Intersection Control Evaluation Report

CTH K Interchange

Project ID 1440-15-01
Fond du Lac - Plymouth Road
(CTH K - CTH W)
STH 23
Fond du Lac County



5950 Seminole Centre Court Suite 200 Madison, WI 53711

January 2009

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	ALTERNATIVE CONTROL TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP (TWSC) EXISTING CONTROL 2-WAY STOP	ALTERNATIVE CONTROL ☐ TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ☐ ROUNDABOUT ☐ 4-WAY STOP ☐ 2-WAY STOP (TWSC) ☐ EXISTING CONTROL 2-WAY STOP	GENERAL COMMENTS
SAFETY	The reconstruction of the existing atgrade intersection with a jug-handle type interchange and two two-way stop controlled (TWSC) intersections will likely result in a reduction in the existing crash rate. This will be due to two factors: 1. High volume and fast moving mainline STH 23 traffic will be removed from the intersections entirely. 2. Traffic turning from STH 23 onto CTH K will be divided between two intersections. Reconstructing the intersection to operate under TWSC will not reduce the number of theoretical conflict points (32), nor will it eliminate the opportunity for "angle" type crashes as vehicles make left turning maneuvers across oncoming traffic.	The reconstruction of the existing atgrade intersection with a jug-handle type interchange and two roundabout intersections will likely result in a reduction in the existing crash rate. This will be due to the same two factors as noted in the TWSC alternative. When compared to a TWSC, roundabouts reduce the number of conflict points for an intersection to 8 (4 diverge and 4 merge, 0 crossing) and greatly lessen the opportunity for "angle" type crashes. Recent studies show that conversion to roundabout control has reduced 39% of the total crashes and 76% of the injury crashes. Roundabout crashes are also typically less severe than those occurring at other types of intersections due to lower vehicle operating speeds. The safety of the mainline will also benefit from the installation of roundabouts. The increased capacity of roundabouts (when compared to TWSC) intersections will decrease the likelihood of traffic interacting with the mainline or rear-end crashes resulting from long queues.	The current crash rate for the existing at-grade intersection (based on crash data between 2001-2005) is 0.84 crashes per million entering vehicles. An intersection crash rate of 1.5 or higher indicates a level of concern that needs to be addressed. In general, both alternatives are likely to provide a safer intersection than the current conditions. Refer to the Crash Report in Appendix G for additional crash related information on the existing intersection. This Crash Report was completed for the entire STH 23 corridor in 2007.

ALTERNATIVE CONTROL TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP (TWSC) EXISTING CONTROL 2-WAY STOP Traffic signal warrants were not met

Traffic signal warrants were not met for either of the jug handle intersections with CTH K. It is anticipated that TWSC with CTH K free flowing is the likely best choice of intersection operation for this alternative. Refer to Appendix B for traffic signal warrant analysis results.

Under TWSC, both intersections will operate at a LOS A under both AM and PM design year peak hours.

CTH K & WB STH 23 JUG HANDLE

*** D D I I I Z C C C		
	Delay Per	
	Vehicl	
	(Seco	onds)
	AM	PM
	Peak	Peak
NB Approach	2.7/A	8.4/A
SB Approach	0.0/A	0.0/A
EB Approach	11.3/B	13.2/B
WB Approach	NA	NA

CTH K & WB STH 23 JUG HANDLE

OPERATIONAL ANALYSIS

TRAFFIC VOLUMES &

	Queue Length (Feet)	
	AM Peak	PM Peak
NB Approach	6'	25'
SB Approach	0'	0'
EB Approach	10'	7'
WB Approach	NA	NA

CTH K & EB STH 23 JUG HANDLE

	Delay Per Vehicle/LOS (Seconds)	
	AM	PM
	Peak	Peak
NB Approach	1.8/A	1.9/A
SB Approach	1.1/A	0.6/A
EB Approach	10.8/B	15.2/B
WB Approach	10.9/B	15.1/B

ALTERNATIVE CONTROL

☐ TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL

ROUNDABOUT

- 4-WAY STOP
- 2-WAY STOP (TWSC)
- ☐ EXISTING CONTROL 2-WAY STOP

Analysis of the traffic shows that single lane roundabouts will operate acceptably for both jug handle intersections with CTH K. Both roundabouts will have an inscribed circular diameter of 139-feet.

With a single lane roundabout, both intersections operate at LOS A under both AM and PM design year peak hours.

CTH K & WB STH 23 JUG HANDLE

	Delay Vehicl (Seco	e/LOS
	AM	PM
	Peak	Peak
NB Approach	3.8/A	4.7/A
SB Approach	3.6/A	3.9/A
EB Approach	3.1/A	3.1/A
WB Approach	NA	NA

CTH K & WB STH 23 JUG HANDLE

	Queue Length (Feet)	
	AM Peak	PM Peak
NB Approach	0'	20'
SB Approach	0'	0'
EB Approach	0'	0'
WB Approach	NA	NA

CTH K & EB STH 23 JUG HANDLE

	Delay Vehicl (Seco	e/LOS
	AM	PM
	Peak	Peak
NB Approach	3.6/A	4.8/A
SB Approach	3.0/A	3.4/A
EB Approach	4.1/A	4.1/A
WB Approach	3.2/A	3.7/A

Traffic Patterns
The design year (2035) peak hour turning movement traffic data for the intersections is shown in Appendix A.

GENERAL COMMENTS

Vehicles using the two CTH K intersections are generally shown to follow the pattern of commuter traffic entering STH 23 westbound towards Fond du Lac during the AM peak hour; and exiting STH 23 to return to the origination point during the PM peak hour. The percentage of traffic using CTH K as a through movement and not entering or exiting STH 23 is higher by nearly 50% during the AM peak hour compared to the PM peak hour. The peak hour traffic distribution percentages are shown in Appendix Α

Traffic volumes on CTH K are higher during the PM peak hour by a factor between 50% and 75% in all cases with the exception of the SB movement at the WB jug handle intersection. The SB movement at the WB Jug handle intersection is slightly higher during the AM peak hour. Traffic volumes on the jug handle ramps and Mary Hill Drive remain relatively constant between either peak hour. There are no significant seasonal traffic volume fluctuations along STH 23 according to the continuous count recorder data sources.

Operational Analysis

Both alternatives exceed the threshold for an intersection to be considered operationally acceptable. Neither alternative is shown to have access blockage resulting from queuing.

A roundabout can have slightly higher delay when compared to a high functioning TWSC intersection.

	ALTERNATIVE CONTROL ☐ TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ☐ ROUNDABOUT ☐ 4-WAY STOP ☐ 2-WAY STOP (TWSC) ☐ EXISTING CONTROL 2-WAY STOP	ALTERNATIVE CONTROL ☐ TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ☐ ROUNDABOUT ☐ 4-WAY STOP ☐ 2-WAY STOP (TWSC) ☐ EXISTING CONTROL 2-WAY STOP	GENERAL COMMENTS
TRAFFIC VOLUMES & OPERATIONAL ANALYSIS (CONT.)	CTH K & EB STH 23 JUG HANDLE Queue Length (Feet) AM PM Peak Peak NB Approach 2' 5' SB Approach 0' 0' EB Approach 28' 56' WB Approach 2' 3' Refer to Appendix C for the full operational analysis results including the results by individual movement.	CTH K & EB STH 23 JUG HANDLE Queue Length (Feet) AM PM Peak Peak NB Approach 0' 20' SB Approach 0' 0' EB Approach 0' 0' WB Approach 0' 0'	This is due to the slower entering speeds at roundabouts compared to the free flowing mainline traffic movement for the TWSC alternative. However, roundabouts have higher capacity potential than a TWSC type intersection. It is important to note that the methods used to analyze roundabouts and traditional intersections differ. Rodel software is used to analyze roundabout alternatives. Rodel utilizes an empirical method. Synchro software was used to analyze the TWSC alternative and utilizes a GAP acceptance method. These differences in the delay calculation will contribute to slight variations in the results. Refer to Appendices C and D for the full results of the TWSC and roundabout operational analysis.
CONSTRUCTION COSTS	Construction Cost = \$909,032 (Approx. Construction Year – 2013) Cost estimate area includes: 1. Jug Handle Ramps from STH 23 to the intersection. 2. CTH K from 1125' north of STH 23 to 960' south of STH 23. 3. Mary Hill Frontage Road from the intersection to 580' east.	Construction Cost = \$1,040,558 (Approx. Construction Year – 2013) Cost estimate area includes: 1. Jug Handle Ramps from STH 23 to the intersection. 2. CTH K from 1325' north of STH 23 to 1265' south of STH 23. 3. Mary Hill Frontage Road from the intersection to 500' east. 4. Hillside Circle from CTH K to 250' east.	These intersections will be constructed as part of the STH 23 expansion project from USH 151 – Log Tavern Road. These construction cost estimates include all major work items with the exception of earthwork and structures. The cost for earthwork and structures is expected to be nearly the same for either option and therefore was not included as part of a comparison of the two intersection alternatives. It is important to note that these intersection construction cost estimates were calculated assuming that they are one section of a much larger overall project. These estimates would likely be higher if this interchange was constructed as a stand-alone contract. This is due to the benefits of spreading contract costs such as mobilization, earthwork, traffic control, etc. over a larger project area. Refer to Appendix E for detailed cost estimate information and a sketch of the construction cost estimate area.

	ALTERNATIVE CONTROL TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP (TWSC) EXISTING CONTROL 2-WAY STOP	ALTERNATIVE CONTROL TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP (TWSC) EXISTING CONTROL 2-WAY STOP	GENERAL COMMENTS
RIGHT-OF-WAY	N/A	N/A	These intersections will be constructed with the STH 23 expansion project from USH 151 – Log Tavern Road. In general, roundabouts will require more right-of-way than a TWSC; however in the context of the overall STH 23 expansion project, the difference in right-of-way required will be negligible.
PRACTICAL FEASIBILITY	Reconstructing the intersections to operate as TWSC should be considered a feasible alternative. In the context of a larger STH 23 expansion project there are no major adverse impacts associated with this intersection alternative that would not exist without the majority of work to upgrade the mainline and construct interchanges. This alternative does have safety and future capacity concerns when compared to the roundabout alternative. However there is no reason this alternative should not be considered feasible if considered on its own merits.	Reconstructing the intersections to operate as roundabouts should be considered a feasible alternative. In the context of a larger STH 23 expansion project there are no major adverse impacts associated with this intersection alternative that would not exist without the majority of work to upgrade the mainline and construct interchanges.	

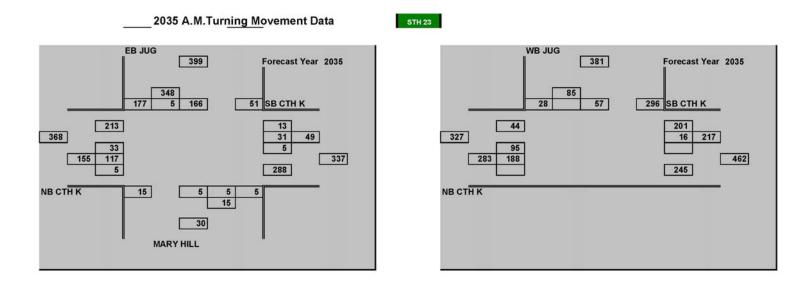
	ALTERNATIVE CONTROL	ALTERNATIVE CONTROL	GENERAL COMMENTS
	☐ TRAFFIC SIGNAL, ANTICIPATING	☐ TRAFFIC SIGNAL, ANTICIPATING	
	TRAFFIC SIGNAL	TRAFFIC SIGNAL	
	☐ ROUNDABOUT ☐ 4-WAY STOP		
	2-WAY STOP (TWSC)	2-WAY STOP (TWSC)	
	EXISTING CONTROL 2-WAY STOP	EXISTING CONTROL 2-WAY STOP	
	There are no operation and	Operation and maintenance concerns	The maintenance of either alternative
	maintenance concerns unique to this	unique to this alternative to be	will include periodic pavement and
	alternative.	considered:	other roadway infrastructure
			rehabilitation. The difference
		Street Lighting – It is reasonable to	between the two is likely to be
		expect that 10 - 12 street light units	negligible with the exception of the
		will be required at each of the two jug-	specific items listed under each
		handle intersections.	alternative.
		Opinion of probable energy	
		costs:	
		Street Lighting =	
		15 – 250 Watt HPS Fixtures,	
		106 kWH/month/fixture =	
		1,590 kWH/month	
S		Plus 7 – 150 Watt HPS Fixtures,	
9		61 kWH/month/fixture =	
)		427 kWH/month	
異			
Ç		Total = $2,017 \text{ kWH/month.}$	
A		(based on 7/8 lights (250W) within	
Z		the circulating roadway and 1 light	
		(150W) at each approach)	
E			
		Yearly Usage	
T.		2,017 kWH/month x 12 months	
		= 24,204 kWH/year	
TIONS & MAINTENANCE COSTS		Vergle Cost @ \$0.10/LWII	
S		Yearly Cost @ \$0.10/kWH = \$2,420.40/year	
Ō		= \$2,420.40/ycai	
		Central Island Landscaping – It is	
A		reasonable to expect that a	
		greenscaped central island will require	
OPERAT		routine maintenance. A specific cost	
F		is not easily attributed without	
		determining the exact design of the	
		roundabout and landscaping items.	
		D	
		Pavement Marking – Roundabouts	
		will generally require more pavement	
		marking than traditional intersections.	
		A specific cost is not easily attributed without determining the exact design	
		of the roundabout.	
		or are roundations.	

