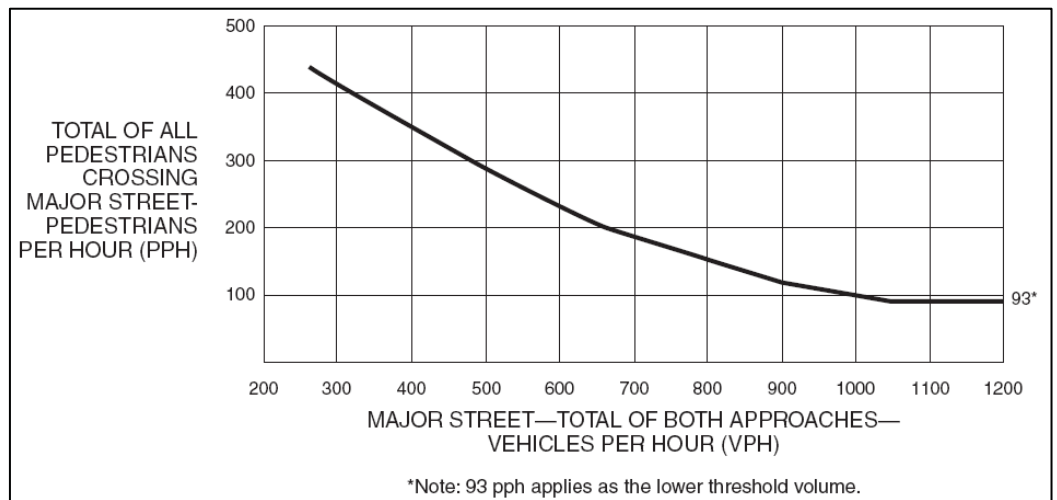
Warrant Satisfied?:

N/A

Criterion 4B

Plot and establish the pedestrian volumes for the peak hour as explained in Criterion 4A.

| | |
|---------------------------|--|
| Hour | |
| Major Vol. | |
| Ped. Vol. | |
| Graph Ped. Volume | |
| 80% of Graphed Ped Volume | |



Criterion B Satisfied?:

N/A

Warrant Satisfied?:

N/A

TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

Sheet 6

Warrant 8 – Roadway Network

Record hours where criteria are fulfilled, the corresponding volume, and other information in the boxes provided. The warrant is satisfied if at least one of the criteria is fulfilled and if all intersecting routes have one or more of the characteristics listed.

| Criteria | | | | | | | Met? | | Fulfilled? | |
|--|---|--|-----------------------|--|--|--|--------------------------|--------------------------|--------------------------|--------------------------|
| | | | | | | | Yes | No | Yes | No |
| 1. Both of the criteria to the right are met. | a. Total entering volume of at least 1,000 veh/h during typical weekday peak hour. | | Entering volume: | | | | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| | b. Five-year projected volumes that satisfy one or more of Warrants 1, 2, or 3. | | Warrant(s) satisfied: | | | | <input type="checkbox"/> | <input type="checkbox"/> | | |
| 2. Total entering volume at least 1,000 veh/h for each of any 5 hrs of a non-normal business day (Sat. or Sun.) | | | | | | | -Hr. | | <input type="checkbox"/> | <input type="checkbox"/> |
| | | | | | | | -Vol. | | | |
| Characteristics of Major Routes | | | | | | | | | Fulfilled? | |
| | | | | | | | | | Yes | No |
| 1. Part of the road or highway system that serves as the principal roadway network for through traffic flow. | | | | | | | | | <input type="checkbox"/> | <input type="checkbox"/> |
| 2. Rural or suburban highway outside of, entering, or traversing a city. | | | | | | | | | <input type="checkbox"/> | <input type="checkbox"/> |
| 3. Appears as a major route on an official plan. | | | | | | | | | <input type="checkbox"/> | <input type="checkbox"/> |

Warrant Satisfied?: N/A

Warrant 9 – Intersection Near a Grade Crossing

Plot the peak hour volume combination on the applicable figure below. Use curve for D (where D = Clear Storage Distance as defined in 1A.13) that is nearest to the actual distance.

| | |
|---------------------|-------|
| Hour | 16:00 |
| Major Vol. | 1142 |
| Minor Vol. | 195 |
| Adjusted Minor Vol. | |

| Adjustment Factors Applied | |
|----------------------------|--|
| Rail Traffic | |
| % Buses | |
| % Trucks | |

| Adjustment Factor for Daily Frequency of Rail Traffic | |
|---|-------------------|
| Rail Traffic per Day | Adjustment Factor |
| 1 | 0.67 |
| 2 | 0.91 |
| 3 to 5 | 1.00 |
| 6 to 8 | 1.18 |
| 9 to 11 | 1.25 |
| 12 or more | 1.33 |

| Adjustment Factor for Percentage of High-Occupancy Buses | |
|--|-------------------|
| % of High-Occupancy Buses* on Minor-Street Approach | Adjustment Factor |
| 0% | 1.00 |
| 2% | 1.09 |
| 4% | 1.19 |
| 6% or more | 1.32 |

* A high-occupancy bus is defined as a bus occupied by at least 20 people.

| Adjustment Factor for Percentage of Tractor-Trailer Trucks | | |
|--|---------------------|----------------------|
| % of Tractor-Trailer Trucks on Minor-Street Approach | Adjustment Factor | |
| | D less than 70 feet | D of 70 feet or more |
| 0% to 2.5% | 0.50 | 0.50 |
| 2.6% to 7.5% | 0.75 | 0.75 |
| 7.6% to 12.5% | 1.00 | 1.00 |
| 12.6% to 17.5% | 2.30 | 1.15 |
| 17.6% to 22.5% | 2.70 | 1.35 |
| 22.6% to 27.5% | 3.28 | 1.64 |
| More than 27.5% | 4.18 | 2.09 |

TRAFFIC SIGNAL WARRANT ANALYSIS WORKSHEET

Sheet 7

Figure 4C-9 – One Approach Lane at the Track Crossing

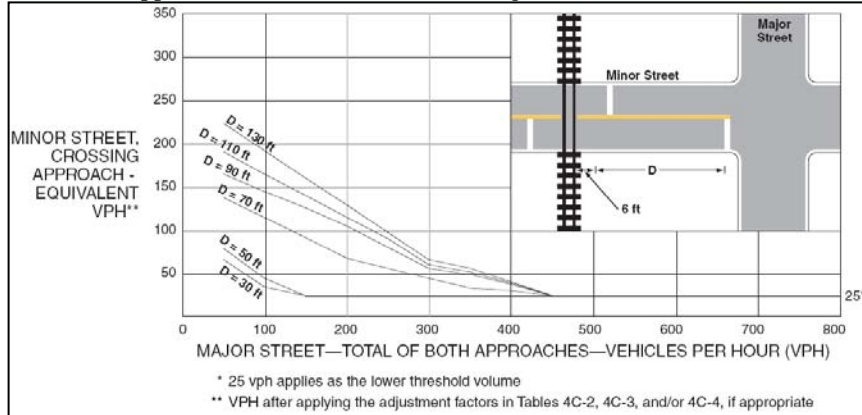
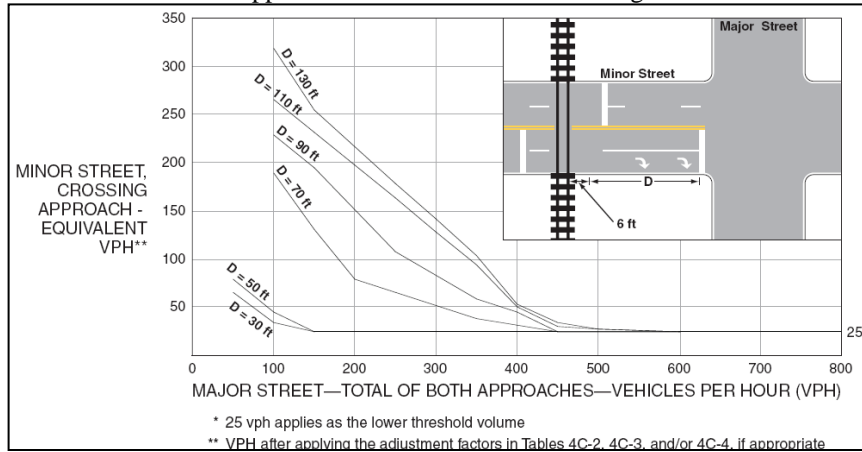


Figure 4C-10 – Two or More Approach Lanes at the Track Crossing



Warrant Satisfied?: N/A

CONCLUSIONS:

Warrant 1A (Minimum Vehicular Volume) and warrant 1C (Combination of condition A and B) as well as Warrant 2 (Four Hour Volume) are met for the installation of a traffic signal. No other warrants were evaluated.