	ALTERNATIVE CONTROL	ALTERNATIVE CONTROL	GENERAL COMMENTS
	☐ TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ☐ ROUNDABOUT ☐ 4-WAY STOP ☐ 2-WAY STOP (TWSC) ☐ EXISTING CONTROL 2-WAY STOP	☐ TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP (TWSC) EXISTING CONTROL 2-WAY STOP	
ENVIRONMENTAL	N/A	N/A	In the context of a larger STH 23 expansion project there are no major adverse impacts associated with either intersection alternative that would not exist without the majority of work to upgrade the mainline and construct interchanges.
PED'S/BIKES	On-street bike lanes and sidewalks will be constructed for pedestrian and bicycle usage with this alternative. Pedestrians will be able to cross the intersections by use of at-grade crosswalks.	On-street bike lanes as well as sidewalk/shared use paths will be constructed for pedestrian and bicycle usage with this alternative. Pedestrians will be able to cross the intersections by use of at-grade crosswalks. Roundabouts will likely provide a safer crossing for pedestrians due to the slower entry speeds and needing to cross any one direction of traffic at a time when compared to the TWSC alternative.	
RECOMMENDATION	A TWSC intersection should be considered a viable alternative for both the east and west bound jughandle intersections. It will operate at an acceptable level of service and can be upgraded to signalized control if traffic volumes increase to a level where warrants are met. This alternative will likely have a lower long term operation and maintenance cost, but may have higher crash potential and less capacity.	A roundabout intersection should be considered a viable alternative for both the east and west bound jug-handle intersections. It will operate at an acceptable level of service with high residual capacity beyond the design year life. This alternative will likely have a higher long term operation and maintenance cost, but may have lower crash potential and higher capacity. A roundabout type intersection is recommended at both the ramp terminals at this location. The higher long term capacity potential of this alternative is a key factor since the area is adjacent to the rapidly growing Fond du Lac area. This higher capacity potential combined with the expected safety benefits further support the use of roundabouts at this location.	Refer to Appendix F for a sketch of each intersection alternative.

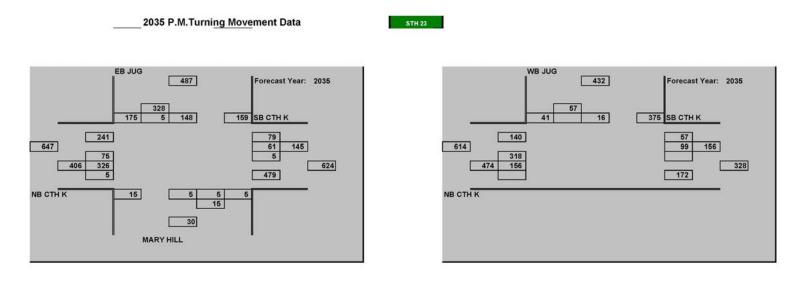
Appendix A

2035 Traffic Volumes & Distribution Percentages

2035 AM Turning Movement Data

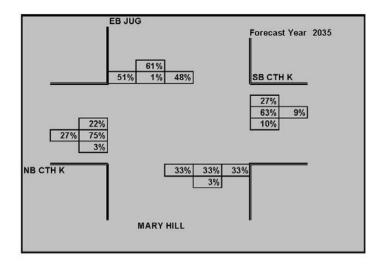


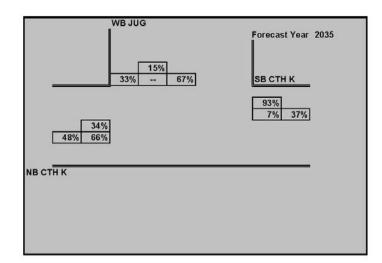
2035 PM Turning Movement Data



2035 AM Peak Traffic Distribution Percentages

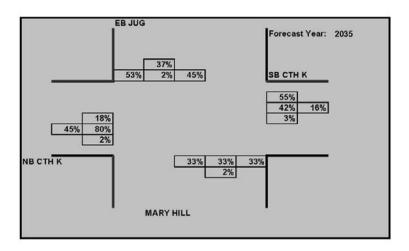
STH 23

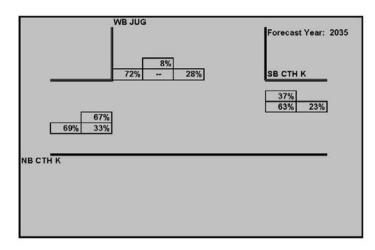




2035 PM Peak Traffic Distribution Percentages

STH 23





Appendix B

2035 Warrant Analysis Check (8-Hour Warrant – Peak Hour Only)

INTERSECTION: STH 23 & CTH K EB Off RAMP

					100% S/	100% SATISFIED	100% S	100% SATISFIED	80% SA	80% SATISFIED	/S %08	80% SATISFIED
2035	pproaches		Minor Approach		>350 Cond	>350 Condition A >105	>525 Con	>525 Condition B >53	>280 Conc	>280 Condition A >84	>420 Con	>420 Condition B >42
art time	NB SB	Totai	EB or WB		MAJOR	MINOR	MAJOR	MINOR	MAJOR	MINOR	MAJOR	MINOR
1:00	0	0	0	1	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
2.00	0	0	Q	0	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
3:00	0	0	0	٠	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
4:00	0	0	0	1	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
2:00	0	0	0	ï	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
00:9	0 0	0	0		NOT MET	NOTMET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
2:00	155 49	204	171		NOT MET	MET	NOT MET	MET	NOT MET	MET	NOT MET	MET
8:00	0	0	0	i	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
00.6	0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
00:00	0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
1.00		0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
2:00	0	0	0	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
3:00		0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
4:00		0	0	٠	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
5:00	***************************************	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
6:00		551	153	•	MET	Æ	MET	MET	MET	MET	MEI	MET
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8:00	0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT ME
00:6	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
00.0	0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
8	0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
2:00	0 0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
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00:0	0 0	0	0	•	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
total	561	755	700			TOUGHT.						

INTERSECTION: STH 23 & CTH K WB Off RAMP

		THE PERSON NAMED IN COLUMN NAM				WANTED I - FIGUR TOOK VERICULAR VOLUME	המא אסטה וו	COLAR VOLUME	,				
						100% SATISFIED	SFIED	100% St	100% SATISFIED	80% SA	80% SATISFIED	¥S %08	80% SATISFIED
2035	Major Approaches CTH K	ches CTH K	040	Minor Approach		>350 Condition A >105	A >105	>525 Conc	>525 Condition B >53	>280 Con	>280 Condition A >84	>420 Cond	>420 Condition B >42
tart time	NB NB	SB	Total	EB or WB		MAJOR	MINOR	MAJOR	MINOR	MAJOR	MINOR	MAJOR	MINOR
90:1	0	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
2:00	0	0	0	o	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
3:00	0	0	0	0	ï	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
4:00	0	0	0	0	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
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9:00	0	0	0	C	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
10:00	0	0	0	0	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
11:00	0	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
12:00	0	0	0	0	i	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
13:00	0	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
14:00	C	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
15:00	0	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
16:00	474	156	630	16		MET	NOT MET			MET	NOT MET	MET	NOT MET
17:00	0	0	o	0	i	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
18:00	0	0	0	0	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
19:00	٥	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
20:00	0	0	0	0	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
21:00	0	0	0	0	,	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
22:00	0	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
23:00	0	0	0	0		NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
00:0	0	0	0	0	ī	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET	NOT MET
total	757	272	1130	7.7		TOM SOLICE	778	ייייייייייייייייייייייייייייייייייייייי	O MONOR MET	CHO	TEM SOLION O	1001	HOLIDS MET

WILL NOT MEET WARRANTS

Appendix C TWSC Operational Analysis Results

	١	-	7	1	-	•	1	†	1	1	Į.	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		ં	7	1000	4			ર્ન	7		सी	ľ
Volume (veh/h)	166	5	177	5	5	5	33	117	5	5	31	13
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	180	5	192	5	5	5	36	127	5	5	34	14
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)			4									
Median type								None			None	
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	252	249	34	342	258	127	48			133		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	252	249	34	342	258	127	48			133		
tC, single (s)	7.2	6.6	6.2	7.2	6.6	6.2	4.1			4.1		
tC, 2 stage (s)												
tF(s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	73	99	81	99	99	99	98			100		
cM capacity (veh/h)	673	631	1 031	480	624	915	1540			1434		
Direction, Lane #	EB1	WB1	NB 1	NB 2	SB1	SB2						
Volume Total	378	16	163	5	39	14						
Volume Left	180	5	36	0	5	0						
Volume Right	192	5	0	5	0	14						
cSH	1367	628	1540	1700	1434	1700						
Volume to Capacity	0.28	0.03	0.02	0.00	0.00	0.01						
Queue Length 95th (ft)	28	2	2	0	0	0						
Control Delay (s)	10.8	10.9	1.8	0.0	1.1	0.0						
Lane LOS	В	В	Α		Α							
Approach Delay (s)	10.8	10.9	1.7		0.8							
Approach LOS	В	В										
Intersection Summary												
Average Delay			7.5									
Intersection Capacity Utiliza	tion		37.4%	IC	U Level o	of Service			A			
Analysis Period (min)			15									

	۶	-	*	1	-	•	1	1	-	1	Ţ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations	44.510	र्स	7		4			र्स	7		4	7
Volume (veh/h)	148	5	175	5	5	5	75	326	5	5	61	79
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	161	5	190	5	5	5	82	354	5	5	66	86
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)			4									
Median type								None			None	
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	603	600	66	692	680	354	152			360		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	603	600	66	692	680	354	152			360		
tC, single (s)	7.2	6.6	6.2	7.2	6.6	6.2	4.1			4.1		
tC, 2 stage (s)												
tF(s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	58	99	81	98	98	99	94			100		
cM capacity (veh/h)	380	385	989	270	346	683	1410			1182		
Direction, Lane #	EB1	WB1	NB 1	NB 2	SB1	SB 2						
Volume Total	357	16	436	5	72	86						
Volume Left	161	5	82	0	5	0						
Volume Right	190	5	0	5	0	86						
cSH	815	372	1410	1700	1182	1700						
Volume to Capacity	0.44	0.04	0.06	0.00	0.00	0.05						
Queue Length 95th (ft)	56	3	5	0	0	0						
Control Delay (s)	15.2	15.1	1.9	0.0	0.6	0.0						
Lane LOS	C	C	Α		Α							
Approach Delay (s)	15.2	15.1	1.9		0.3							
Approach LOS	С	C										
Intersection Summary												
Average Delay			6.7									
Intersection Capacity Utilizat	tion		49.8%	IC	U Level o	of Service			Α			
Analysis Period (min)			15									

	۶	*	1	†	Į.	1
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	ሻ	7	*	†	†	7
Volume (veh/h)	57	28	95	188	16	201
Sign Control	Stop			Free	Free	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	62	30	103	204	17	218
Pedestrians						
Lane Width (ft)						
Walking Speed (tt/s)						
Percent Blockage						
Right turn flare (veh)		4				
Median type				None	None	
Median storage veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	428	17	236			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	428	17	236			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF(s)	3.5	3.3	2.2			
p0 queue free %	88	97	92			
cM capacity (veh/h)	532	1053	1314			
Direction, Lane #	EB 1	NB1	NB 2	SB 1	SB2	
Volume Total	92	103	204	17	218	
Volume Left	62	103	0	0	0	
Volume Right	30	0	0	0	218	
cSH	794	1314	1700	1700	1700	
Volume to Capacity	0.12	0.08	0.12	0.01	0.13	
Queue Length 95th (ft)	10	6	0	0	0	
Control Delay (s)	11.3	8.0	0.0	0.0	0.0	
Lane LOS	В	Α	2,0,000			
Approach Delay (s)	11.3	2.7		0.0		
Approach LOS	В					
Intersection Summary						
Average Delay			2.9			
Intersection Capacity Utiliza	ation		24.4%	10	CU Level o	of Service
Analysis Period (min)			15			

	۶	*	1	†	ļ	4	
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations	1	7	7	↑	↑	7	
Volume (veh/h)	16	41	318	156	99	57	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	17	45	346	170	108	62	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)		4					
Median type				None	None		
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	968	108	170				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	968	108	170				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF(s)	3.5	3.3	2.2				
p0 queue free %	92	95	75				
cM capacity (veh/h)	209	938	1390				
Direction, Lane #	EB1	NB1	NB 2	SB 1	SB 2		
Volume Total	62	346	170	108	62		
Volume Left	17	346	0	0	0		
Volume Right	45	0	0	0	62		
cSH	744	1390	1700	1700	1700		
Volume to Capacity	0.08	0.25	0.10	0.06	0.04		
Queue Length 95th (ft)	7	25	0	0	0		
Control Delay (s)	13.2	8.4	0.0	0.0	0.0		
Lane LOS	В	Α					
Approach Delay (s)	13.2	5.7		0.0			
Approach LOS	В						
Intersection Summary							
Average Delay			5.0				
Intersection Capacity Utiliza	ation		34.3%	10	CU Level o	of Service	А
Analysis Period (min)			15				

Appendix D Roundabout Operational Analysis Results

RODEL Results / CTH K (EAST BOUND)

10:7:08			C	TH K EB	STH 2	3							.30
E (m)	4.25	4.25	4.25	4.25				ME F	ERIO)	min		90
L' (m)	40.00	40.00	40.00	40.00			T	ME S	LICE		man		15
U (m)	3.65	3.65	3.65	3.65			RE	SULT	S PE	RIOD	man		75
RAD (m)	20.00		20.00	20.00			T)	ME C	TRO		\$/hr	15.	00
PHI (d)	25.00		25.00	25.00			FI	OW P	ERIO		min	15	
DIA (m)	45.00		45.00	45.00			FI	LOW I	YPE	peu	/veh		EH
GRAD SEP	Ø	Ø	Ø	Ø			FI	OW F	EAK	am/o	p/pm		AM
EC MONE	D/9I	THENE CA		, 2nd U		DI OF	CT	TVE	OU D	TIO	1,0	T SUL	TIM
вв стн к	1.05	013 031	005	001	1	1.00	50	G 75	1.1) E (A)	7F 1	E AE	75
EB JUG	1.05	177 005	166	003		1.00	50	0 75	1.1	25 0.			
NB CTH K	1.05	005 117	033	002		1.00	50	0.75		5 6			
MARY HILL		005 005	005	001_		1.00	50						75
	1.00	000 000	000	- 100		1.00	30	0.10				. 10	
OT COLD		ro.		MODE 2	47					AUED			2 0
COBOCTEN	ven	50	351	157	16					HOLL	EL	0	3.8
ONFHGIII	ven	1213	1215	1139	1114					LOC	HINET	e e	A
MOX DELOV	0000	3.8	5.3	4.6	4.1					100	BHOL		
OUE OUTUE	ueh	9.0	.0	0	7.6					HEHT	C HR		0.6
HOW OUTSILE		õ	Ø	ő	ē					COOP	- II N	Ž.	9.0

AM 50

10:7:08			0	TH K EB S	TH 23					4
E (m) L* (m) V (m) RAD (m) PHI (d)	4.25 40.00 3.65 20.00 25.00	40.00 4 3.65 20.00 2 25.00 2	4.25 10.00 3.65 20.00 25.00	4.25 40.00 3.65 20.00 25.00		TIM TIM RESU TIM FLOU	E PERIOD E SLICE ULTS PER E COST W PERIOD	10D m	in in 15 hr 15. in 15	75
DIA (m) GRAD SEP	45.00 0		15.00 0	45.00 0		FLO	W TYPE W PEAK	pcu/vi		EH AM
LEG NAME SB CTH K EB JUG NB CTH K MARY HILL	PCU 1.05 1.05 1.05 1.05 1.00	013 031 177 005 005 117 005 005	exit 005 166 033 005	2nd U) 001 003 002 001	FLOF 1.00 1.00 1.00 1.00	85 Ø 85 Ø	FLOW RA .75 1.12 .75 1.12 .75 1.12 .75 1.12	5 0.75 5 0.75	15 45	75
W. Carlot		12.11		MODE 2			1000	100		
FLOW CAPACITY AUE DELAY	veh veh	50 1016 3.7 4.6	351 1018 5.3 7.0	157 942 4.5 5.8	16 907 4.0 5.0			AUEDEL LOS ! LOS UN!	SIG SIG	4.9 A A
OUE OUTSILE	weh	9	1	3.0	9			UEHIC I	IRS	0.8

RODEL Results / CTH K (EAST BOUND)

10:7:08	100 0000	-	C	TH R EB S	TH 23	Complete of the last	-	5
E (m) L' (m) U (m) RAD (m) PHI (d) DIA (m) GRAD SEP	4.25 40.00 3.65 20.00 25.00 45.00	40.00 3.65 20.00 25.00 45.00	4.25 40.00 3.65 20.00 25.00 45.00	4.25 40.00 3.65 20.00 25.00 45.00		TIME PERI TIME SLIC RESULTS P TIME COST FLOW PERI FLOW TYPE FLOW PEAR	OD min E min ERIOD min \$/hr OD min pcu/veh	90 15 15 75 15.00 15 75 VEH PM
LEG MAME SB CTH K EB JUG NB CTH K	PCII 1.05 1.05 1.05	TURNS (1st 079 061 175 005 005 326	005 148 075	2ndU) 001 003 004	1.00	50 0.75 1.	125 0.75 19 125 0.75 19	5 45 75 5 45 75
MARY HILL	1.00	005 005	005	001 MODE 2	1.00	50 0.75 1.	125 0.75 1	5 45 75
FLOW CAPACITY AVE DELAY	veh secs	146 1188 3.4 4.3	331 1197 4.1 5.3	410 1149 4.8 6.4	16 977 3.7 4.7		LOS UNSI	4.3 G A
AVE QUEUE	veh	9	9	1 1	9		UEHIC HE	1.1

PM 50

10:7:08		- 12 CON 10	C	TH K EB S	TH 23	- 100			6
E (m) L' (m) U (m) RAD (m) PHI (d) DIA (m) GRAD SEP	4.25 40.00 3.65 20.00 25.00 45.00	3.65 20.00 2 25.00 2	4.25 0.00 3.65 0.00 5.00 5.00	4.25 40.00 3.65 20.00 25.00 45.00		TI TI RE TI FL FL	ME PERIOD ME SLICE SULTS PERI ME COST OW PERIOD OW TYPE OW PEAK a	mi OD mi \$/h mi pcu/ve m/op/y	15.00 n 15 75 h VEH
EB JUG	PCU 1.05 1.05 1.05 1.05	079 061 175 005 005 326 005 005	005 148 075 005	2ndU) 001 003 004 001		85 85	FLOW RAT 0.75 1.125 0.75 1.125 0.75 1.125 0.75 1.125	0.75 0.75	15 45 75 15 45 75
				MODE 2	_				
FLOW CAPACITY AUE DELAY MAX DELAY	veh veh secs secs	146 991 4.2 5.3	331 1000 5.3 6.9	410 952 6.5 8.9	16 770 4.7 6.1		f I	UEDEL OS S OS UNS	IG 5.
AUE QUEUE	veh	Ø Ø	0	1	Ø Ø		, and	EHIC H	RS 1.4

RODEL Results / CTH K (WEST BOUND)

10:7:08	100,000	V 10000000	СТ	H K WB STI	1 23	The same	The Break			2
E (m) L' (m) U (m) RAD (m) PH1 (d) DIA (m) GRAD SEP	4.2 40.0 3.6 20.0 25.0 45.0	0 40.00 5 3.65 0 20.00 0 25.00	4.25 40.00 3.65 20.00 25.00 45.00			TI TI RE TI FL FL	ME PERI ME SLIC SULIS P ME COSI OW PERI OW TYPE OW PEAK	OD E ERIOD \$ OD pcu/ am/op	/hr 1	90 15 5 75 5 00 5 75 VEH AM
LEG MAME SB CTH K WB JUG NB CTH K	PCU 1.05 1.05 1.05	TURNS (1s 201 016 028 057 188 095	991	2ndU)	1.00	50	FLOW 0.75 1. 0.75 1. 0.75 1.	125 0.7	5 15	W TIP 45 75 45 75 45 75
		2777420	I		URE					- Control of the
FLOW CAPACITY AUE DELAY	veh secs	219 1185 3.6 4.7	86 1228 3.1 3.9	286 1206 3.8 4.9				LOS U	L s SIG NSIG	3.7 A A
AUE QUEUE	veh	7. Ó	9	9				UEHIC	HRS	0.6