Appendix E

Operational Modeling Output

HCM Unsignalized Intersection Capacity Analysis

5: Wisconsin-American Drive & STH 23







2015 AM Stop
STH 23

| | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|------|------|
| |  |  |  |  |  |  | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | ↑↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ | | |
| Volume (veh/h) | 499 | 148 | 18 | 746 | 28 | 4 | | |
| Sign Control | Free | | | Free | Stop | | | |
| Grade | 0% | | | 0% | 0% | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | |
| Hourly flow rate (vph) | 542 | 161 | 20 | 811 | 30 | 4 | | |
| Pedestrians | | | | | | | | |
| Lane Width (ft) | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | |
| Percent Blockage | | | | | | | | |
| Right turn flare (veh) | | | | | | | | |
| Median type | None | | | None | | | | |
| Median storage veh) | | | | | | | | |
| Upstream signal (ft) | 1038 | | | | | | | |
| pX, platoon unblocked | | | | | | | | |
| vC, conflicting volume | | | 703 | | | 987 | 271 | |
| vC1, stage 1 conf vol | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | |
| vCu, unblocked vol | | | 703 | | | 987 | 271 | |
| tC, single (s) | | | 4.3 | | | 6.8 | 6.9 | |
| tC, 2 stage (s) | | | | | | | | |
| tF (s) | | | 2.3 | | | 3.5 | 3.3 | |
| p0 queue free % | | | 98 | | | 87 | 99 | |
| cM capacity (veh/h) | | | 839 | | | 239 | 727 | |
| Direction, Lane # | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | NB 2 |
| Volume Total | 271 | 271 | 161 | 20 | 405 | 405 | 30 | 4 |
| Volume Left | 0 | 0 | 0 | 20 | 0 | 0 | 30 | 0 |
| Volume Right | 0 | 0 | 161 | 0 | 0 | 0 | 0 | 4 |
| cSH | 1700 | 1700 | 1700 | 839 | 1700 | 1700 | 239 | 727 |
| Volume to Capacity | 0.16 | 0.16 | 0.09 | 0.02 | 0.24 | 0.24 | 0.13 | 0.01 |
| Queue Length 95th (ft) | 0 | 0 | 0 | 2 | 0 | 0 | 11 | 0 |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 9.4 | 0.0 | 0.0 | 22.3 | 10.0 |
| Lane LOS | | | | A | | | C | A |
| Approach Delay (s) | 0.0 | | | | 0.2 | | 20.7 | |
| Approach LOS | | | | | | | C | |
| Intersection Summary | | | | | | | | |
| Average Delay | | | 0.6 | | | | | |
| Intersection Capacity Utilization | | | 30.6% | | ICU Level of Service | | | A |
| Analysis Period (min) | | | 15 | | | | | |
| | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Wisconsin-American Drive & STH 23







2015 PM Stop Control
STH 23

| |  |  |  |  |  |  | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|------|------|--|--|--|--|--|--|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | | | | | | | |
| Lane Configurations | ↑↑ | ↑ | ↵ | ↑↑ | ↵ | ↑ | | | | | | | | |
| Volume (veh/h) | 681 | 98 | 20 | 525 | 208 | 31 | | | | | | | | |
| Sign Control | Free | | | Free | Stop | | | | | | | | | |
| Grade | 0% | | | 0% | 0% | | | | | | | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | | | | | | | |
| Hourly flow rate (vph) | 702 | 101 | 21 | 541 | 214 | 32 | | | | | | | | |
| Pedestrians | | | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | | | |
| Median type | None | | | None | | | | | | | | | | |
| Median storage (veh) | | | | | | | | | | | | | | |
| Upstream signal (ft) | 1038 | | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | | | |
| vC, conflicting volume | | | 803 | | 1014 | 351 | | | | | | | | |
| vC1, stage 1 conf vol | | | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | | | |
| vCu, unblocked vol | | | 803 | | 1014 | 351 | | | | | | | | |
| tC, single (s) | | | 4.3 | | 6.8 | 6.9 | | | | | | | | |
| tC, 2 stage (s) | | | | | | | | | | | | | | |
| tF (s) | | | 2.3 | | 3.5 | 3.3 | | | | | | | | |
| p0 queue free % | | | 97 | | 6 | 95 | | | | | | | | |
| cM capacity (veh/h) | | | 767 | | 229 | 645 | | | | | | | | |
| Direction, Lane # | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | NB 2 | | | | | | |
| Volume Total | 351 | 351 | 101 | 21 | 271 | 271 | 214 | 32 | | | | | | |
| Volume Left | 0 | 0 | 0 | 21 | 0 | 0 | 214 | 0 | | | | | | |
| Volume Right | 0 | 0 | 101 | 0 | 0 | 0 | 0 | 32 | | | | | | |
| cSH | 1700 | 1700 | 1700 | 767 | 1700 | 1700 | 229 | 645 | | | | | | |
| Volume to Capacity | 0.21 | 0.21 | 0.06 | 0.03 | 0.16 | 0.16 | 0.94 | 0.05 | | | | | | |
| Queue Length 95th (ft) | 0 | 0 | 0 | 2 | 0 | 0 | 203 | 4 | | | | | | |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 9.8 | 0.0 | 0.0 | 89.6 | 10.9 | | | | | | |
| Lane LOS | | | | A | | | | B | | | | | | |
| Approach Delay (s) | 0.0 | | 0.4 | | | | 79.4 | | | | | | | |
| Approach LOS | | | | | | | F | | | | | | | |
| Intersection Summary | | | | | | | | | | | | | | |
| Average Delay | 12.3 | | | | | | | | | | | | | |
| Intersection Capacity Utilization | 37.0% | | ICU Level of Service | | A | | | | | | | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Wisconsin-American Drive & STH 23

2035 AM Stop
STH 23

| | | | | | | | | |
|-----------------------------------|---|---|---|---|---|---|------|------|
| |  |  |  |  |  |  | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | ↑↑ | ↑ | ↓ | ↑↑ | ↓ | ↑ | | |
| Volume (veh/h) | 653 | 194 | 23 | 933 | 37 | 5 | | |
| Sign Control | Free | | | Free | Stop | | | |
| Grade | 0% | | | 0% | 0% | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | |
| Hourly flow rate (vph) | 710 | 211 | 25 | 1014 | 40 | 5 | | |
| Pedestrians | | | | | | | | |
| Lane Width (ft) | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | |
| Percent Blockage | | | | | | | | |
| Right turn flare (veh) | | | | | | | | |
| Median type | None | | | None | | | | |
| Median storage (veh) | | | | | | | | |
| Upstream signal (ft) | 1038 | | | | | | | |
| pX, platoon unblocked | | | | | | | | |
| vC, conflicting volume | | | 921 | | | 1267 | 355 | |
| vC1, stage 1 conf vol | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | |
| vCu, unblocked vol | | | 921 | | | 1267 | 355 | |
| tC, single (s) | | | 4.3 | | | 6.8 | 6.9 | |
| tC, 2 stage (s) | | | | | | | | |
| tF (s) | | | 2.3 | | | 3.5 | 3.3 | |
| p0 queue free % | | | 96 | | | 74 | 99 | |
| cM capacity (veh/h) | | | 689 | | | 155 | 641 | |
| Direction, Lane # | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | NB 2 |
| Volume Total | 355 | 355 | 211 | 25 | 507 | 507 | 40 | 5 |
| Volume Left | 0 | 0 | 0 | 25 | 0 | 0 | 40 | 0 |
| Volume Right | 0 | 0 | 211 | 0 | 0 | 0 | 0 | 5 |
| cSH | 1700 | 1700 | 1700 | 689 | 1700 | 1700 | 155 | 641 |
| Volume to Capacity | 0.21 | 0.21 | 0.12 | 0.04 | 0.30 | 0.30 | 0.26 | 0.01 |
| Queue Length 95th (ft) | 0 | 0 | 0 | 3 | 0 | 0 | 25 | 1 |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 10.4 | 0.0 | 0.0 | 36.2 | 10.7 |
| Lane LOS | | | | B | | E | | B |
| Approach Delay (s) | 0.0 | | | 0.3 | | 33.2 | | |
| Approach LOS | | | | | | D | | |
| Intersection Summary | | | | | | | | |
| Average Delay | | | 0.9 | | | | | |
| Intersection Capacity Utilization | | | 35.8% | | ICU Level of Service | | A | |
| Analysis Period (min) | | | 15 | | | | | |
| | | | | | | | | |

HCM Unsignalized Intersection Capacity Analysis

5: Wisconsin-American Drive & STH 23

2035 PM Stop
STH 23

| | | | | | | | | |
|-----------------------------------|------|------|-------|------|----------------------|-------|-------|------|
| | → | ↘ | ↙ | ← | ↖ | ↗ | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR | | |
| Lane Configurations | ↑↑ | ↑↗ | ↙ | ↑↑ | ↙ | ↑↗ | | |
| Volume (veh/h) | 871 | 126 | 26 | 676 | 276 | 42 | | |
| Sign Control | Free | | | Free | Stop | | | |
| Grade | 0% | | | 0% | 0% | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | |
| Hourly flow rate (vph) | 898 | 130 | 27 | 697 | 285 | 43 | | |
| Pedestrians | | | | | | | | |
| Lane Width (ft) | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | |
| Percent Blockage | | | | | | | | |
| Right turn flare (veh) | | | | | | | | |
| Median type | None | | | None | | | | |
| Median storage veh | | | | | | | | |
| Upstream signal (ft) | 1038 | | | | | | | |
| pX, platoon unblocked | | | 0.97 | | 0.97 | 0.97 | | |
| vC, conflicting volume | | | 1028 | | 1300 | 449 | | |
| vC1, stage 1 conf vol | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | |
| vCu, unblocked vol | | | 967 | | 1247 | 370 | | |
| tC, single (s) | | | 4.3 | | 6.8 | 6.9 | | |
| tC, 2 stage (s) | | | | | | | | |
| tF (s) | | | 2.3 | | 3.5 | 3.3 | | |
| p0 queue free % | | | 96 | | 0 | 93 | | |
| cM capacity (veh/h) | | | 641 | | 154 | 608 | | |
| Direction, Lane # | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | NB 2 |
| Volume Total | 449 | 449 | 130 | 27 | 348 | 348 | 285 | 43 |
| Volume Left | 0 | 0 | 0 | 27 | 0 | 0 | 285 | 0 |
| Volume Right | 0 | 0 | 130 | 0 | 0 | 0 | 0 | 43 |
| cSH | 1700 | 1700 | 1700 | 641 | 1700 | 1700 | 154 | 608 |
| Volume to Capacity | 0.26 | 0.26 | 0.08 | 0.04 | 0.20 | 0.20 | 1.85 | 0.07 |
| Queue Length 95th (ft) | 0 | 0 | 0 | 3 | 0 | 0 | 534 | 6 |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 10.9 | 0.0 | 0.0 | 456.5 | 11.4 |
| Lane LOS | | | | B | | F | | B |
| Approach Delay (s) | 0.0 | | | 0.4 | | 397.7 | | |
| Approach LOS | | | | | | F | | |
| Intersection Summary | | | | | | | | |
| Average Delay | | | 62.8 | | | | | |
| Intersection Capacity Utilization | | | 46.0% | | ICU Level of Service | | A | |
| Analysis Period (min) | | | 15 | | | | | |
| | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Wisconsin-American Drive & STH 23

2015 AM Traffic Signal
STH 23

| | → | ↘ | ↙ | ← | ↖ | ↗ |
|-----------------------------------|------|------|-------|-------|----------------------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | ↑ | ↘ | ↑↑ | ↘ | ↑ |
| Volume (vph) | 499 | 148 | 18 | 746 | 28 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 5.0 |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3282 | 1468 | 1641 | 3282 | 1770 | 1583 |
| Flt Permitted | 1.00 | 1.00 | 0.45 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3282 | 1468 | 777 | 3282 | 1770 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 542 | 161 | 20 | 811 | 30 | 4 |
| RTOR Reduction (vph) | 0 | 54 | 0 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 542 | 107 | 20 | 811 | 30 | 0 |
| Heavy Vehicles (%) | 10% | 10% | 10% | 10% | 2% | 2% |
| Turn Type | NA | Perm | Perm | NA | NA | Perm |
| Protected Phases | 2 | | | 6 | 4 | |
| Permitted Phases | | 2 | 6 | | | 4 |
| Actuated Green, G (s) | 29.8 | 29.8 | 29.8 | 29.8 | 3.2 | 3.2 |
| Effective Green, g (s) | 29.8 | 29.8 | 29.8 | 29.8 | 3.2 | 3.2 |
| Actuated g/C Ratio | 0.66 | 0.66 | 0.66 | 0.66 | 0.07 | 0.07 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 2173 | 972 | 515 | 2173 | 126 | 113 |
| v/s Ratio Prot | 0.17 | | | c0.25 | c0.02 | |
| v/s Ratio Perm | | 0.07 | 0.03 | | | 0.00 |
| v/c Ratio | 0.25 | 0.11 | 0.04 | 0.37 | 0.24 | 0.00 |
| Uniform Delay, d1 | 3.1 | 2.8 | 2.6 | 3.4 | 19.7 | 19.4 |
| Progression Factor | 0.46 | 0.16 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.3 | 0.2 | 0.0 | 0.1 | 1.0 | 0.0 |
| Delay (s) | 1.7 | 0.7 | 2.7 | 3.5 | 20.7 | 19.4 |
| Level of Service | A | A | A | A | C | B |
| Approach Delay (s) | 1.4 | | | 3.5 | 20.6 | |
| Approach LOS | A | | | A | C | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 2.9 | | HCM Level of Service | A |
| HCM Volume to Capacity ratio | | | 0.36 | | | |
| Actuated Cycle Length (s) | | | 45.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 37.3% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