AM 50

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WB JUG
NB CTH K
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4.9
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                                                                                                                                                                                     0.8
11
                                                                                           P4Fact
                                                                                                                                  F8econ
                                                                                                           F6stats
```

RODEL Results / CTH K (WEST BOUND)

10:7:08		18	TH K WB ST	H 23	NAME OF TAXABLE PARTY.			- 3
E (m) L' (m) U (m) RAD (m) PHI (d) DIA (m) GRAD SEP	4.2! 40.00 3.6! 20.00 25.00 45.00	5 4.25 4.25 0 40.00 40.00 5 3.65 3.65 0 20.00 20.00 0 25.00 25.00			TIME TIME RESUL TIME FLOW FLOW FLOW	PERIOD SLICE IS PERI COST PERIOD IYPE PEAK a	mir oD mir \$/hr mir pcu/vel m/op/pr	90 15 15 15 75 15.00 15 75 VEH PM
LEG NAME SB CTH K WB JUG NB CTH K	PCII 1.05 1.05 1.05	7URNS (1st exit 057 099 002 041 016 001 156 318 005	2ndU)	1.00	50 0.7	5 1.125	0.75 1	LOW TIP 15 45 75 15 45 75 15 45 75
		- Section - Section	L'< 5 when	USE				
FLOW CAPACITY AUE DELAY MAX DELAY	veh veh secs secs	158 58 1060 1181 3.9 3.1 5.1 4.0	479 1229 4.7 6.3			L	VEDEL OS SI OS UNS	8 4.4 IG F
AVE QUEUE	veh	9 9	1			U	EHIC HI	Ø.8 5 13

PM 50

10:7:00			CI	II K WD STI	1423					5
E (m) L' (m) U (m) RAD (m) PHI (d) DIA (m) GRAD SEP	4.25 40.00 3.65 20.00 25.00 45.00	0 40.00 4 5 3.65 0 20.00 2 0 25.00 2	4.25 0.00 3.65 0.00 5.00 5.00			T I RI FI	IME PERIO IME SLICI ESULTS PI IME COST LOW PERIO LOW TYPE LOW PEAK	DD m E m ERIOD m \$/ DD m pcu/vo am/op/	in in 15 hr 15	90 15 75 .00 75 VEH PM
LEG NAME SB CTH K WB JUG NB CTH K	PCU 1.05 1.05 1.05	TURNS (1st 057 099 041 016 156 318	exit; 002 001 005	2ndU)	FLOF 1.00 1.00 1.00		FLOW 1 0.75 1.1 0.75 1.1 0.75 1.1	MIIO 125 Ø.75 125 Ø.75 125 Ø.75	15 4	TIM 5 75 5 75 5 75
				√ 5 when	UATE					
FLOW CAPACITY AUE DELAY	veh veh secs	158 863 5.0 6.5	58 984 3.8 4.8	479 1032 6.4 8.7				LOS UN	SIG SIG	5.9 A A
AUE QUEUE	veh	9	9	1				UEHIC	HRS	1.1 17

Appendix E

Cost Estimates

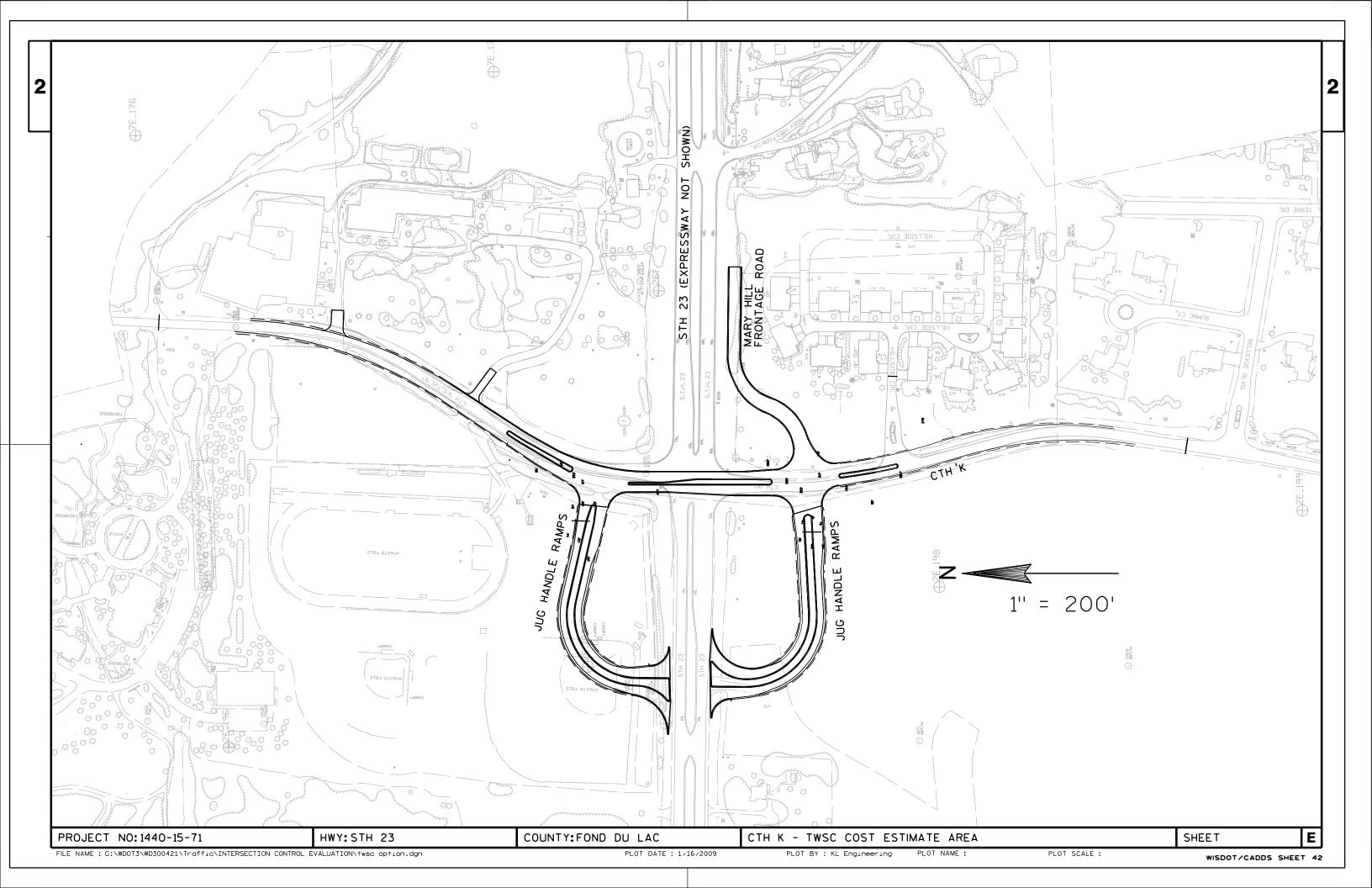
STH 23 PROJECT 1440-15-01

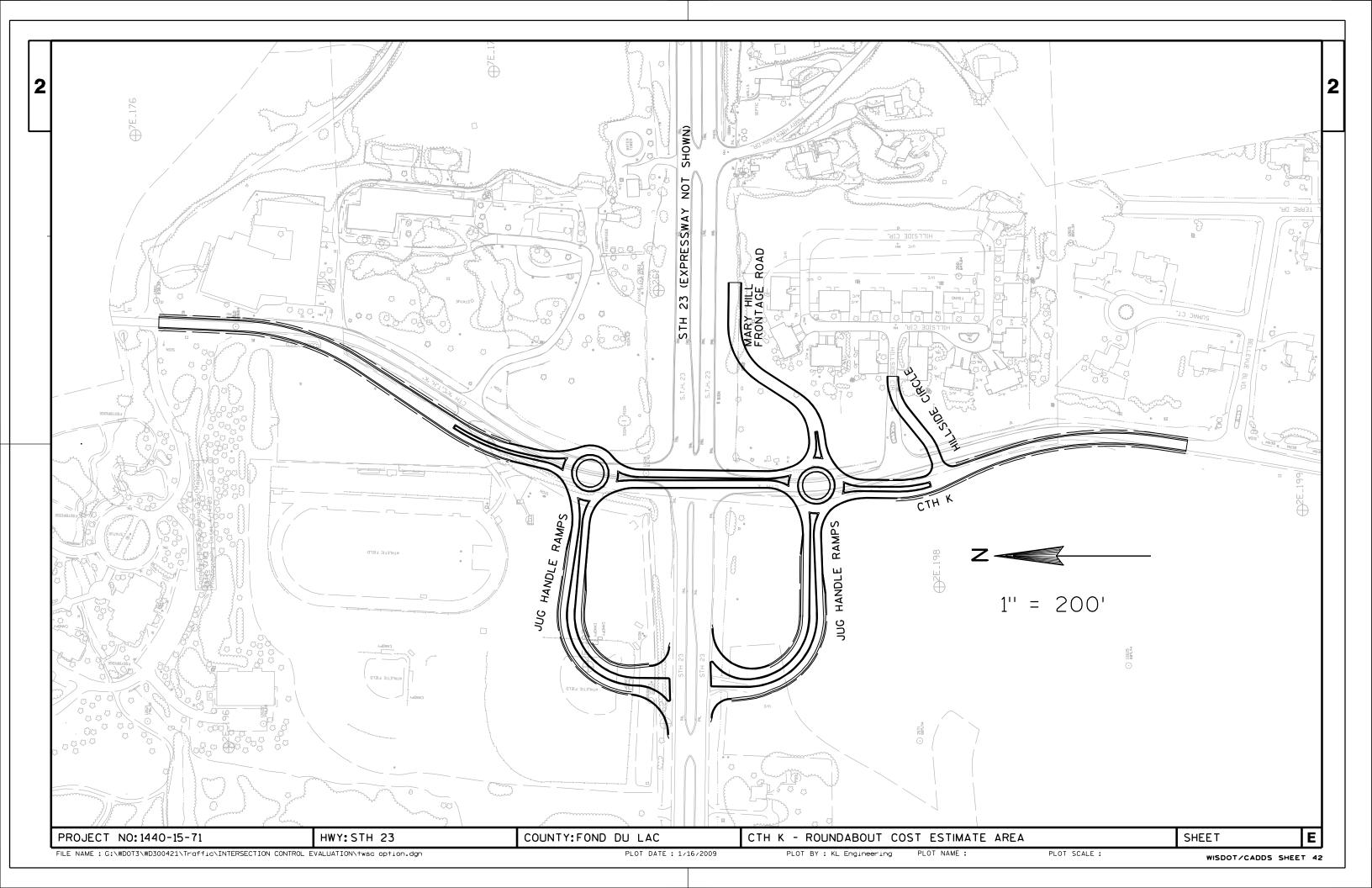
COST ESTIMATE FOR: STH 23 & CTH K - ROUNDABOUT ALTERNATIVE

ITEM	ITEM DESCRIPTION	UNIT	QUANTITY	UNIT PRICE	TOTAL
1	CONCRETE PAVEMENT 8-INCH	SY	4626	\$35.00	\$161,910
2	HMA PAVEMENT TYPE E-0.3	TON	3038	\$50.00	\$151,900
3	HMA PAVEMENT TYPE E-1	TON	196	\$65.00	\$12,740
4	ASPHALTIC MATERIAL	TON	194	\$450.00	\$87,300
5	TACK COAT	GAL	350	\$2.50	\$875
6	BASE AGGREGATE DENSE 3/4-INCH	TON	570	\$12.50	\$7,125
7	BASE AGGREGATE DENSE 1 1/4-INCH	TON	17128	\$10.00	\$171,280
8	CONCRETE SIDEWALK	SF	17624	\$3.00	\$52,872
9	CONCRETE CURB & GUTTER 30-INCH	LF	7077	\$10.50	\$74,309
10	CONCRETE CURB & GUTTER 36-INCH	LF	2050	\$12.00	\$24,600
11	CONCRETE TRUCK APRON	SY	575	\$55.00	\$31,625
12	DRAINAGE ITEMS	LS	15% Of Items 1 - 11		\$116,480
13	LANDSCAPING ITEMS	LS	2% Of Items 1 - 11		\$15,531
14	EROSION CONTROL ITEMS	LS	2% Of Items 1 - 11		\$15,531
15	PAVEMENT MARKING ITEMS	LS	3% Of Items 1 - 11		\$23,296
16	SIGNING ITEMS	LS	2% Of Items 1 - 11		\$15,531
17	LIGHTING ITEMS	LS	10% Of Items 1 - 11		\$77,654
				GRAND TOTAL COST	\$1,040,558

STH 23 & CTH K - TWO WAY STOP CONTROL ALTERNATIVE

ITEM	ITEM DESCRIPTION	UNIT	QUANTITY	UNIT PRICE	TOTAL
1	CONCRETE PAVEMENT 8-INCH	SY	5332	\$35.00	\$186,620
2	HMA PAVEMENT TYPE E-0.3	TON	3532	\$50.00	\$176,600
3	HMA PAVEMENT TYPE E-1	TON	211	\$65.00	\$13,715
4	ASPHALTIC MATERIAL	TON	225	\$450.00	\$101,250
5	TACK COAT	GAL	405	\$2.50	\$1,013
6	BASE AGGREGATE DENSE 3/4-INCH	TON	629	\$12.50	\$7,863
7	BASE AGGREGATE DENSE 1 1/4-INCH	TON	17771	\$10.00	\$177,710
8	CONCRETE SIDEWALK	SF	0	\$3.00	\$0
9	CONCRETE CURB & GUTTER 30-INCH	LF	4129	\$10.50	\$43,355
10	CONCRETE CURB & GUTTER 36-INCH	LF	3082	\$12.00	\$36,984
11	DRAINAGE ITEMS	LS	15% Of Items 1 - 10		\$111,766
12	LANDSCAPING ITEMS	LS	2% Of Items 1 - 10		\$14,902
13	EROSION CONTROL ITEMS	LS	2% Of Items 1 - 10		\$14,902
14	PAVEMENT MARKING ITEMS	LS	2% Of Items 1 - 10		\$14,902
15	SIGNING ITEMS	LS	1% Of Items 1 - 10		\$7,451
16	LIGHTING ITEMS	LS	0% Of Items 1 - 10		\$0
				GRAND TOTAL COST	\$909,032





Appendix F Sketch of Alternatives

WISDOT/CADDS SHEET 40 SHEET CTH K & EB STH 23 JUG HANDLE - TWSC ALTERNATIVE CTH K & EB STH 23 JUB HANDLE - TWSC ALTERNATIVE COUNTY: FOND DU LAC HWY: STH 23 PROJECT NO: 1440-15-71 830 825 820 86 5

2 ш SHEET CTH K & WB STH 23 JUG HANDLE - TWSC ALTERNATIVE 76.719 86.858 85.213 609.63 87.178 629.89 COUNTY: FOND DU LAC \$ 806.53 85127 NAMES OF TAKEN OF STATES OF THE STATES OF TH PROJECT NO: 1440-15-71 825 830 820 99 805 2

CTH K & WB STH 23 JUB HANDLE - TWSC ALTERNATIVE

2 WISDOT/CADDS SHEET 40 840 930 825 s/n_ 85 SHEET CTH K & EB STH 23 JUG HANDLE - ROUNDABOUT ALTERNATIVE 75.25.8 50.05.8 82779 82779 82.61a 02.02a 8 COUNTY: FOND DU LAC 2 815.26 8 630.09 20.M3 \$ 81.518 8 81.05 615.19 621.55 HWY: STH 23 E8.E13 0 STA, II+15 Z4-NCH X 175'RCD* N Z APRÓN ENDWALLS R P127+88.45 PROJECT NO: 1440-15-71 840 830 835 825 850 86 810 5

CTH K & EB STH 23 JUB HANDLE - ROUNDABOUT ALTERNATIVE

5 WISDOT/CADDS SHEET 40 SHEET CTH K & WB STH 23 JUG HANDLE - ROUNDABOUT ALTERNATIVE 76.719 62.858 25.21a 629.03 87.178 629.89 COUNTY: FOND DU LAC 15.018 25.008 38,308 550.81 \$ 806.53 8 83127 HWY: STH 23 8 8271S PROJECT NO: 1440-15-71 830 852 820 835 80 805

CTH K & WB STH 23 JUB HANDLE - ROUNDABOUT ALTERNATIVE

Appendix G STH 23 Corridor Crash Report

Crash Report

Project ID 1440-15-01
Fond du Lac - Plymouth Road
(CTH K - CTH W)
STH 23
Fond du Lac County



5950 Seminole Centre Court Suite 200 Madison, WI 53711

June, 2007

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I. Introduction

The proposed project begins at USH 151 and proceeds easterly approximately 8.3 miles to Log Tavern Road.

This report summarizes crash data for STH 23 from USH 151 to Log Tavern Road. The corridor was divided into 3 segments to correlate crashes with AADT. The segments included the 0.7 mile segment from the Northbound ramps of USH 151 to CTH K which is a primarily four lane divided rural section (posted speed from 35 mph to 45mph), the 1.3 mile segment from CTH K to the CTH UU which is primarily a four lane divided rural section (posted speed 55 mph) and the 6.3 mile segment from CTH UU to Log Tavern Road which is a two lane undivided rural section (posted speed of 55 mph). See Appendix A for Project Location Map.