5: Wisconsin-American Drive & STH 23

2035 PM Signal
STH 23

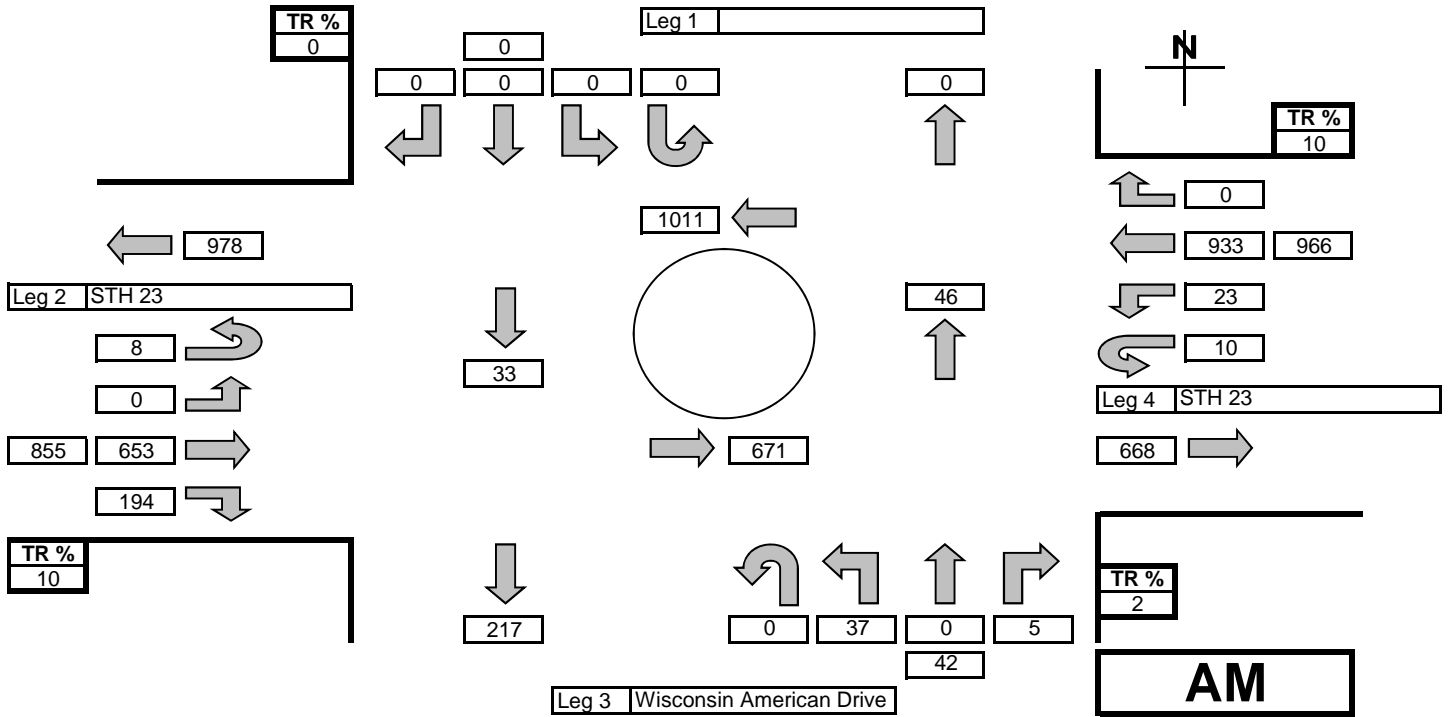
| | → | ↘ | ↙ | ← | ↖ | ↗ |
|-----------------------------------|-------|------|-------|------|----------------------|------|
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | ↑ | ↘ | ↑↑ | ↘ | ↑ |
| Volume (vph) | 871 | 126 | 26 | 676 | 276 | 42 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 5.0 |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3282 | 1468 | 1641 | 3282 | 1770 | 1583 |
| Flt Permitted | 1.00 | 1.00 | 0.30 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3282 | 1468 | 510 | 3282 | 1770 | 1583 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 898 | 130 | 27 | 697 | 285 | 43 |
| RTOR Reduction (vph) | 0 | 64 | 0 | 0 | 0 | 32 |
| Lane Group Flow (vph) | 898 | 66 | 27 | 697 | 285 | 11 |
| Heavy Vehicles (%) | 10% | 10% | 10% | 10% | 2% | 2% |
| Turn Type | NA | Perm | Perm | NA | NA | Perm |
| Protected Phases | 2 | | | 6 | 4 | |
| Permitted Phases | | 2 | 6 | | | 4 |
| Actuated Green, G (s) | 25.4 | 25.4 | 25.4 | 25.4 | 12.6 | 12.6 |
| Effective Green, g (s) | 25.4 | 25.4 | 25.4 | 25.4 | 12.6 | 12.6 |
| Actuated g/C Ratio | 0.51 | 0.51 | 0.51 | 0.51 | 0.25 | 0.25 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 1667 | 746 | 259 | 1667 | 446 | 399 |
| v/s Ratio Prot | c0.27 | | | 0.21 | c0.16 | |
| v/s Ratio Perm | | 0.04 | 0.05 | | | 0.01 |
| v/c Ratio | 0.54 | 0.09 | 0.10 | 0.42 | 0.64 | 0.03 |
| Uniform Delay, d1 | 8.3 | 6.3 | 6.4 | 7.7 | 16.7 | 14.1 |
| Progression Factor | 0.84 | 1.07 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 1.2 | 0.2 | 0.8 | 0.8 | 3.0 | 0.0 |
| Delay (s) | 8.2 | 7.0 | 7.2 | 8.5 | 19.7 | 14.1 |
| Level of Service | A | A | A | A | B | B |
| Approach Delay (s) | 8.0 | | | 8.4 | 18.9 | |
| Approach LOS | A | | | A | B | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 9.9 | | HCM Level of Service | A |
| HCM Volume to Capacity ratio | | | 0.57 | | | |
| Actuated Cycle Length (s) | | | 50.0 | | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | | | 49.4% | | ICU Level of Service | A |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

Roundabout Summary

Project: Wisconsin American Drive
Project No.: 1440-15-01
Intersection: STH 23-Wisconsin American
Time Period: AM Peak

Drawn By:

Sheet **of**



Capacity Guidelines for Single Lane

1. Single lane service volumes
< 900 vph - 1200 vph
2. Exit Flow < 900 vph - 1200 vph
3. Entry Flow + Circulating Flow
< 1400 vph - 1800 vph
4. Circulating Flow downstream of on Entry
1400 vph - 1800 vph
5. $V/C > 0.85$

| Rodel Inputs | | | | | | |
|--------------|--------------------------|------|-----|-----|----|----|
| Leg | Street Name | PCU | RT | TH | LT | UT |
| 1 | 0 | 1.00 | 0 | 0 | 0 | 0 |
| 2 | STH 23 | 1.10 | 194 | 653 | 0 | 8 |
| 3 | Wisconsin American Drive | 1.02 | 5 | 0 | 37 | 0 |
| 4 | STH 23 | 1.10 | 0 | 933 | 23 | 10 |

Right Turn Bypass
None

Right Turn Bypass
None

Right Turn Bypass
None

Right Turn Bypass
None

STH 23 and Wisconsin-American Drive Roundabout Analysis

AM Design Year 2035

Dual Lane Eastbound & Westbound STH 23, Single Lane Wisconsin-American

50% Confidence Level

| | | | | | | | | | | | | |
|-----------------|----------|--------|--------------------------|--------------------------|---------|--------|------------|--------|----------------|-----------|----------|-----|
| 31:5:12 | | | | STH23 WISCONSIN AMERICAN | | | | 15 | | | | |
| E | (m) | 8.00 | 4.25 | 8.00 | | | | | TIME PERIOD | min | 90 | |
| L' | (m) | 40.00 | 40.00 | 40.00 | | | | | TIME SLICE | min | 15 | |
| V | (m) | 7.30 | 3.65 | 7.30 | | | | | RESULTS PERIOD | min | 15 75 | |
| RAD | (m) | 20.00 | 20.00 | 20.00 | | | | | TIME COST | \$/hr | 15.00 | |
| PHI | (d) | 25.00 | 25.00 | 25.00 | | | | | FLOW PERIOD | min | 15 75 | |
| DIA | (m) | 50.00 | 45.00 | 50.00 | | | | | FLOW TYPE | pcu/veh | VEH | |
| GRAD SEP | | 0 | 0 | 0 | | | | | FLOW PEAK | am/op/pm | AM | |
| | | | | | | | | | | | | |
| LEG NAME | | PCU | TURNS (1st exit, 2nd..U) | | FLOF | CL | FLOW RATIO | | | FLOW TIME | | |
| STH 23 EB | | 1.10 | 194 | 653 | 0 | 1.00 | 50 | 0.75 | 1.125 | 0.75 | 15 45 75 | |
| WISC AMER | | 1.02 | 005 | 037 | 0 | 1.00 | 50 | 0.75 | 1.125 | 0.75 | 15 45 75 | |
| STH 23 WB | | 1.10 | 933 | 023 | 0 | 1.00 | 50 | 0.75 | 1.125 | 0.75 | 15 45 75 | |
| | | | | | | | | | | | | |
| L' < 5 when VaE | | | | | | | | | | | | |
| FLOW | | veh | 847 | 42 | 956 | | | | | AVEDEL | s | 2.8 |
| CAPACITY | | veh | 2214 | 885 | 2206 | | | | | LOS SIG | A | |
| AVE DELAY | | secs | 2.6 | 4.2 | 2.8 | | | | | LOS UNSIG | A | |
| MAX DELAY | | secs | 3.4 | 5.5 | 3.8 | | | | | | | |
| AVE QUEUE | | veh | 1 | 0 | 1 | | | | | VEHIC HRS | 1.4 | |
| MAX QUEUE | | veh | 1 | 0 | 1 | | | | | COST | \$ | 21 |
| | | | | | | | | | | | | |
| F1mode | F2direct | F3peak | CtrlF3rev | F4fact | F6stats | F8econ | F9prnt | F10run | Esc | | | |

| | EB | NB | WB | Intersection |
|-----------------------------------|-------------|-------------|-------------|--------------|
| Average Stopped Delay(from above) | 2.6 | 4.2 | 2.8 | 2.8 |
| Geometric Delay | 14 | 9 | 14 | 14 |
| Total Delay | 16.6 | 13.2 | 16.8 | 16.8 |
| Level of Service (LOS) | B | B | B | B |
| 95% Queue (from next page) | 50 | 50 | 75 | |