II. Traffic and Crash Data

Annual Daily Traffic (AADT)

Year 2000 AADT's from the Wisconsin Highway Traffic Volume Data and Traffic Counts for 2006 provided by WisDOT were used to interpolate AADT's for the years 2001 - 2005; using the equation F=P(1+i)^n where F is the future year, P is the present year's AADT, i is the growth rate and n is the number of years from the present year. Table 1 shows the AADT's for the period from 2001-2005. See Appendix B for AADT computations and Appendix C for Wisconsin Highway Traffic Volume Data maps.

SEGMENT **FROM** TO 2001 2002 2003 2004 2005 1 USH 151 CTH K 13600 13600 13600 13600 13600 2 CTH K CTH UU 10395 10593 10795 11001 11211 3 CTH UU LOG TAVERN RD 8181 8263 8346 8430 8515

Table 1: AADT's

Vehicle Miles Traveled (VMT)

Vehicles miles traveled is a measure of the number of vehicles and the distance that was traveled by those vehicles. The VMT is used to compute a crash rate. Table 2 summarizes the vehicle miles traveled in millions and was computed using the following:

 $VMT = (AADT \times 365 \text{ days } \times LENGTH)/1,000,000$

Table 2: VMT in Millions

	LENGTH	2001	2002	2003	2004	2005
SEGMENT 1	0.70 MILES	3.5	3.5	3.5	3.5	3.5
SEGMENT 2	1.26 MILES	4.8	4.9	5.0	5.1	5.2
SEGMENT 3	6.29 MILES	18.8	19.0	19.2	19.3	19.5

Total Crashes

The crash data provided by WisDOT includes crashes from 2001 thru 2005 that occurred on the State Trunk Highway System. The database includes crashes involving \$1,000 or more damage to any one vehicle, an injury of fatality, and \$200 or more in damage to government property such as traffic sign's or guard rail. Table 3 summarizes the crashes by segment according to crash severity.

Table 3: Total # of Crashes

Segment	Total # of	Property	Crash	Crash
Number	Crashes	Damage	With Injury	With Fatality
Segment 1	28	14	14	0
Segment 2	21	10	11	0
Segment 3	53	25	28	0
Project Totals	102	49	53	0

Intersection and Non-Intersection Related crashes

The crash data that was used for this analysis identifies the crashes that are intersection related and those that are not related to intersections. "Intersection Related" is defined in the Law Enforcement Officer's Instruction Manual for Completing the Wisconsin Motor Vehicle Crash Report Form (MV4000) as the following:

""Intersection Related" crashes are crashes which result from an activity, behavior, or traffic control which affects a unit's movement in relation to an intersection; whether or not the point of origin or first harmful event occurred within the intersection"

Intersection Related Crashes

Each intersection along the corridor was analyzed to determine the number, type and severity of crashes that occurred. The number of crashes at the intersections accounted for 43 percent of the total crashes through the corridor and 49 percent of injury crashes. Segment 1 accounts for 50 percent of intersection related crashes.

Table 4 summarizes crash data by crash severity and crash type for each intersection. Figure 1 shows the percentage of intersection related crashes at each intersection. Figure 2 shows the breakdown of the collision type for intersection related crashes.

Table 4: Intersection Crash Summary

SEGMENT 1	TOTAL	PROP. DAMAGE	INJURIES	FATALITIES	ANGLE	UNKNOWN	HEAD-ON	FIXED-OBJ.	REAR-END	SIDESWIPE - SAME DIR.	SIDE SWIPE OPP. DIR.
COUNTY ROAD K	20	9	11	0	13	0	1	3	2	0	1
WISCONSIN AMERICAN	2	1	1	0	2	0	0	0	0	0	0
SEGMENT 2					_						
UU	6	2	4	0	3	0	0	1	2	0	0
HILLTOP DR	1	0	1	0	1	0	0	0	0	0	0
WHISPERING SPRINGS BLVD	1	0	1	0	0	0	0	0	1	0	0
SEGMENT 3											
SEVEN HILLS RD	2	0	2	0	1	0	0	0	1	0	0
POPLAR RD	1	0	1	0	0	0	0	0	1	0	0
COUNTY ROAD W	9	5	4	0	2	1	0	0	4	2	0
HINN RD	0	0	0	0	0	0	0	0	0	0	0
RICHARDS RD	OAD W 9 5 0 0		0	0	0	0	0	0	0	1	0
LOG TAVERN RD	0	0	0	0	0	0	0	0	0	0	0
TAFT RD	0	0	0	0	0	0	0	0	0	0	0
TOWER RD.	_ 1_	0	_ 1_	_ 0_	0	0	0	0	1	0	0
TOTALS	44	18	24	0	22	1	2	4	12	3	1

Figure 1: Percentage of Crashes at Intersections

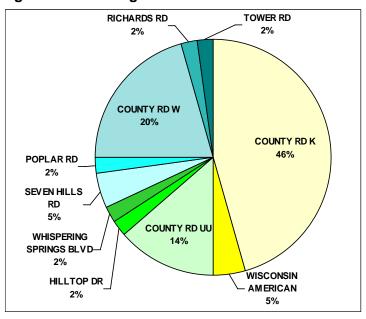
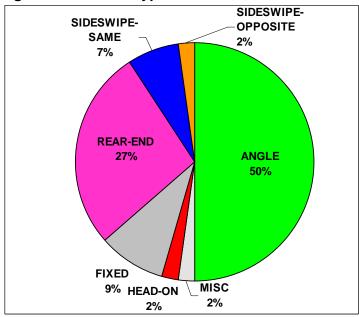


Figure 2: Collision Type at Intersections



Non-Intersection Related Crashes

Non-Intersection related crashes were classified into segments of the roadway in which they occurred. Non-Intersection related crashes accounted for 66 percent of the total crashes. Collisions with fixed objects accounted for 43 percent of the non-intersection related crashes. 54 percent of these crashes occurred while it was snowing or raining.

See Appendix D for map of non-intersection related crashes locations. Table 5 summarizes crashes based on severity and crash type. Figure 3 shows the percentage of crashes per Segment. Figure 4 shows the collision type percentage for non-intersection related crashes.

OPPOSITE SIDE SWIPE SAME PROP DAMAGE FIXED OBJECT SWIPE REAR-END **HEAD-ON** NJURY ANGLE **FATAL** TOTAL 回 **SEGMENT TOTALS**

Table 5: Non-Intersection Collision Types by Segment

Figure 3: Percentage of Non-Intersection crashes by segment

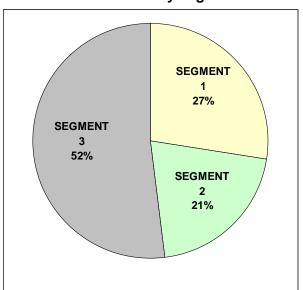
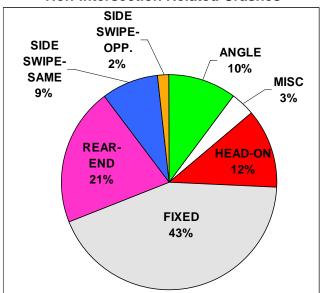


Figure 4: Collision Types for Non-Intersection Related Crashes



III. Crash Rates

Crash rates for each segment were computed for total number of crashes, crashes resulting in an injury and crashes resulting in a fatality. These rates were then compared to the statewide crash rate for comparable rural State trunk highways. The statewide crash rate is expressed as number of crashes per hundred million vehicle miles traveled. Crash rates were computed by dividing the total number of crashes by the VMT. Table 6 summarizes the crash rates by year, segment and severity of crash. Values above the statewide average are underlined and bold.

Table 6: Crash Rates Comparison to Statewide Average for Rural STH

	,	TOTAL			INJURY		FA	TALITY	<i>I</i>
YEAR	STATE	SEG2	SEG3	STATE	SEG2	SEG3	STATE	SEG2	SEG3
2001	104	42	53	42	42	27	2	0	0
2002	106	61	37	42	41	21	2	0	0
2003	117	80	89	46	40	<u>52</u>	2	0	0
2004	121	<u>138</u>	67	47	<u>59</u>	31	2	0	0
2005	115	97	31	43	39	15	2	0	0
AVG	113	84	55	44	44	29	2	0	0

There was a significant decrease in the accident rates between 2003 and 2004.

Segment 1 is a 0.7 mile segment that is includes an interchange in a semi-urban area. There are no statewide averages for a segment of this type. Due to this and its length being less than one mile, which is considered the minimum length appropriate for comparison, this segment was not included in this section of the report.

IV. Conclusion

There were 102 crashes along STH 23 from 2001 thru 2005. Crashes involving property damage accounted for 47 percent of the total while crashes resulting in personal injury accounted for 53 percent. There were no fatalities during this time period. A review of the database (minus deer related crashes) indicated the following:

- Segment 3, the longest segment, was responsible for 51 percent of the total number of crashes, 74 percent of which were non-intersection related.
- Intersection related crashes accounted for 44 percent of the total crashes, 52 percent of those were angle type crashes.
- Non-intersection related crashes that were not from a collision with a fixed object are concentrated near the intersections and driveways. See Appendix D for map showing non-intersection related crash locations.

SEGMENT 1

- There were 28 crashes (29 percent of total) during the study period.
- 80 percent of crashes were intersection related crashes, 71 percent of which occurred near the County Road K intersection.
- 43 percent of the crashes were angle type crashes at the County Road K intersection.
- 2001-2003 the segment averaged 9 crashes per year, after 2003 the segment only averaged 1.5 crashes.

SEGMENT 2

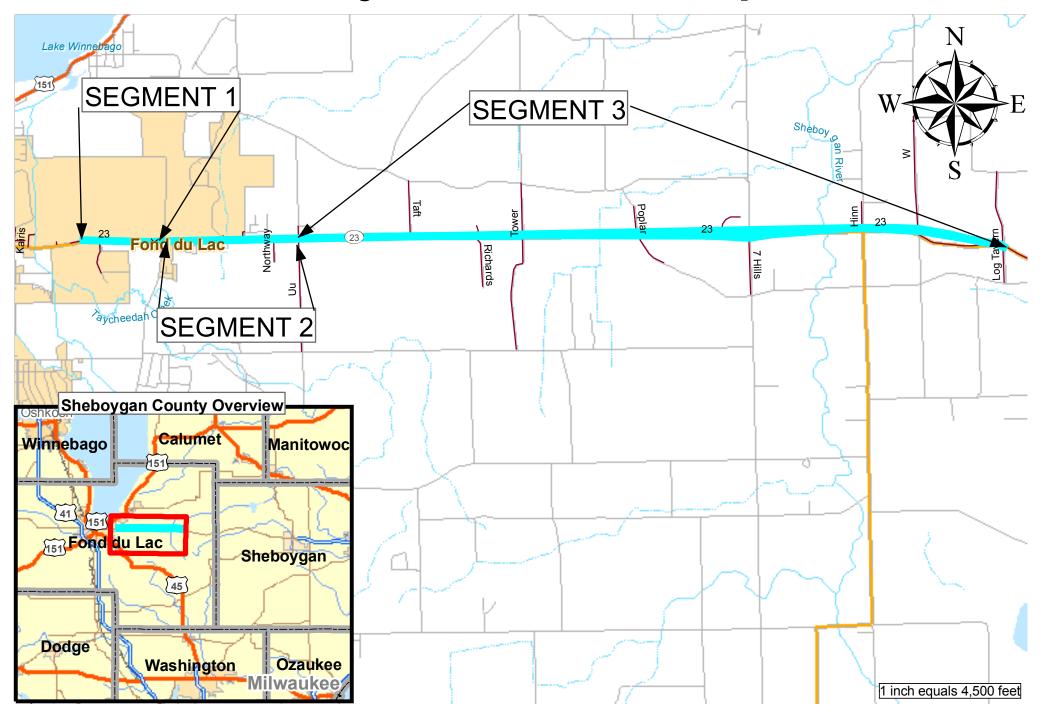
- There were 21 crashes (20 percent of total) during the study period.
- 48 percent of crashes in Segment 2 occurred near the County Road UU intersection.
- 2001-2003 the segment averaged 3 crashes per year, after 2003, 6 crashes.
- In 2004 the segment had crashes rates higher than the statewide average for crashes and crashes with injury.

SEGMENT 3

- There were 53 crashes (51 percent of total) during the study period.
- 40 percent of crashes were with fixed objects such as signs, the ditch, light poles or trees.
- 9 crashes occurred at the County Road W intersection, four of which were rearend type crashes.
- In 2003 the injury crash rate was higher than the statewide average.

APPENDIX A PROJECT LOCATION MAP

Project Location Map



APPENDIX B

AADT & CRASH RATE COMPUTATIONS

AADT & Crash Rate Computations

ADT CALCULATOR

KNOWN TRAFFIC	<u>151-K</u>	<u>K-UU</u>	UU-LOG	<u>TAVERN</u>
START YEAR	<u>2000</u>	<u>2000</u>	<u>2000</u>	FROM TRAFFIC COUNTS BOOK 2002
ADT	13600	10200	8100	
END YEAR ADT	<u>2006</u> 13600	<u>2006</u> 11425	<u>2006</u> 8600	FROM TRAFFIC COUNTS COMPLETED IN 2006
GROWTH RATE = F=P(1+i)^n	0.00%	1.91%	1.00%	

ADT PROJECTIONS

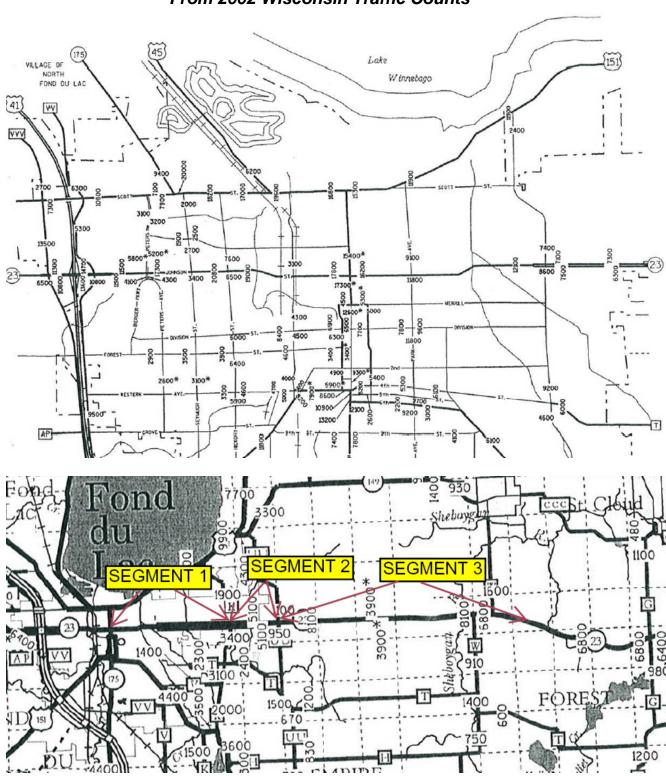
MILLION VEHICLE MILES (MVM) = (ADT x 365 x LENGTH)/1,000,000

<u>151-CTH K</u>		0.70	MILES			
	YEAR	2001	2002	2003	2004	2005
	ADT	13600	13600	13600	13600	13600
	MVM	3.5	3.5	3.5	3.5	3.5
	TOTAL	143.5	315.6	258.2	28.7	57.4
	INJ	86.1	172.1	143.5	0.0	28.7
	FATL	0.0	0.0	0.0	0.0	0.0
CTH K - CTH UU		1.26	MILES			
	YEAR	2001	2002	2003	2004	2005
	ADT	10395	10593	10795	11001	11211
	MVM	4.8	4.9	5.0	5.1	5.2
	TOTAL	41.7	61.4	80.3	137.9	96.6
	INJ	41.7	40.9	40.1	59.1	38.7
	FATL	0.0	0.0	0.0	0.0	0.0
UU-LOG TAVERN		6.29	MILES			
	YEAR	2001	2002	2003	2004	2005
	ADT	8181	8263	8346	8430	8515
	MVM	18.8	19.0	19.2	19.3	19.5
	TOTAL	53.3	36.9	88.7	67.2	30.7
	INJ	26.6	21.1	52.2	31.0	15.4
	FATL	0.0	0.0	0.0	0.0	0.0

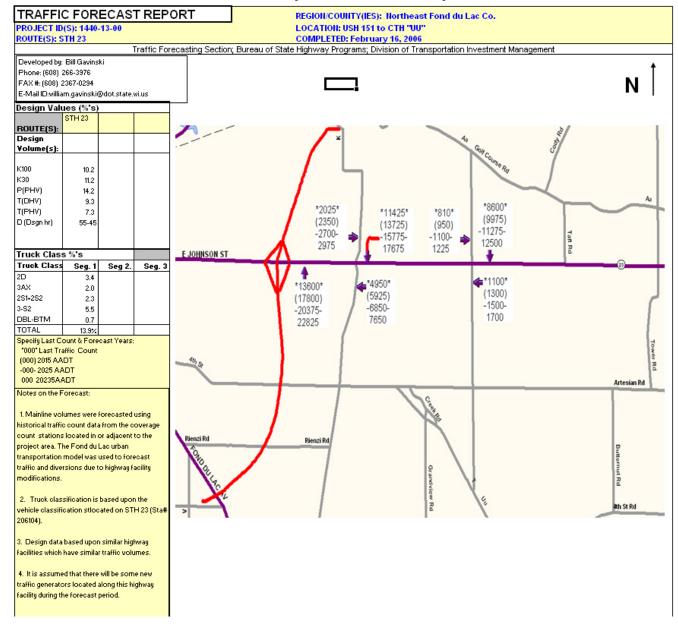
APPENDIX C

WISCONSIN TRAFFIC VOLUME DATA

From 2002 Wisconsin Traffic Counts

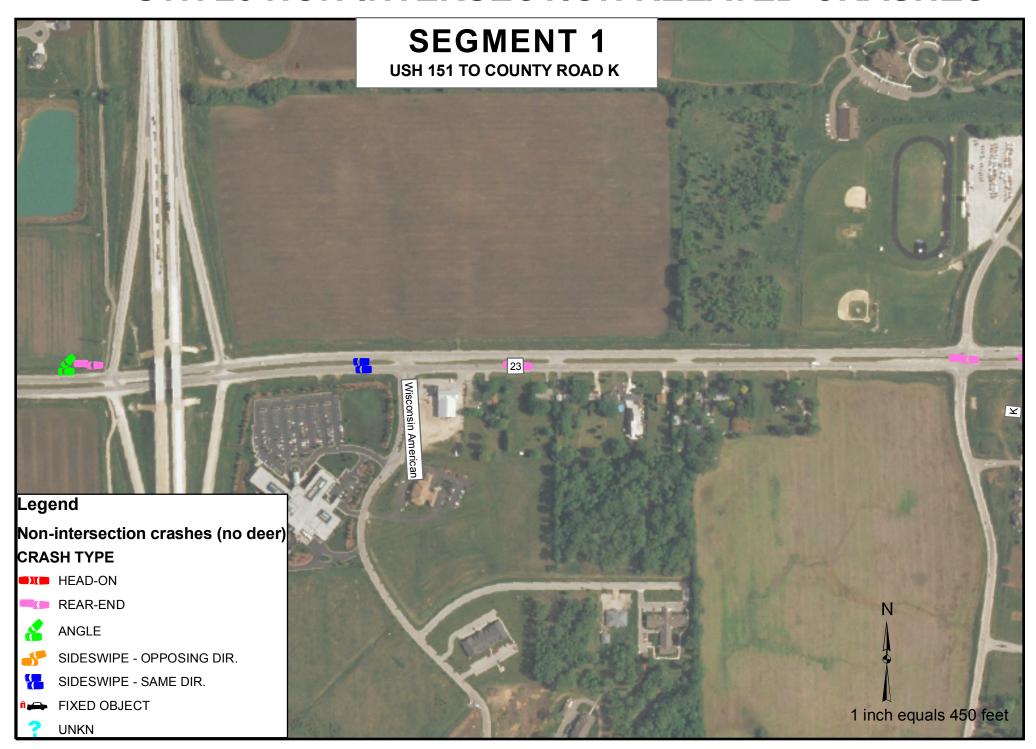


From Wisconsin Department of Transportation

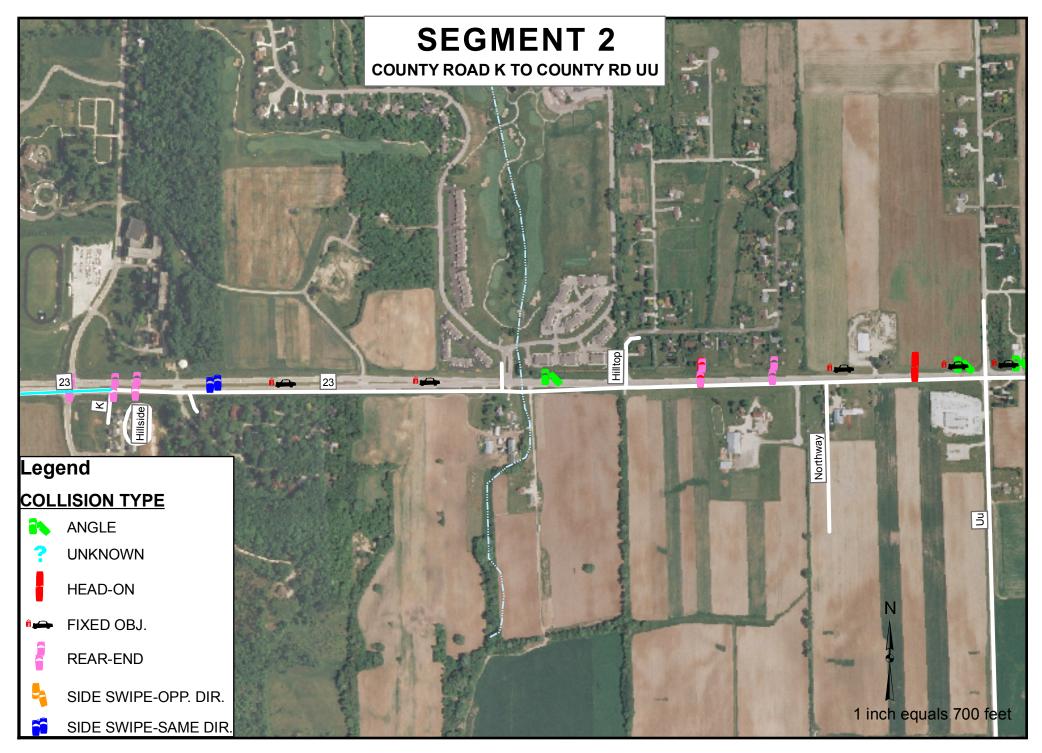


APPENDIX D CRASH MAPS

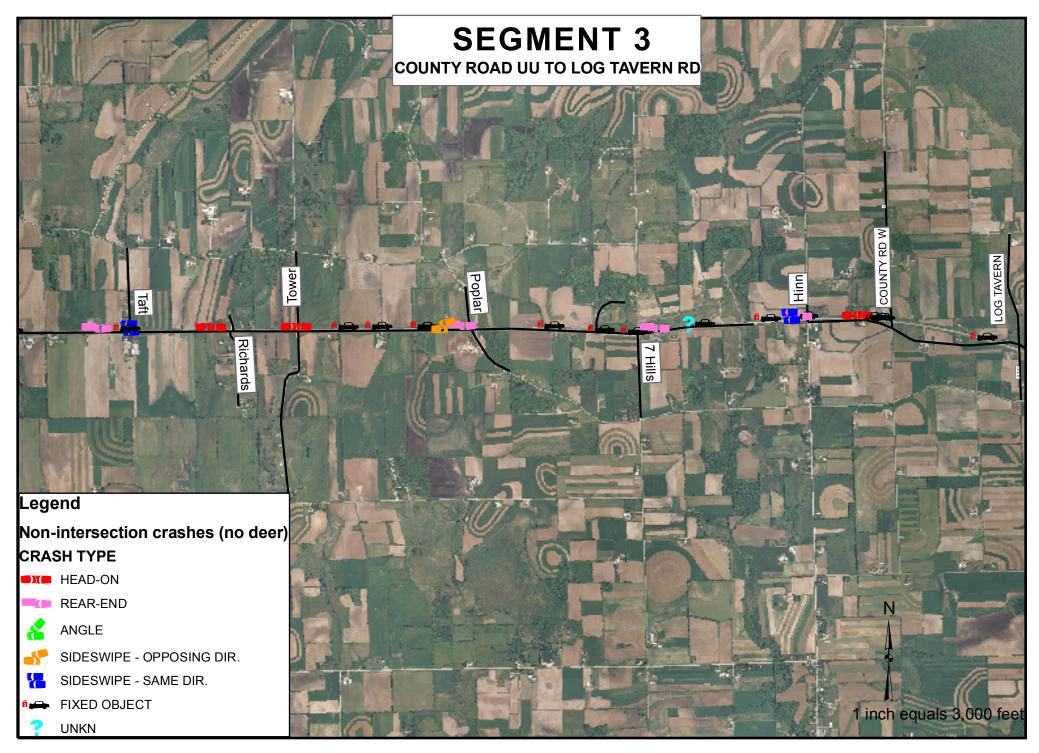
STH 23 NON-INTERSECTION RELATED CRASHES



STH 23 NON-INTERSECTION RELATED CRASHES



STH 23 NON-INTERSECTION RELATED CRASHES



APPENDIX E INTERSECTION RELATED CRASH DATA

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S	W W I Y Y R F	D D L I I O	A N	W T H R C O N D	L G T C O N D	S V R	T O T F A N T L	A C C D T Y P E	M N R C O L	T O T V E	D R V R P C 1 A	POSTSAGD11	D F C S C F 2 D A 2	S A G G E 2 2	M C F L N M B R	COLLØN ITYPE	R H E A R D	N G	0 8	F M S X I S E S S D C	A T	A C T I O N S	Y e a r
1 K	ON 23 E	0 /					4 0		ANGL	3		45 59		35 85		ANGL		1	-		-	EB GO STR SB GO STR	2001
1 K	ON 23 E	0 /		CLDY		INJ	2 0		HEAD	2 F		35 17		45 19		HEAD	- 1	-	-		-	EB LT TRN WB GO STR	2001
1 K	ON 23 W	0 /				INJ	1 0		ANGL	2 F	TY	55 31		45 53		ANGL		1	-		-	NB GO STR WB GO STR	2001
1 K	ON E	0 /	WET	CLDY		PD	0 0		REAR	2		35 52		35 45		REAR	1 -	-	-		1	NB BACKNG NB STOPED	2001
1 K	ON K E	0 /		CLDY		PD	0 0		ANGL	2 F	_	35 49		45 52		ANGL		1	-		-	SB GO STR EB GO STR	2001
1 K	ON 23 E	0 /				INJ	1 0	BIKE	NO C	1 F		35 19		45 34		FIXED		-	-	- 1 -	-	NB GO STR HIT BIKE WB GO STR	2002
1 K	ON 23 E	0 /		CLDY	DARK	PD	0 0)	ANGL	2 F		35 30		45 59		ANGL		1	-		-	NB GO STR EB GO STR	2002
1 K	ON 23 W E	1 <i>I</i>	WET	BLNK		INJ	1 0)	REAR	3 T		45 39		45 58		REAR	1 -	-	-		-	WB GO STR WB STOPED	2002
1 K	ON 23 E	0 /				PD	0 0)	ANGL	2 F	TY	55 16		45 42		ANGL		1	-		-	NB GO STR EB GO STR	2002
1 K	ON 23 W	0 /			DARK		2 0		ANGL	2 D	С	45 20	FTY 3	35 59	02281402641	ANGL		1	-		-	WB GO STR NB GO STR	2002
1 K	ON 23 W	0 /		CLDY		PD	0 0)	ANGL	2 F	TY	45 23	4	45 17	02341700109	ANGL		1	-		1	NB LT TRN WB GO STR	2002
1 K	RTSH 23 E	0 /	Υ	CLDY	DARK	INJ	1 0	DITCH	NO C	1 T	FC	45 40			02100422824	FIXED		-	-	- 1	-	EB LT TRN HIT DITCH	2002
1 K	ON 23 E	0 /		CLDY		PD	0 0)	ANGL	2 F	TY	35 64	4	45 37	03613210982	ANGL		1	-		-	NB GO STR EB GO STR	2003
1 K	ON 23 E	0 /				PD	0 0		ANGL	2		45 37	FTY 4	45 16	03050300044	ANGL		1	-		-	SB GO STR NB LT TRN	2003
1 K	ON 23 E	0 /	WET	RAIN		INJ	2 0		ANGL	2 F	TY	45 20	4	45 51	03633290549	ANGL		1	-		1	SB GO STR EB GO STR	<u>2003</u>
1 K	ON 23 W	0 /				INJ	2 0		ANGL	3 F	TY	35 19	4	45 38	03080450925	ANGL		1	-		1	SB GO STR EB GO STR	2003
1 K	ON 23 E	0 /		CLDY		INJ	3 0		ANGL	2		45 26	FTY 4	45 81	03321811108	ANGL		1	-			EB GO STR SB GO STR	2003
1 K	ON 23 E	0 /	WET	CLDY		PD	0 0		ANGL	2 IT	-	45 28	4	45 27	04652720532	ANGL		1	-		1	WB LT TRN EB GO STR	2004
1 K	ON 23 W	0 /	SNOW	SNOW	LIGT	PD	0 0	GR FAC	NO C	1		45 63			05003491018	FIXED		-	-	- 1	-	NB RT TRN HIT GR FAC	2005
1 K	ON 23 E	0 /		CLDY		INJ	7 0		SSOP	3 F	TY	35 35	4	45 45	05001390234	SSOP		-	1		-	SB GO STR EB GO STR	2005
1 WISCONSIN AMERI	ON 23 E	0 /		CLDY	LIGT	INJ	1 0		ANGL	2 D	С	45 54	4	45 23	03181010400	ANGL		1	-		-	WB LT TRN EB GO STR	2003