85% Confidence Level

| | | | | | | | | | | | |
|--|-------|--------------------------|-------|--------------------------|------|----|------------|----------------|-----------|-----------|-------|
| 31:5:12 | | | | STH23 WISCONSIN AMERICAN | | | | 18 | | | |
| E (m) | 8.00 | 4.25 | 8.00 | | | | | TIME PERIOD | min | 90 | |
| L' (m) | 40.00 | 40.00 | 40.00 | | | | | TIME SLICE | min | 15 | |
| V (m) | 7.30 | 3.65 | 7.30 | | | | | RESULTS PERIOD | min | 15 | 75 |
| RAD (m) | 20.00 | 20.00 | 20.00 | | | | | TIME COST | \$/hr | 15.00 | |
| PHI (d) | 25.00 | 25.00 | 25.00 | | | | | FLOW PERIOD | min | 15 | 75 |
| DIA (m) | 50.00 | 45.00 | 50.00 | | | | | FLOW TYPE | pcu/veh | VEH | |
| GRAD SEP | 0 | 0 | 0 | | | | | FLOW PEAK | am/op/pm | AM | |
| | | | | | | | | | | | |
| LEG NAME | PCU | TURNS (1st exit, 2nd..U) | | | FLOF | CL | FLOW RATIO | | | FLOW TIME | |
| STH 23 EB | 1.10 | 194 | 653 | 0 | 1.00 | 85 | 0.75 | 1.125 | 0.75 | 15 | 45 75 |
| WISC AMER | 1.02 | 005 | 037 | 0 | 1.00 | 85 | 0.75 | 1.125 | 0.75 | 15 | 45 75 |
| STH 23 WB | 1.10 | 933 | 023 | 0 | 1.00 | 85 | 0.75 | 1.125 | 0.75 | 15 | 45 75 |
| | | | | | | | | | | | |
| L' < 5 when VaE | | | | | | | | | | | |
| FLOW | veh | 847 | 42 | 956 | | | | | AVEDEL | s | 3.2 |
| CAPACITY | veh | 2026 | 682 | 2017 | | | | | LOS SIG | A | |
| AVE DELAY | secs | 3.0 | 5.5 | 3.3 | | | | | LOS UNSIG | A | |
| MAX DELAY | secs | 4.0 | 7.3 | 4.6 | | | | | VEHIC HRS | 1.7 | |
| AVE QUEUE | veh | 1 | 0 | 1 | | | | | COST | \$ | 25 |
| MAX QUEUE | veh | 1 | 0 | 1 | | | | | | | |
| F1mode F2direct F3peak CtrlF3rev F4fact F6stats F8econ F9prnt F10run Esc | | | | | | | | | | | |

| | EB | NB | WB | Intersection |
|-----------------------------------|-----------|-------------|-----------|--------------|
| Average Stopped Delay(from above) | 3 | 5.5 | 3..3 | 3.2 |
| Geometric Delay | 14 | 9 | 14 | 14 |
| Total Delay | 17 | 14.5 | 14 | 17.2 |
| Level of Service (LOS) | B | B | B | B |

STH 23 and Wisconsin-American Drive Roundabout Analysis

AM Design Year 2035

Dual Lane Eastbound & Westbound STH 23, Single Lane Wisconsin-American

Queue Length Outputs

Eastbound STH 23

| 31:5:12 | | STH23 WISCONSIN AMERI | | | | | | 15 |
|-------------|--|-----------------------|-------------|-------------------|----------|-----------------|-----------------|---------------------|
| AM | | LEG NUMBER 1 | | | | | | STH 23 EB |
| TIME SLICES | | ARR FLOW v/slice | CAP v/slice | CIRC FLOW v/slice | VC RATIO | END QUEUES vehs | 95% QUEUES vehs | EXIT FLOW veh/slice |
| 0 15 | | 159.42 | 554.60 | 4.32 | 0.287 | 0.40 | 1.05 | 181.56 |
| 15 30 | | 190.36 | 553.96 | 5.17 | 0.344 | 0.52 | 1.36 | 217.24 |
| 30 45 | | 233.14 | 553.08 | 6.32 | 0.422 | 0.72 | 1.88 | 265.98 |
| 45 60 | | 233.14 | 553.08 | 6.33 | 0.422 | 0.73 | 1.88 | 266.25 |
| 60 75 | | 190.36 | 553.96 | 5.18 | 0.344 | 0.53 | 1.37 | 217.68 |
| 75 90 | | 159.42 | 554.59 | 4.33 | 0.287 | 0.40 | 1.06 | 182.22 |

Northbound Wisconsin American Drive

| 31:5:12 | | STH23 WISCONSIN AMERI | | | | | | 15 |
|-------------|--|-----------------------|-------------|-------------------|----------|-----------------|-----------------|---------------------|
| AM | | LEG NUMBER 2 | | | | | | WISC AMER |
| TIME SLICES | | ARR FLOW v/slice | CAP v/slice | CIRC FLOW v/slice | VC RATIO | END QUEUES vehs | 95% QUEUES vehs | EXIT FLOW veh/slice |
| 0 15 | | 7.90 | 245.63 | 132.24 | 0.032 | 0.03 | 0.09 | 43.93 |
| 15 30 | | 9.44 | 231.22 | 158.18 | 0.041 | 0.04 | 0.11 | 52.56 |
| 30 45 | | 11.56 | 211.51 | 193.69 | 0.055 | 0.06 | 0.15 | 64.36 |
| 45 60 | | 11.56 | 211.41 | 193.84 | 0.055 | 0.06 | 0.15 | 64.41 |
| 60 75 | | 9.44 | 231.07 | 158.42 | 0.041 | 0.04 | 0.11 | 52.65 |
| 75 90 | | 7.90 | 245.39 | 132.63 | 0.032 | 0.03 | 0.09 | 44.08 |

Westbound STH 23

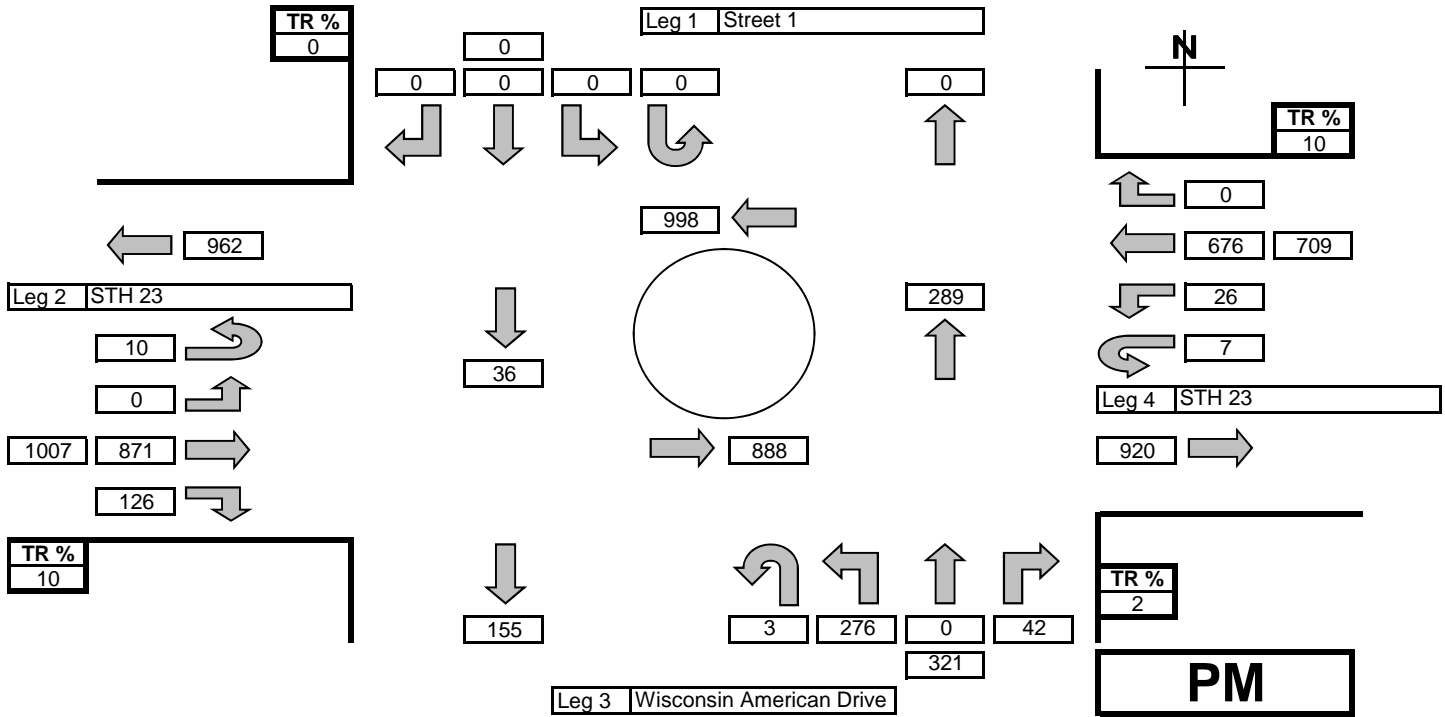
| 31:5:12 | | STH23 WISCONSIN AMERI | | | | | | 15 |
|-------------|--|-----------------------|-------------|-------------------|----------|-----------------|-----------------|---------------------|
| AM | | LEG NUMBER 3 | | | | | | STH 23 WB |
| TIME SLICES | | ARR FLOW v/slice | CAP v/slice | CIRC FLOW v/slice | VC RATIO | END QUEUES vehs | 95% QUEUES vehs | EXIT FLOW veh/slice |
| 0 15 | | 179.93 | 553.00 | 6.43 | 0.325 | 0.48 | 1.25 | 123.46 |
| 15 30 | | 214.86 | 552.04 | 7.70 | 0.389 | 0.63 | 1.65 | 147.71 |
| 30 45 | | 263.14 | 550.73 | 9.43 | 0.478 | 0.91 | 2.34 | 180.86 |
| 45 60 | | 263.14 | 550.72 | 9.44 | 0.478 | 0.91 | 2.35 | 181.02 |
| 60 75 | | 214.86 | 552.03 | 7.72 | 0.389 | 0.64 | 1.66 | 147.96 |
| 75 90 | | 179.93 | 552.98 | 6.46 | 0.325 | 0.48 | 1.26 | 123.87 |