1 WISCONSIN AMERI	ON 23 E	0 /				PD	0 0		ANGL	2 F	TY	25 16	4	45 61	03120700781	ANGL		1	-		-	NB LT TRN EB GO STR	2003
		I				PD	13									INT.	1 -	13	1	- 3	4		

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S E I G N T E _ N N T A M # E	R L T N R D W Y	O W Y H C W I Y F	O N H I I V N T D I I R R R	A I CO T D L I CO S CO) F L) A	R O A D C O N D	W T H R C O N D	L G T C O N D	A C C D S V R	T 0 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Γ Ο Γ = - -	A C M C N D R T C Y O P L E	T C T V E	D R V R P C 1 A	P O S T S A D E 1 1 1	D R V R P C C 2 A	P O S T S P D 2		M C F L N M B R	C O L L S N -T Y P E	R E A R	H E A G L		000	Х	M I S C	W E A T H	A C T I O N S	Y e a r
2 HILLTOP DR	ON	23 E		0 <i>I</i>			CLDY		INJ	1	0	ANGL		2	55 4	9 FTY	55	5 47	04451910331	ANGL	-	- 1	-	-	-	-	-	EB GO STR SB GO STR	2004
2 UU	ON	23 E		0 /					INJ	2	0	REAR		2 ID	55 4	7	55	5 49	01190850456	REAR	1		-	-	-	-	-	EB GO STR EB STOPED	2001
2 UU	ON	23 E		0 /		WET	CLDY		INJ	3	0	ANGL		2 FTY	55 2	3	55	5 71	02050181034	ANGL	-	- 1	-	-	-	-	1	NB GO STR EB GO STR	2002
2 UU	ON	23 E		0 /		WET	CLDY		INJ	2	0	ANGL		2 FTY	55 1	8	55	5 22	03160910632	ANGL	-	- 1	-	-	-	-	1	NB LT TRN EB GO STR	2003
2 UU	RTSH	23 E	W	1 <i>I</i>					PD	0	0 DIT	CH NO C		1 ID	55 2	8			03462580144	FIXED	-		-	-	1	-	_	WB GO STR HIT DITCH	2003
2 UU	ON	23 E		0 /					PD	0	0	ANGL		2	55 6	1 FTY	55	5 49	05000840529	ANGL	-	- 1	-	-	-	-	-	EB GO STR NB GO STR	2005
2 UU	ON	23 E		0 /		WET	SNOW		INJ	1	0	REAR		2 FTC	55 1	7	55	5 16	05003611286	REAR	1		-	-	-	-	1	EB GO STR EB LT TRN	2005
2 WHISPERING SPRI	ON	23 E	E	1 <i>I</i>					INJ	2	0	REAR		2 FTC	45 4	0	45	5 53	05002270241	REAR	1		-	-	-	-	-	EB GO STR EB STOPED	2005
				I					PD	10										INT.	3	- 4	-	-	1	-	3		

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S	R L T N R D W Y	O N H O W Y H D W I R) N H I V N ' T O D I R R	A C C C D L O C	L C F L A G	R O A D C O N D	W T H R C O N D	L G T C O N D	A C C D S V R	T O T F A N T J L	A C C D T Y P E	M N R C O L L	T O T V E H	D R V R P C 1 A	POSTSPD1	D R V R A P G C E 2	P O S T S A G D E 2 2		M C F L N M B R	C O L L S N -T Y P E	R H E A A R D	N G	0	F I X S E D	S	W E A T H	A C T I O N S	Y e a r
3 POPLAR RD 3 RICHARDS RD	ON	23 E 23 E		2 1		NOW	SNOW	DARK	PD	1 ()	REAR	2			22 FTC 33 IO	55 16 55 33			REAR	1 -	-	-				WB SL/ST WB GO STR	2004 2001
3 SEVEN HILLS RD	ON	23 E		01			RAIN	DARK	INL	0 0	,	SSS	2	-		28 FTC	55 53			SSS		-	-	1 -			WB LT TRN WB OVT LT	
	SHLD			01	<u> </u>	VET			INJ	1 (,	REAR		ID	_			_		REAR	1 -	-	-		+ -		EB OTHER EB OVT RT	2003
3 SEVEN HILLS RD	ON	23 E		1					INJ	1 ()	ANGL	+	ID	55		55 56			ANGL		1	-				EB OVT RT WB GO STR	2004
3 TOWER RD	ON	23 E		0 /			CLDY		INJ	3 ()	REAR	+	ID	55		55 44	_		REAR	1 -	-	-				EB GO STR EB STOPED	2001
3 W	ON	23 E		5 /	S	SNOW	WIND		INJ	1 ()	REAR	2	FTY	55		55 30			REAR	1 -	-	-				WB GO STR WB GO STR	2001
3 W	ON	23 E		0 /			CLDY		PD	0 ()	NO C	3	IT	55	43	55 71	1	01241070574	MISC		-	-		. 1	-	WB LT TRN WB GO STR	2001
з W	ON	23 E		0 /	V	VET	RAIN		INJ	1 ()	REAR	2		55	32 TFC	55 71	1	03351951301	REAR	1 -	-	-	- -	- -	1	EB LT TRN EB LT TRN	2003
3 W	ON	23 E	Е	20 /					INJ	1 ()	REAR	2	FTC	55	46	55 79	9	03281560575	REAR	1 -	-	-			-	EB GO STR EB SL/ST	2003
3 W	ON	W E		0 /			CLDY	DUSK	INJ	1 ()	REAR	2	UB	55	17	55 26	6	03281560577	REAR	1 -	-	-			-	SB BACKNG SB STOPED	2003
3 W	ON	23 E		0 /					PD	0 ()	ANGL	2	FTY	55	18	55 17	7	03542930965	ANGL		1	- 1			-	SB GO STR WB SL/ST	2003
3 W	ON	23 E		0 /					PD	0 (ANGL		FTY	55		55 25	_		ANGL		1	-	-	. -		EB LT TRN EB GO STR	2003
3 W	ON	23 E		0 /					PD	0)	SSS		IT	55		55 48	_		SSS		_	-	1 -	. _		WB LT TRN WB GO STR	2003
3 W	ON	23 E		0/			CLDY		PD	0 (SSS		IT	55		55 38	_		SSS		T -		1 -	. -		NB RT TRN WB GO STR	2005
				ı					PD	25										INT.	7 -	3	-	3 -	1	5	,	

APPENDIX F NON-INTERSECTION RELATED CRASH DATA

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S	R L T N R D W Y	O N H O W H D W I Y R)	A C C T D L O S C	F L A	R O A D C O R D	W T H R C O N D	L G T C O N D	A C C D S V R	T O T I N J	T COCT DF TAY	M N R C O L L	T O T V E H	D R V R P C 1 A	POSTSAGDE111	D R V R P C 2 A	P O S T S P D 2	A G E 2	M C F L N M B R	C O L S N -T Y P E	R E A R	H A B G L	0	888	F MX II	Α		A C T I O N S	Y e a r
1 K	ON	23 W	W	6 N			CLDY	DARK	INJ	1	0	REAR	2 F	TC	45 17	7	45	16	02351760307	REAR	1		-	-	-	-	WB GO STR	WB SL/ST	2002
1 WISCONS	N AMERI ON	23 E	W	30 N					INJ	1	0	ANGL	2		45 58	B FTY	77	24	02613191505	ANGL	-	- 1	-	-	-	-	EB GO STR	NB GO STR	2002
1 WISCONS	N AMERI ON	23 W	W	6 N					PD	0	0	REAR	2	D	45 41		45	16	03020090350	REAR	1		-	-	-	-	WB GO STR	WB STOPED	2002
1 WISCONS	N AMERI ON	23 E	Е	9 N			CLDY		PD	0	0	REAR	2 F	TC	45 47	7	45	42	02542800202	REAR	1		-	-	-		EB GO STR	EB RT TRN	2002
1 WISCONS	N AMERI BLNK	23 E	W	4 N		BLNK	BLNK		PD	0	0	SSS	2	D	3 36	6	35	16	03362020530	SSS	-		-	1	-	-	WB CHG LN	WB GO STR	2003
1 WISCONS	N AMERI ON	23 E	W	28 N					INJ	1	0	REAR	2 I	D	45 42	2	45	60	03301670194	REAR	1		-	-	-	-	EB GO STR	EB SL/ST	2003
				N																NON-INT	4	- 1	-	1	-				

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S E I G N T E _ N T A M # E	R L T N R D & Y	O N H W Y	O N H I W N Y T D D I R R	I N T D I S	D I L I O A		W T H R C O N	L G T C O N D	ACCDS>R	T C C T F I A N T J L	A C C D T Y P E	M N R C O L L	T O T V E H	D R V R P C 1 A	P O S T S P D 1	D R V R A P G C E 2 1 A	POSTSPD2	A G E 2	M C F L N M B R	COLLØN ITYPE	R H E A R	N G	0	F I S X S E S D	M I S C		A C T I O N S	Y e a r
2 HILLTOP DR	ON	23	E E	40	N				INJ	2	0	REAR	2		55	16 ID	55	57	01321380148	REAR	1 -	-	-	-		-	EB SL/ST EB GO STR	2001
2 HILLTOP DR	ON	23	E E	10	N Y				INJ	1	0	HEAD	2		55	32 DC	55	65	04662780502	HEAD	- 1	-	-	-		_	WB BACKNG WB GO STR	2004
2 HILLTOP DR	ON	23	E E	+	N	SNOW	SNOW		INJ	3	0	REAR	2	FVC	45	19	45	21	04110470845	REAR	1 -	-	-	-		1	WB GO STR ?B GO STR	2004
2 HILLTOP DR	ON	23		+	N				PD	0	0	REAR	2	ID	-	21	55	43	05002000717	REAR	1 -	-	-	-		-	WB GO STR WB STOPED	2005
2 K	ON	23	E E	30	N			DARK	PD	0	0 OBNF	X NO C	1		45	23			02663510434	FIXED		-	-	- ·	1 -	-	WB GO STR HIT OBNFX	2002
2 K	RTSH	23	E E	50	N	ICE	SNOW	DARK	PD	0	0 OVRT	RNNO C	1		45	34	ļ. ļ.		04003520180	FIXED		-	-	- '	1 -	-	EB GO STR HIT OVRTRN	2004
2 K	ON	23	E E	20	N				PD	0	0	SSS	2	IO	45	56	45	59	04251050134	SSS		-	-	1		1	WB NPASZN WB GO STR	2004
2 K	ON	23	W E	9	N	ICE	SLET	DARK	PD	0	0	REAR	2	TFC	45	43	45	47	05000280356	REAR	1 -	-	-	-		1	WB GO STR WB GO STR	2005
2 UU	ON	23	E W	3	N	ICE	SNOW	DARK	INJ	2	0	ANGL	2		55	48 TFC	55	57	02221020545	ANGL		1	-	-		1	WB GO STR EB GO STR	2002