Roundabout Summary

Project: Wisconsin American Drive
Project No.: 1440-15-01
Intersection: STH 23-Wisconsin American
Time Period: PM Peak

Drawn By:

Sheet **of**



Capacity Guidelines for Single Lane

1. Single lane service volumes
< 900 vph - 1200 vph
2. Exit Flow < 900 vph - 1200 vph
3. Entry Flow + Circulating Flow
< 1400 vph - 1800 vph
4. Circulating Flow downstream of on Entry
1400 vph - 1800 vph
5. $V/C > 0.85$

| Rodel Inputs | | | | | | |
|--------------|--------------------------|------|-----|-----|-----|----|
| Leg | Street Name | PCU | RT | TH | LT | UT |
| 1 | Street 1 | 1.00 | 0 | 0 | 0 | 0 |
| 2 | STH 23 | 1.10 | 126 | 871 | 0 | 10 |
| 3 | Wisconsin American Drive | 1.02 | 42 | 0 | 276 | 3 |
| 4 | STH 23 | 1.10 | 0 | 676 | 26 | 7 |

Right Turn Bypass
None

Right Turn Bypass
None

Right Turn Bypass
None

Right Turn Bypass
None

STH 23 and Wisconsin-American Drive Roundabout Analysis

PM Design Year 2035

Dual Lane Eastbound & Westbound STH 23, Single Lane Wisconsin-American

50% Confidence Level

| | | | | | | | | | | | |
|-----------------|----------|--------------------------|-----------|--------------------------|---------|------------|--------|----------|-----------|----------|--|
| 31:5:12 | | | | STH23 WISCONSIN AMERICAN | | | | 16 | | | |
| E (m) | 8.00 | 4.25 | 8.00 | TIME PERIOD | | | | min | 90 | | |
| L' (m) | 40.00 | 40.00 | 40.00 | TIME SLICE | | | | min | 15 | | |
| V (m) | 7.30 | 3.65 | 7.30 | RESULTS PERIOD | | | | min | 15 75 | | |
| RAD (m) | 20.00 | 20.00 | 20.00 | TIME COST | | | | \$/hr | 15.00 | | |
| PHI (d) | 25.00 | 25.00 | 25.00 | FLOW PERIOD | | | | min | 15 75 | | |
| DIA (m) | 50.00 | 45.00 | 50.00 | FLOW TYPE | | | | pcu/veh | VEH | | |
| GRAD SEP | 0 | 0 | 0 | FLOW PEAK | | | | am/op/pm | PM | | |
| | | | | | | | | | | | |
| LEG NAME | PCU | TURNS (1st exit, 2nd..U) | | FLOF | CL | FLOW RATIO | | | FLOW TIME | | |
| STH 23 EB | 1.10 | 126 | 871 | 0 | 1.00 | 50 | 0.75 | 1.125 | 0.75 | 15 45 75 | |
| WISC AMER | 1.02 | 042 | 276 | 0 | 1.00 | 50 | 0.75 | 1.125 | 0.75 | 15 45 75 | |
| STH 23 WB | 1.10 | 676 | 026 | 0 | 1.00 | 50 | 0.75 | 1.125 | 0.75 | 15 45 75 | |
| | | | | | | | | | | | |
| L' < 5 when VaE | | | | | | | | | | | |
| FLOW | veh | 997 | 318 | 702 | AVEDEL | | | | s | 3.7 | |
| CAPACITY | veh | 2212 | 755 | 2038 | LOS | | | | SIG | A | |
| AVE DELAY | secs | 2.9 | 8.4 | 2.7 | LOS | | | | UNSIG | A | |
| MAX DELAY | secs | 3.9 | 12.3 | 3.5 | VEHIC | | | | HRS | 2.1 | |
| AVE QUEUE | veh | 1 | 1 | 1 | COST | | | | \$ | 31 | |
| MAX QUEUE | veh | 1 | 1 | 1 | | | | | | | |
| F1mode | F2direct | F3peak | CtrlF3rev | F4fact | F6stats | F8econ | F9prnt | F10run | Esc | | |

| | EB | NB | WB | Intersection |
|-----------------------------------|-------------|-------------|-------------|--------------|
| Average Stopped Delay(from above) | 2.9 | 8.4 | 2.7 | 3.7 |
| Geometric Delay | 14 | 9 | 14 | 14 |
| Total Delay | 16.9 | 17.4 | 16.7 | 17.7 |
| Level of Service (LOS) | B | B | B | B |
| 95% Queue (from next page) | 75 | 75 | 50 | |

85% Confidence Level

| | | | | | | | | | | | |
|-----------------|----------|--------------------------|-----------|--------------------------|---------|------------|--------|----------------|-----------|---------|--|
| 31:5:12 | | | | STH23 WISCONSIN AMERICAN | | | | 17 | | | |
| E (m) | 8.00 | 4.25 | 8.00 | | | | | TIME PERIOD | min | 90 | |
| L' (m) | 40.00 | 40.00 | 40.00 | | | | | TIME SLICE | min | 15 | |
| V (m) | 7.30 | 3.65 | 7.30 | | | | | RESULTS PERIOD | min | 15 75 | |
| RAD (m) | 20.00 | 20.00 | 20.00 | | | | | TIME COST | \$/hr | 15.00 | |
| PHI (d) | 25.00 | 25.00 | 25.00 | | | | | FLOW PERIOD | min | 15 75 | |
| DIA (m) | 50.00 | 45.00 | 50.00 | | | | | FLOW TYPE | pcu/veh | VEH | |
| GRAD SEP | 0 | 0 | 0 | | | | | FLOW PEAK | am/op/pm | PM | |
| | | | | | | | | | | | |
| LEG NAME | PCU | TURNS (1st exit, 2nd..U) | | FLOF | CL | FLOW RATIO | | | FLOW TIME | | |
| STH 23 EB | 1.10 | 126 | 871 0 | 1.00 | 85 | 0.75 | 1.125 | 0.75 | 15 | 45 75 | |
| WISC AMER | 1.02 | 042 | 276 0 | 1.00 | 85 | 0.75 | 1.125 | 0.75 | 15 | 45 75 | |
| STH 23 WB | 1.10 | 676 | 026 0 | 1.00 | 85 | 0.75 | 1.125 | 0.75 | 15 | 45 75 | |
| | | | | | | | | | | | |
| L' < 5 when VaE | | | | | | | | | | | |
| FLOW | veh | 997 | 318 702 | | | | | | AVEDEL | s 5.5 | |
| CAPACITY | veh | 2024 | 552 1850 | | | | | | LOS | SIG A | |
| AVE DELAY | secs | 3.5 | 17.0 3.1 | | | | | | LOS | UNSIG A | |
| MAX DELAY | secs | 4.7 | 27.8 4.1 | | | | | | | | |
| AVE QUEUE | veh | 1 | 2 1 | | | | | | VEHIC | HRS 3.1 | |
| MAX QUEUE | veh | 1 | 2 1 | | | | | | COST | \$ 46 | |
| | | | | | | | | | | | |
| F1mode | F2direct | F3peak | CtrlF3rev | F4fact | F6stats | F8econ | F9prnt | F10run | Esc | | |

| | EB | NB | WB | Intersection |
|-----------------------------------|-------------|-----------|-------------|--------------|
| Average Stopped Delay(from above) | 3.5 | 17 | 3.1 | 5.5 |
| Geometric Delay | 14 | 9 | 14 | 14 |
| Total Delay | 17.5 | 26 | 17.1 | 19.5 |
| Level of Service (LOS) | B | C | B | C |