2 UU	RTSH	23	E W	4	N	ICE	CLDY		INJ	1	0 DITCH	I NO C	1	TFC	55	23			03211150199	FIXED		-	-	- '	1 -	1	EB GO STR HIT DITCH	<u>2003</u>
2 UU	RTSH	23	E W	20	N	SNOW	SNOW		PD	0	0 EMBK	м по с	1	TFC	55	58			04010051741	FIXED		-	-	- '	1 -	1	WB GO STR HIT EMBKMT	2003
2 UU	ON	23	E W	10	N	SNOW	WIND		PD	0	0	HEAD	2	TFC	55	17	55	25	04110480477	HEAD	- 1	-	-	-		1	WB GO STR EB GO STR	2004
2 WHISPERING SPRI	ON	23	E E	10	N			DARK	PD	0	0	ANGL	2	ID	45	18	45	49	04582430915	ANGL		1	-	-		-	WB GO STR WB GO STR	2004
					N															NON-INT	4 2	2	-	1 4	4 -	7		

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S E I G N T E N N T A M	R O A A A T H I I C I N O W N N C C R N Y T T D F D H D D L I W W I I I I O A	R W O T A H D R C C C C O N N	L G T C O N	A C C D S V	T O O T F I A N T	A C M C N D R T C Y O P L	T O T V E	D R V R P C 1	P O S T S P D	D R V R P C 2	P O S T S A G D E	M C F L N M B	C O L L S N T Y P	R E A		A S S O	<i>w w</i>	F I X E		A C T I O N	Y e a
# E	Y Y R R S C C	D D	D	R .	J L	E L	Н	A	1 1	Ā	2 2	R	E		D I	L P	S		Č I	d S	r
3 HINN RD	ON 23 E W 20 N	CLDY		INJ	1 0 D	ITCH NO C	1 1	D	55 46			02482460414	FIXED	-	-	- -	-	1	-	- WB GO STR HIT DITCH	2002
3 LOG TAVERN RD	RTSH 23 E W 30 N	ICE SLET		INJ		SIGN NO C	1	FVC	55 50	+		01170720166	FIXED	-	-		-	1	-	1 WB GO STR HIT TFSIGN	2001
3 LOG TAVERN RD	RTSH 23 E W 20 N Y			INJ	1 0 O	VRTRNNO C	1 1	FVC	55 25			03120691918	FIXED	-	-		-	1	-	- EB GO STR HIT OVRTRN	<u>2003</u>
3 POPLAR RD	ON 23 E W 10 N	CLDY	DUSK	INJ	2 0	REAR	5		55 34	FVC	55 27	01663190959	REAR	1	-		-	-	-	- EB STOPED EB SL/ST	2001
3 POPLAR RD	ON 23 E W 30 N	XWIND		PD	0 0 0	BNFX NO C	2		55 44		55 21	01251140904	FIXED	-	-		-	1	-	- EB GO STR HIT OBNFX WB GO STR	2001
3 POPLAR RD	RTSH 23 E E 10 N	ICE SLET		INJ	1 0 D	ITCH NO C	1	TFC	55 23			03030170438	FIXED	-	-	- -	-	1	-	1 WB GO STR HIT DITCH	2003
3 POPLAR RD	RTSH 23 E W 30 N	SNOW SNOW		PD	0 0 E	MBKMTNO C	1	TFC	55 53			04200860191	FIXED	-	-		-	1	-	1 WB GO STR HIT EMBKMT	2004
3 POPLAR RD	ON 23 E W 20 N	CLDY		INJ	1 0	SSOP	2		55 19	FVC	55 18	04451910406	SSOP	-	-	- 1	-	-	-	- EB GO STR WB GO STR	2004
3 RICHARDS RD	ON 23 E W 10 N	ICE CLDY	DARK	INJ	2 0	HEAD	2	TFC	55 45		55 55	03663430880	HEAD	-	1		-	-	-	1 EB GO STR WB GO STR	2003
3 SEVEN HILLS RD	ON 23 E W 10 N Y		DARK	INJ	2 0	HEAD	2	0	55 22		55 52	02532770811	HEAD	-	1		-	-	-	- WB OVT LT EB GO STR	2002
3 SEVEN HILLS RD	ON 23 E E 40 N	WET CLDY		INJ	2 0 O	VRTRNNO C	1	TFC	110 97	•		02351750169	FIXED	-	-		-	1	-	1 WB GO STR HIT OVRTRN	2002
3 SEVEN HILLS RD	ON 23 E W 1 N	CLDY		PD	0 0 0	T ANM NO C	1		55 27			02291440151	FIXED	-	-		-	1	-	- WB GO STR HIT OT ANML	2002
3 SEVEN HILLS RD	ON 23 E E 10 N	ICE	DARK	INJ	1 0	REAR	2		55 56	TFC	55 0	04823480652	REAR	1	-		-	-	-	1 EB GO STR EB GO STR	2004
3 SEVEN HILLS RD	ON 23 E W 50 N	CLDY		INJ	1 0 O	TH NC NO C	2		55 33		55 47	05002710227	FIXED	-	-		-	1	-	- EB GO STR HIT OTH NC WB GO STR	2005
3 SEVEN HILLS RD	ON 23 E E 30 N	SNOW SNOW	DARK	INJ	2 0	NO C	5	FVC	55 19	FVC	55 67	05000810617	MISC	-	-		-	-	1	1 WB GO STR EB GO STR	2005
3 TAFT RD	ON 23 E W 10 N	ICE SNOW	DARK	PD	0 0	SSS	2		55 43	FTY	55 31	03070381451	SSS	-	-		1	-	-	1 EB GO STR EB LT TRN	2003
3 TAFT RD	ON 23 E W 20 N			PD	0 0 M	AILBO REAR	2		55 17	ID	55 17	04391660287	REAR	1	-		- 1	-	-	- EB STOPED HIT MAILBOX EB SL/ST	2004
3 TAFT RD	ON 23 E W 20 N			INJ	1 0	REAR	2	FTC	55 44		55 55	04512151347	REAR	1	-		- 1	-	-	- WB SL/ST WB SL/ST	2004
3 TOWER RD	ON 23 E E 50 N			PD	0 0 FI	RE NO C	1		55 49		l	01431930687	FIXED	-	-		-	1	-	- WB GO STR HIT FIRE	2001
3 TOWER RD	ON 23 E E 30 N			PD		BNFX NO C	3		55 37	+	55 23	02200950425	FIXED	-	-		-	1	-	- WB GO STR HIT OBNFX WB GO STR	
3 UU	ON 23 E E 20 N		DARK	INJ	1 0	SSS	2		55 39	+	55 22	02653432657	SSS	-	-		1	-	-	- EB LT TRN EB OVT LT	2002
3 UU	ON 23 E E 10 N	SNOW SNOW		INJ	1 0	ANGL	2	TFC	55 20	1	55 32	04010051696	ANGL	-	-	1 -	- 1	-	-	1 WB GO STR IWB GO STR	2003
3 UU	ON 23 E E 15 N	WET		INJ	1 0	REAR		FTC	55 17	1	55 41	03160870065	REAR	1	-		-	-	-	1 WB GO STR WB SL/ST	2003
3 UU	RTSH 23 E E 15 N	SNOW SNOW		INJ	1 00	T PST NO C	+ +		55 19	+			FIXED		_		1	1		1 WB GO STR HIT OT PST	2003
3 UU	ON 23 E E 5 N	CLDY	DARK	PD	0 0	ANGL		FTY	55 33	-	55 23	03673500448	ANGL	_	_	1 -	- 1		_	- EB MERGNG WB GO STR	2003
3 UU	LTSH 23 E E 100 N	ICE SNOW		PD	0 0 TI	REE NO C	1		0 42	+		03663430696	FIXED	_	_	<u> </u>	- 1	1	_	1 ?B BLNK HIT TREE	2003
3 UU	ON 23 E E 10 N	CLDY		PD		T ANM NO C	1		55 30	_	<u> </u>	04733061602	FIXED	_	_		1	1		- EB GO STR HIT OT ANML	2004
3 UU	LTSH 23 E E 30 N Y		_	PD		AILBO NO C	1	DC	55 65	_		04682850559	FIXED	_	_			1	_	- WB GO STR HIT MAILBOX	2004
3 UU	RTSH 23 E E 3 N			PD		ULVRT NO C	1		55 18			04421800849	FIXED	_				1		- EB GO STR HIT CULVRT	2004
3 UU	ON 23 E E 10 N	CLDY		IN.I	2 0	ANGL	2		55 73	+	110 83		ANGL	_	_	1 -	- 1	Ė	_	- EB LT TRN WB GO STR	2004
3 UU	RTSH 23 E E 20 N	SNOW SNOW	DAWN	PD	0 0 0	TPOLE NO C			55 32		110 00	05000600467	FIXED	_	_	<u> </u>	- 1	1	_	1 EB GO STR HIT UTPOLE	2005
3 UU	LTSH 23 E E 10 N	SNOW SNOW	DARK	IN.I		REE NO C			55 19			05000671340	FIXED	_				1		1 EB GO STR HIT TREE	2005
3 W	ON 23 E W 20 N			IN.I	3 0	HEAD	3		55 16	+	55 39		HEAD	_	1			Ė		- WB GO STR EB GO STR	2001
3 W	PLOT 23 E W 10 N		DUSK	PD	0 0	NO C	3		55 57	_	55 17	01633060204	MISC						1	- WB GO STR EB RT TRN	2001
3 W	ON 23 E W 6 N	SNOW SNOW		PD	0 0	REAR	21		55 41	+	55 17	02100422272	REAR	1						1 WB RT TRN WB GO STR	2002
3 W	ON 23 E E 10 N	SNOW WIND		PD	0 0	SSS		TFC	55 24	_	55 45	03140790111	SSS				1			1 WB OVT LT WB GO STR	2003
3 W	LTSH 23 E W 10 N	SNOW SNOW		PD	0 0 0	TCH NO C			55 24	_	00 40	04200860179	FIXED					1		1 EB GO STR HIT DITCH	2003
3 W	RTSH 23 E W 4 N	SNOW SNOW		PD		SIGN NO C		TFC	55 25	+		04200860179	FIXED					1		1 WB GO STR HIT TFSIGN	2004
3 W	LTSH 23 E W 6 N	SNOW SNOW		PD		SIGN NO C			55 20	1		05000770385	FIXED					1		1 EB GO STR HIT TFSIGN	2004
3 V V	LISH 23E W 6N	SNOW	DAKK	<u>עו</u>	0 0 11	SIGN INC C		10	33 20			03000770363	NON-INT	6	2	3 1	3	04	2 '	9	2003

INTERSECTION LOCATION - STH 23 EB & WB JUB HANDLE & CTH K

Project ID - 1440-15-70 Intersection Location – STH 23 EB & WB Jug Handle & CTH K	WB Jug Handle & CTH K			
Factor	ALTERNATIVE CONTROL TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP 2-WAY STOP EXISTING CONTROL		ALTERNATIVE CONTROL TRAFFIC SIGNAL, ANTICIPATING TRAFFIC SIGNAL ROUNDABOUT 4-WAY STOP 2-WAY STOP EXISTING CONTROL	
Safety				
Operational Analysis				
Construction Cost				
Right-of-Way				
Practical Feasibility				
Operation & Maintenance Cost				
Environmental				
Pedestrian and Bicycles				
Recommendation				
Responsibility	PIP Team	PDS Team	PIP Team	PDS Team