STH 23 and Wisconsin-American Drive Roundabout Analysis

PM Design Year 2035

Dual Lane Eastbound & Westbound STH 23, Single Lane Wisconsin-American
Queue Length Outputs

Eastbound STH 23

| 31:5:12 | | STH23 WISCONSIN AMERI | | | | | 19 |
|-------------|------------------|-----------------------|-------------------|----------|-----------------|-----------------|---------------------|
| PM | | LEG NUMBER 1 | | | | STH 23 EB | |
| TIME SLICES | ARR FLOW v/slice | CAP v/slice | CIRC FLOW v/slice | VC RATIO | END QUEUES vehs | 95% QUEUES vehs | EXIT FLOW veh/slice |
| 0 15 | 187.65 | 554.17 | 4.88 | 0.339 | 0.51 | 1.33 | 174.78 |
| 15 30 | 224.07 | 553.45 | 5.84 | 0.405 | 0.68 | 1.76 | 209.21 |
| 30 45 | 274.43 | 552.46 | 7.15 | 0.497 | 0.98 | 2.52 | 256.00 |
| 45 60 | 274.43 | 552.45 | 7.16 | 0.497 | 0.98 | 2.53 | 256.51 |
| 60 75 | 224.07 | 553.44 | 5.85 | 0.405 | 0.68 | 1.77 | 209.96 |
| 75 90 | 187.65 | 554.17 | 4.90 | 0.339 | 0.51 | 1.34 | 175.65 |

Northbound Wisconsin American Drive

| 31:5:12 | | STH23 WISCONSIN AMERI | | | | | 19 |
|-------------|------------------|-----------------------|-------------------|----------|-----------------|-----------------|---------------------|
| PM | | LEG NUMBER 2 | | | | | WISC AMER |
| TIME SLICES | ARR FLOW v/slice | CAP v/slice | CIRC FLOW v/slice | VC RATIO | END QUEUES vehs | 95% QUEUES vehs | EXIT FLOW veh/slice |
| 0 15 | 59.85 | 221.14 | 176.35 | 0.271 | 0.37 | 0.96 | 30.77 |
| 15 30 | 71.47 | 201.92 | 210.96 | 0.354 | 0.54 | 1.41 | 36.81 |
| 30 45 | 87.53 | 175.65 | 258.29 | 0.498 | 0.97 | 2.50 | 45.07 |
| 45 60 | 87.53 | 175.49 | 258.55 | 0.499 | 0.98 | 2.53 | 45.12 |
| 60 75 | 71.47 | 201.67 | 211.36 | 0.354 | 0.56 | 1.45 | 36.89 |
| 75 90 | 59.85 | 220.79 | 176.94 | 0.271 | 0.38 | 0.98 | 30.88 |

Westbound STH 23

| 31:5:12 | | STH23 WISCONSIN AMERI | | | | | | 19 |
|-------------|------------------|-----------------------|-------------------|----------|-----------------|-----------------|---------------------|-----------|
| PM | | LEG NUMBER 3 | | | | | | STH 23 WB |
| TIME SLICES | ARR FLOW v/slice | CAP v/slice | CIRC FLOW v/slice | VC RATIO | END QUEUES vehs | 95% QUEUES vehs | EXIT FLOW veh/slice | |
| 0 15 | 132.13 | 521.66 | 47.88 | 0.253 | 0.34 | 0.89 | 170.77 | |
| 15 30 | 157.77 | 514.47 | 57.38 | 0.307 | 0.44 | 1.15 | 204.34 | |
| 30 45 | 193.23 | 504.85 | 70.11 | 0.383 | 0.62 | 1.60 | 250.15 | |
| 45 60 | 193.23 | 504.59 | 70.44 | 0.383 | 0.62 | 1.61 | 250.46 | |
| 60 75 | 157.77 | 514.10 | 57.86 | 0.307 | 0.44 | 1.16 | 204.82 | |
| 75 90 | 132.13 | 521.32 | 48.31 | 0.253 | 0.34 | 0.89 | 171.43 | |

Appendix F

Cost Estimates

Wisconsin Department of Transportation
I.D. 1440-15-71
USH 151 - TAFT ROAD
WISCONSIN AMERICAN DRIVE INTERSECTION
STH 23
Preliminary Cost Estimate Summary

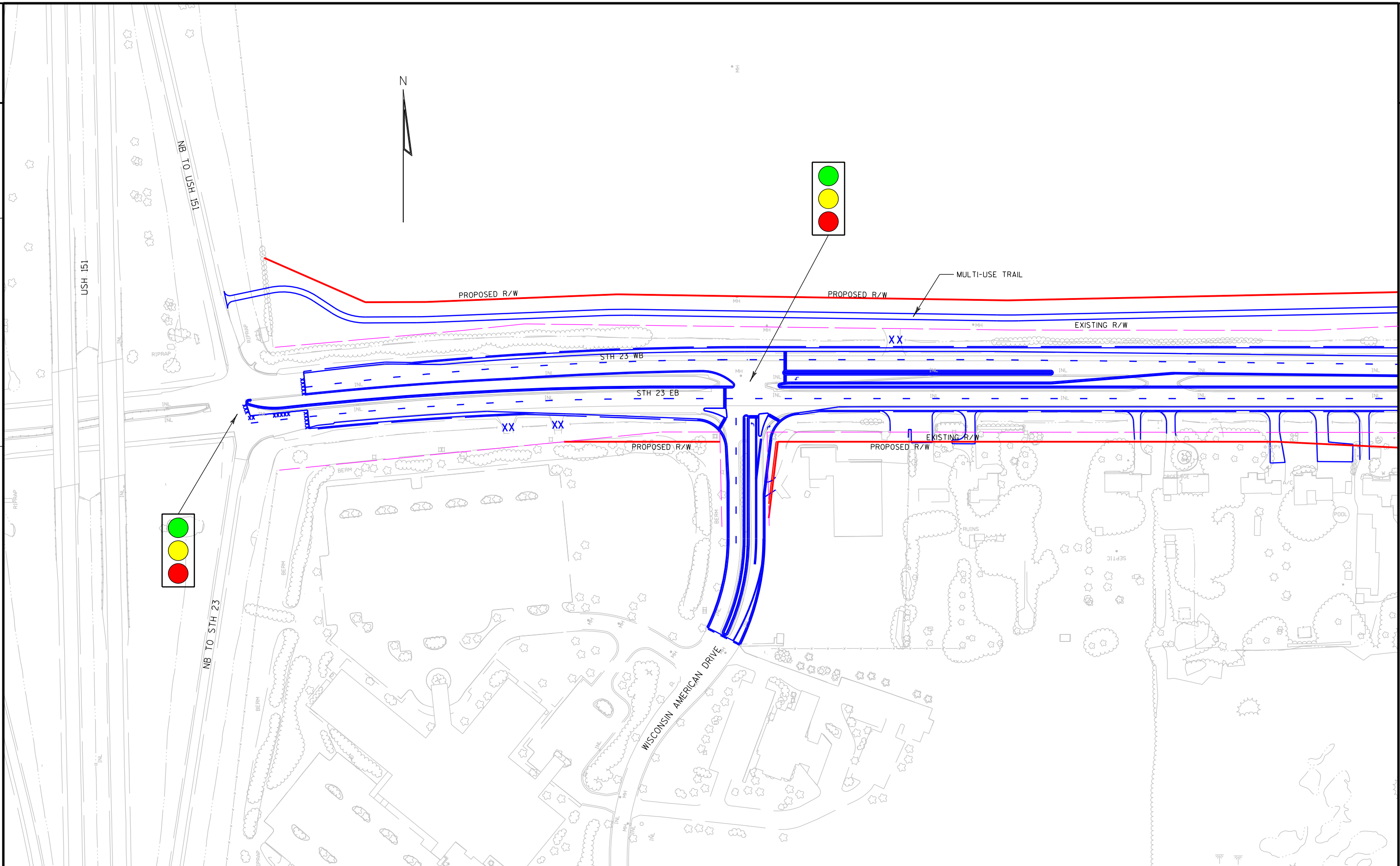
| ITEM DESCRIPTION | | | | TOTAL |
|---|------|--------------------|------------|-----------------------|
| ITEMS DETAILED | UNIT | QUANTITY | UNIT COST | TOTAL |
| HMA PAVEMENT | TN | 430 | \$40.00 | \$17,200.00 |
| CONCRETE PAVEMENT | SY | 14550 | \$30.00 | \$436,500.00 |
| ASPHALTIC MATERIALS (AC) | TN | 26 | \$375.00 | \$9,675.00 |
| BASE AGGREGATE DENSE | TN | 9160 | \$10.00 | \$91,600.00 |
| CURB & GUTTER | LF | 5600 | \$12.00 | \$67,200.00 |
| <i>Major Roadway Items Detailed Subtotalled</i> | | | | \$622,175.00 |
| | UNIT | QUANTITY | UNIT PRICE | |
| SIGNALIZE INTERSECTION | LS | 1 | \$150,000 | \$150,000.00 |
| DRAINAGE | LS | % of Major Item \$ | 20% | \$124,000.00 |
| EROSION CONTROL & RESTORATION | LS | % of Major Item \$ | 15% | \$93,000.00 |
| TRAFFIC CONTROL & STAGING | LS | % of Major Item \$ | 40% | \$249,000.00 |
| LIGHTING | EACH | 6 | 10,000 | \$60,000.00 |
| SIGNING/MARKING | LS | % of Major Item \$ | 6% | \$37,000.00 |
| ROADWAY INCIDENTALS | LS | % of Major Item \$ | 30% | \$187,000.00 |
| Construction Costs Subtotal | | | | \$1,522,175.00 |
| CONSTRUCTION DESIGN CONTINGENCY | LS | % of Constr. Costs | 15% | \$228,000.00 |
| ESTIMATED CONTRACT LET AMOUNT | | | | \$1,750,000.00 |
| TOTAL COST | | | | \$1,750,000 |

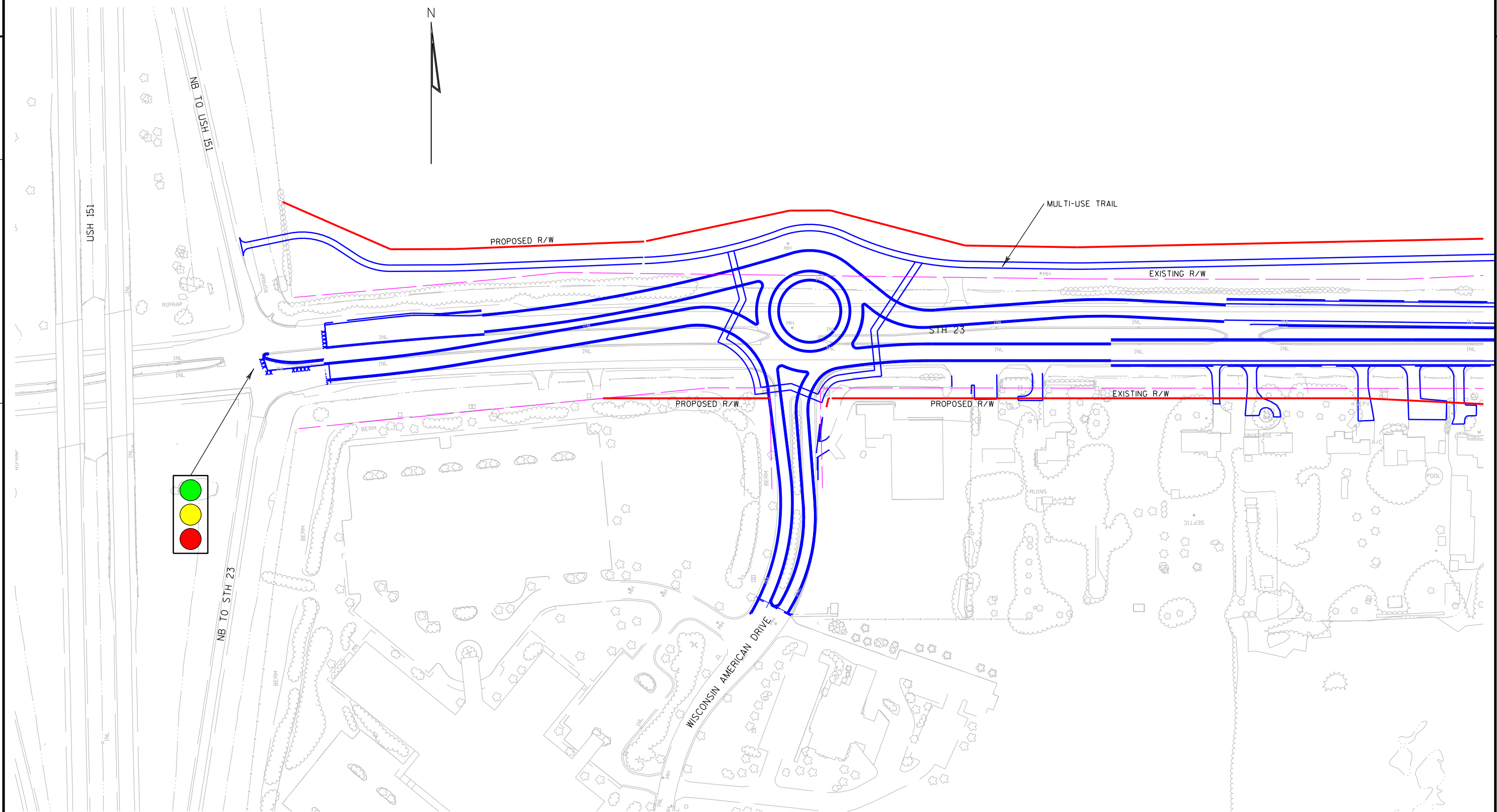
Wisconsin Department of Transportation
I.D. 1440-15-71
USH 151 - TAFT ROAD
WISCONSIN AMERICAN DRIVE ROUNDABOUT
STH 23
Preliminary Cost Estimate Summary

| ITEM DESCRIPTION | | | | TOTAL |
|---------------------------------------|------|--------------------|------------|----------------|
| ITEMS DETAILED | UNIT | QUANTITY | UNIT COST | TOTAL |
| HMA PAVEMENT | TN | 0 | \$40.00 | \$0.00 |
| CONCRETE PAVEMENT | SY | 10710 | \$30.00 | \$321,300.00 |
| ASPHALTIC MATERIALS (AC) | TN | 0 | \$375.00 | \$0.00 |
| BASE AGGREGATE DENSE | TN | 4900 | \$10.00 | \$49,000.00 |
| CURB & GUTTER | LF | 8110 | \$12.00 | \$97,320.00 |
| Major Roadway Items Detailed Subtotal | | | | \$467,620.00 |
| | UNIT | QUANTITY | UNIT PRICE | |
| SIGNALIZE INTERSECTION | LS | - | \$150,000 | \$0.00 |
| DRAINAGE | LS | % of Major Item \$ | 20% | \$94,000.00 |
| EROSION CONTROL & RESTORATION | LS | % of Major Item \$ | 15% | \$70,000.00 |
| TRAFFIC CONTROL & STAGING | LS | % of Major Item \$ | 40% | \$187,000.00 |
| LIGHTING | EACH | 10 | 10,000 | \$100,000.00 |
| SIGNING/MARKING | LS | % of Major Item \$ | 6% | \$28,000.00 |
| ROADWAY INCIDENTALS | LS | % of Major Item \$ | 30% | \$140,000.00 |
| Construction Costs Subtotal | | | | \$1,086,620.00 |
| CONSTRUCTION DESIGN CONTINGENCY | LS | % of Constr. Costs | 15% | \$163,000.00 |
| ESTIMATED CONTRACT LET AMOUNT | | | | \$1,250,000.00 |
| TOTAL COST | | | | \$1,250,000 |

Appendix G

Sketch of Alternatives





| | | | | | |
|-----------------------|------------|--------------------|------------------------|-------|---|
| PROJECT NO:1440-05-01 | HWY:STH 23 | COUNTY:FOND DU LAC | ROUNDABOUT ALTERNATIVE | SHEET | E |
|-----------------------|------------|--------------------|------------------------|-------|---|